



**A GENERAL STUDY OF UNDERSAMPLING PROBLEMS IN
MONTE CARLO CALCULATIONS**

**A Dissertation
Presented for the
Doctor of Philosophy
Degree
The University of Tennessee, Knoxville**

Wilson José Vieira

December, 1989

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To the Graduate Council:

I am submitting herewith a dissertation written by Wilson José Vieira entitled "A General Study of Undersampling Problems in Monte Carlo Calculations ." I have examined the final copy of this dissertation for form and content and recommend that it be accepted in partial fulfillment of the requirements for the degree of Doctor of Philosophy, with a major in Nuclear Engineering.

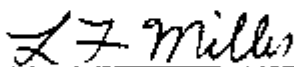


Paul N. Stevens, Major Professor

We have read this dissertation
and recommend its acceptance:







Accepted for the Council:



Vice Provost
and Dean of The Graduate School

DEDICATION

to Ligia and Daniel.

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ABSTRACT

Various techniques devised to flag undersampling conditions were investigated. Undersampling conditions can often lead to underestimation and a solution which can be significantly smaller than the true solution but the estimate of the standard deviation may seem acceptably small. In an attempt to identify undersampling in Monte Carlo calculations, the estimation of F values, the coefficient of variation of the standard deviation, the figure of merit, and a particle contribution distribution histogram were incorporated into the MORSE code.

It was found for the problems considered that the F tests were not conclusive because the distribution of contributions was not normally distributed. The calculation of the coefficient of variation turned out to require significantly more computational effort than that necessary to directly achieve a very small standard deviation because of its dependency upon the kurtosis of the distribution which takes much longer than the variance to achieve a stable value. If the kurtosis is not too large, this coefficient can be used in problems which demand high degrees of precision such as criticality calculations.

The figure of merit $FOM = 1/\sigma^2t$ is a function of the variance of the population which becomes stable faster than its coefficient of variation. Therefore, the *FOM* provides a more reliable guarantee of a stable solution - also, because it tends to a constant value, it is more easily analyzed. However, in severe undersampling conditions the *FOM* may become apparently constant over a large range of sample sizes and then abruptly changing with the sampling of rare particles. Also, a sudden increase in the variance may not have an accompanying significant change in the mean while the figure of merit experiences a jump. Under this condition, the solution may still be a perfectly acceptable estimate.

The creation of the particle contribution distribution which is output at the end of each

batch provides a very effective way of detecting undersampling. If only a few particles account for a large fraction of the response, the estimates of both mean and standard deviation should be regarded as unreliable and, therefore, the sample size should be increased.

Although not thoroughly investigated, the utilization of the statistical tools implemented into the MORSE code was demonstrated to be useful in the study of the behavior of particle distributions when subjected to various biasing and/or estimation procedures.

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Chapter 1

Introduction

Monte Carlo calculations are possible in almost every field which involve mathematical modeling. All such Monte Carlo analyses comprise of the generation of sequences of random variables and have as solutions estimates of means and variances. The problems can range from the estimation of the mean of a small set of Monte Carlo generated data to the estimation of detailed radiation particle flux distributions which represent the solutions of the familiar integro-differential Boltzmann transport equation.

The quality of a Monte Carlo calculation involves two basic concerns: accuracy and precision. Accuracy is a measure of how close the Monte Carlo estimate is from the true value and is related with the amount of *bias*. Precision is a measure of the statistical uncertainty associated with the estimate and is usually expressed in terms of the standard deviation. Many factors can introduce bias into the Monte Carlo solution of a problem which will affect accuracy as well as the behavior of the estimator of precision. Bias can be caused by inadequacies of the model such as may occur in geometry or cross section descriptions and through the use of some sampling schemes such as point-detector estimators whose expected values are not the true solutions. One interesting way to understand the role of the parameters involved in a statistical estimation is to address the following question: *How can the quality of an estimate be guaranteed?* This raises another question: *Does the population sample represent the true population?* The answer to these questions is the major objective of this work which is to analyze the statistical features of the mean, variance, and

population sample and to devise schemes to utilize more of the information generated during the calculation.

Undersampling occurs in problems where the effect of interest is determined primarily by very rare events and a very large population sample is required to achieve a good estimate. In a completely analog Monte Carlo particle transport calculation, the distribution of the scores is binomial and the effect of interest is simply the probability of scoring a success. Therefore the scores of a problem with a small scoring probability would be mostly zeroes and would require on the order of 400 successes (rare events) to achieve a 5% fractional standard deviation - approximately $1/\sqrt{n}$ where n is the number of successes. Undersampling has been recognized as a major source of concern. The inexperienced user may not recognize this condition and accept a solution that can be orders of magnitude too low even though the standard deviation indicates good precision. This problem was pointed out by Gelbard [1] and Cramer et al. [2], both of whom considered that many of the problems associated with statistical uncertainty were still unresolved. Dubi et al. [3] showed that the one-particle method yields more reliable estimates of the variance, but also recognized the usefulness of the batch method. Lux et al. [4] devised a correction scheme for the estimates of the mean and variance and emphasized the importance of distinguishing between rare events and the unimportant background.

The problem of *undersampling* is particularly important when point-detector estimators are used because the contributions to the outer detectors from collisions near the source region are by their nature very small and can be essentially of the same magnitude. If a sufficient number of particles are not sampled to include enough particles which experience rare events, the final results will be unrealistically small while their standard deviations may indicate seemingly acceptable results. In this work, this condition will be called *underestimation*. The computational evolution of a statistically acceptable estimate of an effect of interest, in a deep penetration problem using a point-detector estimator, presents three different stages. The first stage is when undersampling is so severe that no major-contributing

particle is sampled. A major-contributing particle is not only a particle that yields a high contribution relative to background values but also the value of its contribution has to be sufficiently high to significantly move the estimated solution up to values around the true mean. One way of detecting the undersampled condition during the first stage would be to analyze the statistics throughout the region between the source and the point of interest. This procedure is based on the fact that the standard deviation should increase with the distance from the source. If it decreases, this condition indicates that the contributions are due to collisions far from the detector and that there were no important collisions (rare events) near the detector. The second stage is when a few major-contributing particles are sampled. The results as they evolve during this stage will experience jumps in the estimated fluxes and also in their variances. Finally, the third stage is reached when a sufficient number of major-contributing particles are sampled and unbiased estimates are achieved. This behavior is more or less obvious and depends upon factors such as the distance in mean free paths between the source and the detector and the utilization of the various variance reduction techniques.

In Chapter 2 some theoretical considerations about the interpretation of Monte Carlo results are presented. Chapter 3 describes the modifications made to a standard version of the MORSE code [5] to accomplish the calculation and output of the additional information. This modified version of MORSE will be designated as the MORSE/STAT package.

Chapter 4 describes the problems studied and the techniques used in their solution, such as type of estimators and variance reduction techniques used. The results for each problem are analyzed in Chapter 4 with respect to the benefits realized by the user through the proper interpretation of the additional information compiled by the bookkeeping procedures implemented into the MORSE code.

Chapter 2

Theoretical Background

The mathematical and statistical bases which underlie this study are presented in this chapter.

2.1 Measures of Error

The variance and mean square error are central to the characterization of the error associated with a sampling distribution. The population variance of an estimator is a measure of the dispersion of the distribution around the mean, and the mean square error which is a measure of the dispersion around the true value of the parameter. The mean square error can be defined as the sum of the variance plus the square bias i.e.

$$MSE = E(x - \bar{x})^2 + E(\bar{x} - \mu)^2. \quad (2.1)$$

Bias is another concept of error and is defined as the difference between the estimated mean and the true value of the parameter. If the bias is equal to zero, then the mean square error is given by the variance alone.

2.2 Estimators for the Mean and Variance

The statistical behavior of estimators commonly used in Monte Carlo calculations can be better understood with the consideration of some *Analysis of Variance* theory. Consider a

Table 2.1: A Standard Analysis-of-Variance Table.

<i>Group</i>						
1	2	...	i	...	I	
x_{11}	x_{21}	...	x_{i1}	...	x_{I1}	
x_{12}	x_{22}	...	x_{i2}	...	x_{I2}	
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	
x_{1j}	x_{2j}	...	x_{ij}	...	x_{Ij}	
\vdots	\vdots	\vdots	\vdots	\vdots	\vdots	
x_{1J}	x_{2J}	...	x_{iJ}	...	x_{IJ}	
\bar{x}_1	\bar{x}_2	...	\bar{x}_i	...	\bar{x}_I	\bar{x}

population sample of I groups each with J elements as shown in Table 2.1. Summing the x_{ij} over j , the mean corresponding to the i th group is given by

$$\bar{x}_i = \frac{1}{J} \sum_{j=1}^J x_{ij}. \quad (2.2)$$

An estimator for the total mean μ is the average of the I \bar{x}_i estimates

$$\bar{x} = \frac{1}{I} \sum_{i=1}^I \bar{x}_i, \quad (2.3)$$

which is equivalent to the estimator

$$\bar{x} = \frac{1}{N} \sum_{n=1}^N x_n, \quad (2.4)$$

where $N = I \times J$. Equation 2.4 effectively considers all elements to belong in just one group, i.e.

$$\bar{x} = \frac{1}{IJ} \sum_{i=1}^I \sum_{j=1}^J x_{ij}. \quad (2.5)$$

It is possible to derive various estimators for the population variance σ^2 . The first one S_w^2 is called the variance of *mean square within*, which can be calculated using

$$S_i^2 = \frac{1}{J-1} \sum_{j=1}^J (x_{ij} - \bar{x}_i)^2 \quad (2.6)$$

so that

$$S_w^2 = \frac{1}{I} \sum_{i=1}^I S_i^2. \quad (2.7)$$

This estimator is used when results from several runs are combined and represents the population variance of the grand mean.

Another estimator for the population variance S_0^2 is called variance of the *mean square between*, which is based on the fact that for a sufficient number of elements, the group means are normally distributed with a variance equal to the population variance divided by J

$$\frac{\sigma^2}{J} = \frac{1}{I-1} \sum_{i=1}^I (\bar{x}_i - \bar{x})^2, \quad (2.8)$$

and

$$S_0^2 = \frac{J}{I-1} \sum_{i=1}^I (\bar{x}_i - \bar{x})^2. \quad (2.9)$$

This is the *batch* estimate of the population variance and is the procedure used in standard versions of the MORSE Monte Carlo code.

Finally, a third estimator for the population variance is designated as S_t^2 and is called the variance of the *mean square total*,

$$S_t^2 = \frac{1}{N-1} \sum_{i=1}^I \sum_{j=1}^J (x_{ij} - \bar{x})^2. \quad (2.10)$$

This is the *one particle* estimate of the population variance and is the procedure used in most Monte Carlo programs.

Any of the equations 2.11, 2.12, or 2.13 can be used to calculate an estimate for the population variance S^2 and estimates for the variance of mean $S_{\bar{x}}^2$ are given by:

$$S_{\bar{x}}^2 = \frac{1}{N} S_w^2, \quad (2.11)$$

$$S_{\bar{x}}^2 = \frac{1}{N} S_0^2, \quad (2.12)$$

and

$$S_{\bar{x}}^2 = \frac{1}{N} S_t^2. \quad (2.13)$$

Equations 2.12 and 2.13 represent the *batch* estimator and the *one particle* estimator of the variance of the mean, respectively.

The fractional standard deviation (*FSD*) is the estimate of precision calculated in the MORSE code and is given by:

$$FSD = \frac{\sqrt{S_x^2}}{\bar{x}} \quad (2.14)$$

Equations 2.7, 2.9, and 2.10 can be written as

$$S_w^2 = \frac{SSW}{I(J-1)} \quad (2.15)$$

$$S_b^2 = \frac{SSB}{I-1} \quad (2.16)$$

$$S_t^2 = \frac{SST}{N-1} \quad (2.17)$$

Remembering the *sum-of-squares* identity

$$\sum_{i=1}^I \sum_{j=1}^J (x_{ij} - \bar{x})^2 = J \sum_{i=1}^I (\bar{x}_i - \bar{x})^2 + \sum_{i=1}^I \sum_{j=1}^J (x_{ij} - \bar{x}_i)^2, \quad (2.18)$$

the following relationship follows

$$SST = SSB + SSW. \quad (2.19)$$

Therefore, just two of the three sums have to be calculated and the other can be obtained from Equation 2.19.

2.3 An F-test for the Equality of the Group Means

One way to guarantee sufficient accuracy in the Monte Carlo estimate is to observe the individual solutions of the groups which comprise the total solution. It is expected that the group means are normally distributed, but suppose that one of the groups yielded a much larger value for its mean. This would strongly suggest the existence of undersampling in all the batches — since the batches were drawn from the same population, individual groups having equal numbers of samples should have essentially the same estimates for their means and variances. Therefore, it would be necessary to increase the group size so that the distribution of the group means becomes more normal and also the variance of the grand

mean becomes smaller. Before proceeding further, expressions for the expected values of S_b^2 and S_w^2 are derived. From a linear model, each element x_{ij} from the i -th group is written as

$$x_{ij} = \mu_i + \epsilon_{ij}, \quad (2.20)$$

where μ_i is the mean of the i -th group and ϵ_{ij} is the random error of the individual samples which is assumed to have a mean zero and a variance σ^2 . The x_{ij} can be expressed in terms of the the group mean μ_i and the grand mean μ

$$x_{ij} = \mu + \alpha_i + \epsilon_{ij}, \quad (2.21)$$

where

$$\mu_i = \mu + \alpha_i. \quad (2.22)$$

Therefore, it will be possible to distinguish between the variance production due to the variation of the group means μ_i and that due to the variation of the elements of the population ϵ_{ij} . The *fixed effect* model is characterized by $\sum_{i=1}^I \alpha_i = 0$, otherwise the *random effect* model [6] applies. However, since both models utilize the same F-test, the fixed effect model will be used — which should be appropriate for the present analysis.

The expected value of S_b^2 can be calculated by substituting

$$\bar{x}_i = \mu + \alpha_i + \bar{\epsilon}_i \quad (2.23)$$

and

$$\bar{x} = \mu + \bar{\epsilon} \quad (2.24)$$

into Equation 2.9, which yields

$$E(S_b^2) = \frac{J}{I-1} \sum_{i=1}^I E(\alpha_i + \bar{\epsilon}_i - \bar{\epsilon})^2. \quad (2.25)$$

Since $\sum_{i=1}^I \alpha_i = 0$ and $E(\epsilon_{ij}) = 0$, Equation 2.25 can be rewritten as

$$E(S_b^2) = \frac{J}{I-1} \sum_{i=1}^I E(\alpha_i^2 + \bar{\epsilon}_i^2 + \bar{\epsilon}^2). \quad (2.26)$$

With the fact that

$$E(\bar{\epsilon}_i^2) = \sigma^2/J, \quad (2.27)$$

and

$$E(\bar{\epsilon}^2) = \sigma^2/IJ, \quad (2.28)$$

Equation 2.26 becomes

$$E(S_b^2) = \sigma^2 + \frac{J}{I-1} \sum_{i=1}^I \alpha_i^2, \quad (2.29)$$

which can be written as

$$E(S_b^2) = \sigma^2 + J\bar{\alpha}^2. \quad (2.30)$$

The expected value of S_w^2 can be derived by substituting $E(\bar{x}_i) = \mu$ into Equation 2.7.

That is

$$E(S_w^2) = E\left(\frac{1}{I} \sum_{i=1}^I \frac{1}{J-1} \sum_{j=1}^J (x_{ij} - \mu)^2\right), \quad (2.31)$$

which yields

$$E(S_w^2) = E\left(\frac{1}{J} \sum_{i=1}^I \sigma^2\right) = \sigma^2. \quad (2.32)$$

A statement of the F-test for the equality of the group means would be:

$$\begin{aligned} H_0 : \mu_1 = \mu_2 = \dots = \mu_I \\ H_1 : \text{at least one is different,} \end{aligned} \quad (2.33)$$

and it is performed by calculating

$$F_{(I-1)(N-I)} = \frac{S_b^2}{S_w^2}, \quad (2.34)$$

which has as expected value

$$\frac{\sigma^2 + J\bar{\alpha}^2}{\sigma^2}. \quad (2.35)$$

When the null hypothesis is true, the test yields a value of one. The ability to perform such tests is one of the most important features of the batch method.

From the above discussion there are some important observations. First, S_b^2 is greater than or at least equal to S_w^2 . Therefore, S_w^2 and S_t^2 are more reliable because they provide

tighter bounds for the statistical error. Second, as demonstrated above, S_f^2 can be used together with S_w^2 to calculate F values that may detect anomalous differences between the group means — which can be an effect associated with undersampling. Another interesting fact is that because both S_w^2 and S_f^2 take in account the variations within the elements of the population they are approximately equal — which also can be implied from the fact that they have the same expected value σ^2 . This means that S_w^2 can be used instead of S_f^2 which is a good way to avoid computational round-off errors.

2.4 Coefficients of Variation

Another procedure that provides measures of reliability of the various estimators is the concept of relative error. The coefficient of variation V is defined as the square root of the relative variance of the population V^2 , which is given by:

$$V^2 = \frac{S^2}{\bar{x}^2} = \frac{1}{N-1} \sum_{i=1}^N \frac{(x_i - \bar{x})^2}{\bar{x}^2}. \quad (2.36)$$

Analogously, the relative variance of the variance is given by:

$$V_{S^2}^2 = \frac{\sigma_{S^2}^2}{(\sigma^2)^2}. \quad (2.37)$$

Hansen, Hurwitz, and Madow [7] (see Appendix D) demonstrated that Equation 2.37 can be expressed as

$$V_{S^2}^2 = \frac{1}{N} \left(\beta - \frac{N-3}{N-1} \right), \quad (2.38)$$

where

$$\beta = \frac{\mu_4}{(\sigma^2)^2}, \quad (2.39)$$

$$\sigma^2 = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})^2, \quad (2.40)$$

$$\mu_4 = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})^4 \quad (2.41)$$

$$= \bar{x}_4 - 4\bar{x}\bar{x}_3 + 6\bar{x}^2\bar{x}_2 - 3\bar{x}^4, \quad (2.42)$$

and

$$\bar{x}_r = \frac{1}{N} \sum_{i=1}^N x_i^r. \quad (2.43)$$

For sufficiently large N , Equation 2.38 becomes:

$$V_{S^2}^2 = \frac{\beta - 1}{N}, \quad (2.44)$$

and for sufficiently large β

$$V_{S^2}^2 = \frac{\beta}{N}. \quad (2.45)$$

For I random groups of J elements, it can be shown that

$$V_{S^2}^2 = \frac{1}{I} \left(\beta_J - \frac{I-3}{I-1} \right), \quad (2.46)$$

where

$$\beta_J = \frac{\beta}{J} + 3 \frac{J-1}{J}. \quad (2.47)$$

The derivations of Equations 2.46 and 2.47 can be found in reference [7] (see Appendix D).

The coefficient of variation of the standard deviation V_S is related with the coefficient of variation of the variance V_{S^2} by

$$V_S = \frac{V_{S^2}}{2}. \quad (2.48)$$

The proof of Equation 2.48 can also be found in reference [7] (see also Appendix D). A reasonable value for V_S is a subject for concern. The confidence limits for the standard deviation do not need to be the same as the confidence limits for the mean. Because V_S depends upon the kurtosis of the distribution, the significance of the confidence limits of the standard deviation varies for different distributions. A distribution with a large kurtosis is characterized by a large value for V_S which can be more reliable than an undersampled distribution with a small kurtosis and a much smaller V_S .

According to the central limit theorem, as J increases the distribution of the group means becomes more normal and β_J approaches the value of 3. If a normal distribution for the group means is assumed and if a 0.1 value for V_S is desired, at least 51 groups would

be necessary as indicated by Equation 2.46. Therefore, to achieve a coefficient of variation of the standard deviation on the order of 0.1, a reasonable number of groups ($I > 50$) and a sufficiently large value of J are required so that the group means would be normally distributed. However, the results obtained with Equation 2.38 were consistently smaller than those obtained with Equation 2.46, which may be explained by the same argument that the expected value of the mean square within is smaller than the expected value of the mean square between. Because of this reasoning, Equation 2.38 is used instead of Equation 2.46. Also, it is shown in Chapter 4 that to achieve a stable value of β , a sample size larger than the one necessary to achieve a sufficiently reliable estimate of S^2 is required.

2.5 The Figure of Merit

The figure of merit $\sigma_{\bar{x}}^2 T$ is widely accepted as a measure of the calculational efficiency and also as an indicator that the solution has achieved the asymptotic $1/\sqrt{N}$ behavior as predicted by the central limit theorem. The figure of merit can also be expressed as

$$FOM = \frac{1}{\sigma_{\bar{x}}^2 T}, \quad (2.49)$$

where $\sigma_{\bar{x}}^2$ is the variance of the mean and T is the total computation time. A larger FOM indicates a more efficient calculation.

Considering t as the average computation time per particle, Equation 2.49 can be rewritten as

$$FOM = \frac{N}{\sigma^2 N t} = \frac{1}{\sigma^2 t}. \quad (2.50)$$

Therefore, when σ^2 becomes constant, i.e. a sufficient number of particles have been sampled, the figure of merit also becomes constant. However, for highly skewed distributions with a small proportion of very large contributions, the behavior of $\sigma_{\bar{x}}^2$ is typically not $1/\sqrt{N}$ and may assume either faster or slower rates of convergence. The figure of merit will become stable only after a sufficient number of particles have been sampled. Also, if undersampling is severe, the figure of merit will appear essentially constant over a wide range of sample sizes thus giving false indications about the solution.

2.6 Sampling of Rare Events

In deep penetration particle transport problems, the utilization of some form of importance sampling is necessary. For example, an analog solution of a deep penetration problem with a transmission factor of 10^{-12} will require an average of 10^{12} particles to score a success. It is obvious that if a reasonable number of successes are not scored, the results will be worthless. If the parameter being estimated is already known, the sampling scheme can be modified so that every sample yields the same contribution - which results in what is called a zero-variance calculation. It is possible to use any previously known information about the population distribution to enhance the probability of scoring. This procedure is commonly referred to as importance sampling.

Importance sampling may be accomplished by variance reduction techniques such as Russian-roulette, splitting, survival biasing, stratified sampling, weight cut-offs, exponential transform etc. The variance can also be reduced by using estimators or samplers such as the last-flight and the next-event estimators. The utilization of importance sampling requires the use of weight corrections so that the bias introduced by the sampling scheme is eliminated thereby preserving the fair game. However, some techniques such as the point-detector estimator introduce some bias that is not properly corrected by weight correction alone [8]. Importance sampling schemes in general will result in reliable (unbiased) estimates if a sufficiently large number of particles are sampled and provided of course that all sources of bias are corrected. It is also true that improper utilization of importance sampling techniques can result in a calculation that is less efficient.

A counter was introduced into the MORSE code that records the number of particles that have the value of their contributions within a given range or channel. Therefore, it is possible to know how many particles account for specific fractions of the total response. This counter is collapsed from 188 intervals to 10 percentage intervals which would indicate if a small number of particles are responsible for a large percentage of the total value of the

response. This provision turn out to be very useful in the analysis and identification of the undersampled condition because of its ability to isolate the contribution background.

Chapter 3

Modifications Introduced into the MORSE Code

Modifications were introduced into the MORSE code in order to calculate the statistics on a per particle basis according to equations 2.4 and 2.13. The original MORSE input was maintained and the output of the fractional standard deviations for the total responses calculated on a batch basis with Equation 2.12 was also retained. Another feature introduced was a table that shows in terms of percentage bins the distribution of all particle contributions according to their increasing values. This table is created from a 188 multichannel-type histogram as shown in Figure 3.1. This histogram is shown in a scale which enhances the importance of particles in the higher channels. Figure 3.2 shows this table in the output of the same batch that generated the histogram in Figure 3.1. Analyzing Detector 2 in Figure 3.2, 69700 particles account for the first 20% of the total response, 14634 particles account for the next 10% fraction of the response, and so on until the 5 particles of highest weight which account for the last 10% of the total response.

Besides the addition of the histogram mentioned above, this new version of the MORSE code also includes the output of the total responses and their standard deviations for each batch and for the accumulated estimates. The output also presents the estimates of the coefficient of variation and figure of merit, based on the accumulated statistics after each batch is completed.

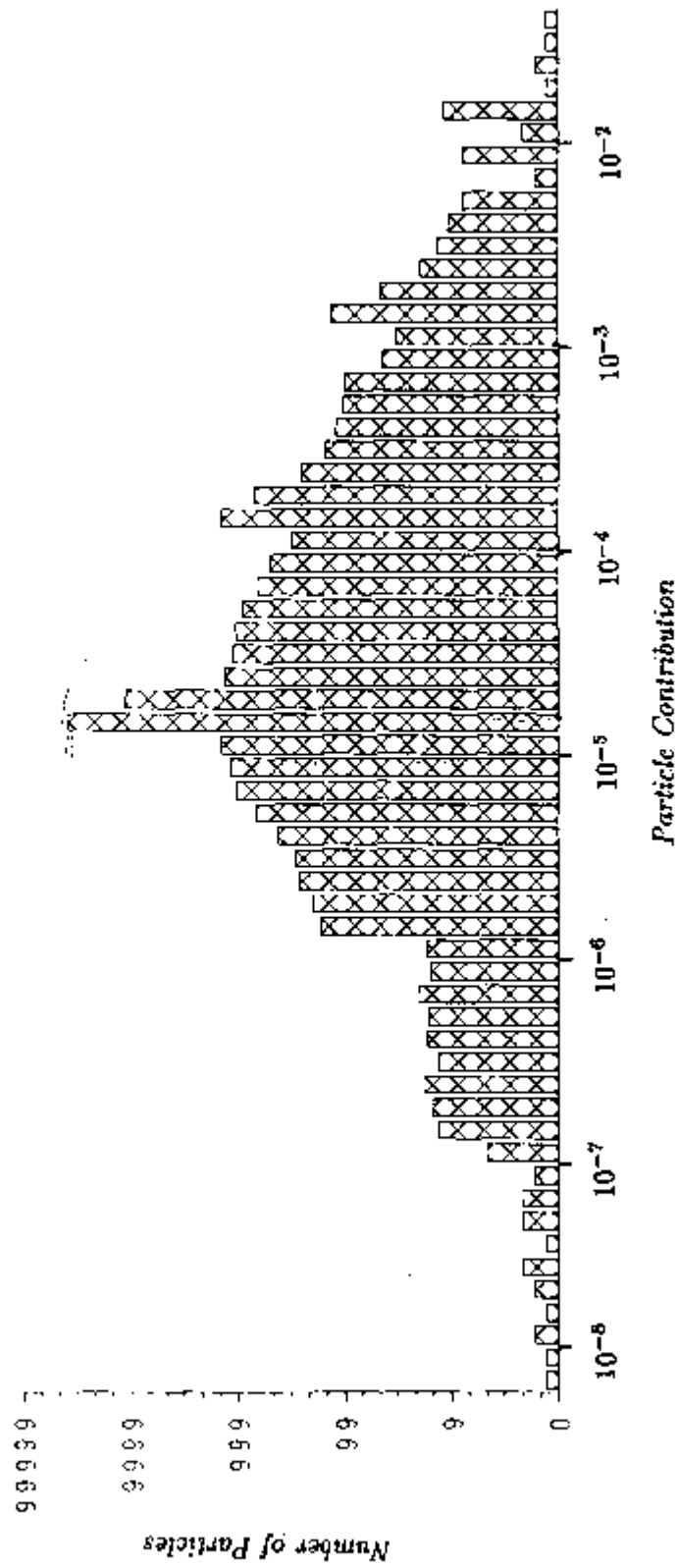


Figure 3.1: Particle Contribution Histogram for Detector 2 - Batch 1.

***START BATCH 1 RANDOM-13579BDFBR97

SOURCE DATA
 YOU ARE USING THE DEFAULT VERSION OF SOURCE WHICH SETS WATE TO DDP AND PROVIDES AN ENERGY IG.
 YOU ARE USING THE DEFAULT VERSION OF GTMED WHICH ASSURES GEOMETRY AND XSECT MEDIA ARE IDENTICAL.
 WTAVE IAVE UAVE VAWE YAVE XAVE YAVE ZAVE
 1.000E+05 1.00 -0.0022 -0.0005 0.0016 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CY(SD)	FCM
	BATCH RESPONSE	FSD	ACCUMULATED RESPONSE	FSD			
1	3.8195D-04	0.02420	3.8195D-04	0.02420	0.18380	0.18380	9.6140D+01
2	4.0657D-05	0.03220	4.0657D-05	0.03220	0.17042	0.17042	5.4278D+01
3	1.0318D-05	0.18977	1.0318D-05	0.18977	0.45750	0.45750	1.5631D+00
4	2.2010D-06	0.10484	2.2010D-06	0.10484	0.24872	0.24872	5.1215D+00
5	5.8018D-07	0.16399	5.8018D-07	0.16399	0.24418	0.24418	2.0933D+00
6	1.3670D-07	0.13992	1.3670D-07	0.13992	0.20058	0.20058	2.8754D+00
7	1.0456D-07	0.65115	1.0456D-07	0.65115	0.49116	0.49116	1.3276D-01
8	3.6075D-08	0.39992	3.6075D-08	0.39992	0.31527	0.31527	3.5196D-01
9	4.4715D-09	0.26794	4.4715D-09	0.26794	0.26414	0.26414	6.7894D-01
10	8.1909D-10	0.22073	8.1909D-10	0.22073	0.24052	0.24052	1.1553D+00

DETECTOR	PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS										
	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	82140	0	0	0	6767	7358	717	735	251	49	
2	63700	0	14634	7215	3000	1316	971	68	103	5	
3	78956	13447	1962	1753	289	144	23	13	1	0	
4	81208	12320	2213	405	198	43	21	6	5	0	
5	90177	4818	1100	165	76	18	7	3	1	1	
6	88529	6763	885	246	37	34	2	4	2	0	
7	96335	288	15	3	1	0	0	0	0	0	
8	96700	30	0	1	1	1	0	0	0	0	
9	96124	619	63	10	0	1	2	0	0	0	
10	96140	703	86	21	0	3	2	0	1	0	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY GAMLOST
 100000 0 0 0 188986 0 98169 48 99952 0 0 0 0 0 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 45 SECONDS.

Figure 3.2: Present MORSE Output after a Batch is Completed.

LOCSD		
1	SD	Standard MORSE per batch statistics
2	SSD	
3	SSD2	
4	SD	New MORSE per particle batch statistics
5	SSD	
6	SSD2	
7	SSD	Accumulated statistics
8	SSD2	
9	SSD	Working area
10	SSD2	
11	SSD3	Statistics used in the calculation of the kurtosis
12	SSD4	
13	SSD5	
14	SSD6	
LOCQE	15	SUD and SSD units

Figure 3.3: Layout of the New Storage Areas in the Blank Common.

To perform the necessary additional bookkeeping the *user* part of the *blank common* was separated, augmented, and put in double precision (COMMON /SSS/). The particle bank now can accept only one source particle and any number of secondaries particles (NMOST). Therefore, the memory requirements are substantially reduced and the utilization of double precision arithmetic was required to work with numbers of particles on the order of several millions. Figure 3.3 shows the lay out of the new storage areas.

In Appendix C, a listing of all added and modified subroutines is included. All major characteristics of these subroutines are presented in the following list:

1. FLUXST - modified to perform additional bookkeeping in COMMON /SSS/.
2. FTEST - calculates the F values.
3. GSTORE - modified to include only one source particle in the particle bank and at most (NMOST) secondary particles.
4. INPUT1 - minor modification in the input format of CARD B.

5. MAIN - modified to include COMMON /SSS/.
6. MORSE - modified to perform additional calculations for the per particle analysis.
7. MSOUR - modified to help the interim batch information output.
8. NBATCH - now performs only the total response in the per batch method.
9. NPART - called at the end of each history to do the sums needed in the per particle analysis.
10. NRNPRI - perform all calculations in the per particle basis and outputs the new batch information.
11. NRUN - modified to output the differential responses in the per particle basis.
12. OUTPT - modified to accomplish the interim batch information output.
13. RELCOL - this subroutine was modified according to Appendix B and it is shown only because of this purpose.
14. SCORIN - modified to create the new bookkeeping area in COMMON /SSS/.
15. STBTCH - now performs only the zeroing of the per batch bookkeeping areas.
16. STPART - provides the zeroing of the proper bookkeeping areas of the per particle analysis.
17. TESTW - modified in order to handle the the new allocation of secondary particles.
18. VAR2 - modified to include the per particle estimate of the *FSD*.
19. VAR3 - modified to perform only estimates of the *FSD* in the per particle basis.
20. VAR4 - provides the estimates of the *FSD* and of the *CV(SD)*.

Chapter 4

Analysis of Results

At the beginning of this work it was necessary to identify a problem which has a solution with an underestimated mean and a small standard deviation. The search for such a problem yielded what became the main objective of this work — which was to provide the user with more information, and thereby to better understand the behavior of the solution and the associated sampling distribution. This information will be the key for a successful calculation.

Because of the extensive amounts of output generated, the solutions to most of the sample problems were put in Appendix A. The reader can more easily refer to these data for more refined comparisons.

4.1 Sample Problem 1

Sample problem 1 consists of a 1-meter radius concrete sphere with 10 detectors positioned at 10-cm intervals from the center of the sphere. An isotropic monoenergetic (14-Mev) neutron point source is located at the center of the sphere. All responses are for the first group only. Table 4.1 shows the group structure for the cross sections.

This problem offers several degrees of difficulty for the effects of interest calculated. For example, the response of Detector 1 is very easy to calculate as compared with that of Detector 10. Also, the utilization of point detectors makes the flux estimation of Detector 10 very difficult to accomplish because of the three-dimensional nature of point detectors.

Table 4.1: Energy Structure for Sample Problem 1.

Group	Upper Energy	Group	Upper Energy	Group	Upper Energy
1	1.50E+07	2	1.22E+07	3	1.00E+07
4	8.18E+06	5	6.36E+06	6	4.96E+06
7	4.06E+06	8	3.01E+06	9	2.46E+06
10	2.35E+06	11	1.83E+06	12	1.11E+06
13	5.50E+05	14	1.11E+05	15	3.35E+03
16	5.83E+02	17	1.01E+02	18	2.90E+01
19	1.07E+01	20	3.06E+00	21	1.12E+00
22	4.14E-01				

4.1.1 Next-Event Surface Crossing Estimator Solution

The utilization of a next-event surface crossing estimator (NESXE) posed no problems in the solution of sample problem 1. Figures 4.1, 4.2, and 4.3 show the evolution of the flux, FSD , and FOM with increasing number of particles for detectors 2, 6, and 10 respectively. It is useful to observe the asymptotic behavior of these statistics over a wide range of sample sizes. In this problem the solutions are free from undersampling because it was possible to process a sufficient number of particles and the statistical quality of these solutions are described by the central limit theorem. There is no reason to question the statistics calculated in this problem. Even FSD 's much higher than 0.5 are likely to yield fluxes within 3σ of the expected values most of the time.

An important fact suggested from Figure 4.1 and from the data in Appendix A.1.1 is that the coefficient of variation of the standard deviation $CV(SD)$ generally follows but is almost always higher than the standard deviation. Also, the amount by which the $CV(SD)$ changes is often much more peaked than that experienced by the standard deviation because of the changes in the kurtosis of the distribution. An increase in the $CV(SD)$ may reflect either a small increase or even a decrease in the standard deviation. Another interesting aspect of these results is that the FOM accepts the solution of Detector 10 much earlier than the solution of Detector 2 which indicates that this parameter may cause the rejection of perfectly acceptable solutions.

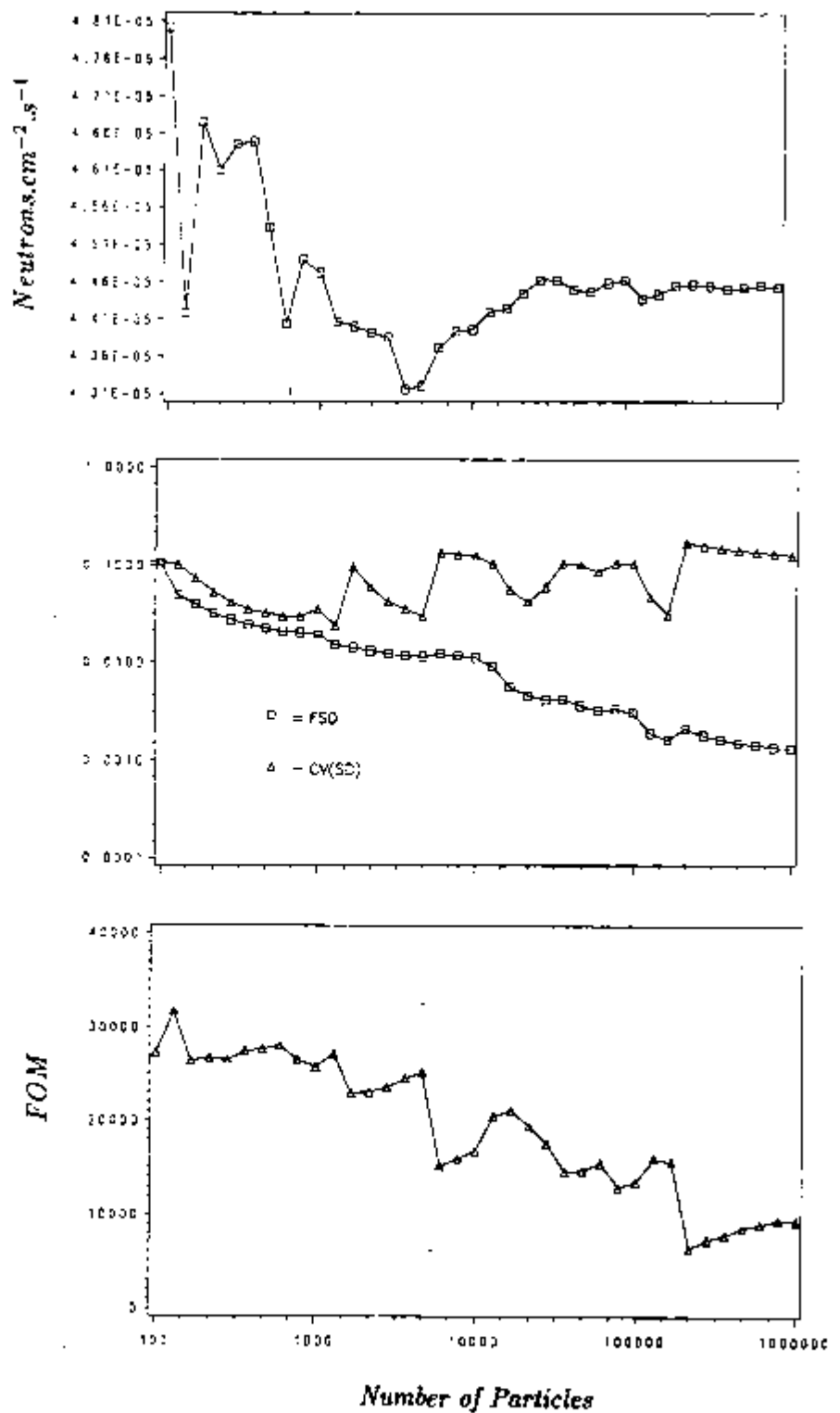


Figure 4.1: Neutron Flux, *FSD*, *CV(SD)*, and *FOM* Behavior for Detector 2 - NESXF.

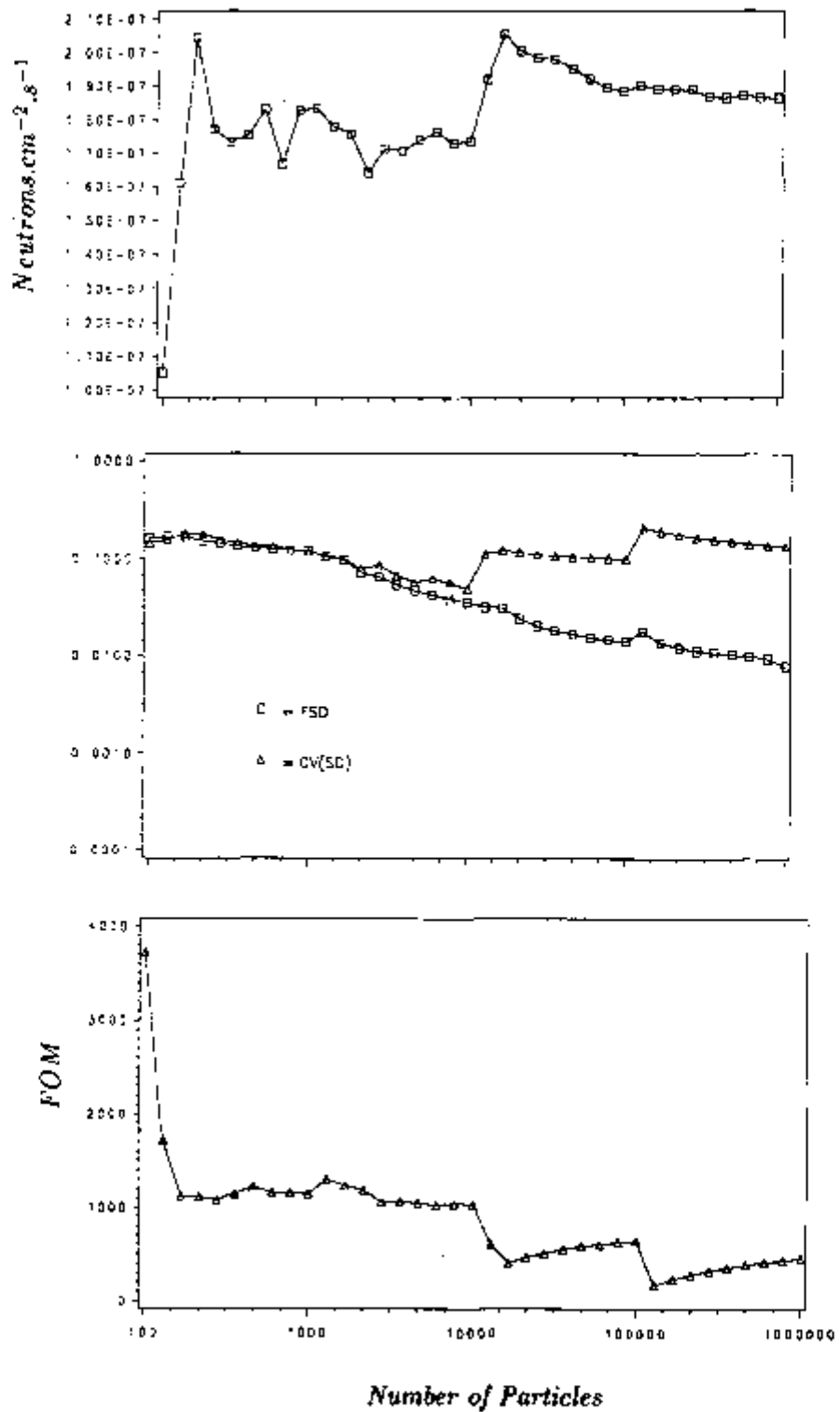


Figure 4.2: Neutron Flux, *FSD*, *CV(SD)*, and *FOM* Behavior for Detector 6 – NESXE.

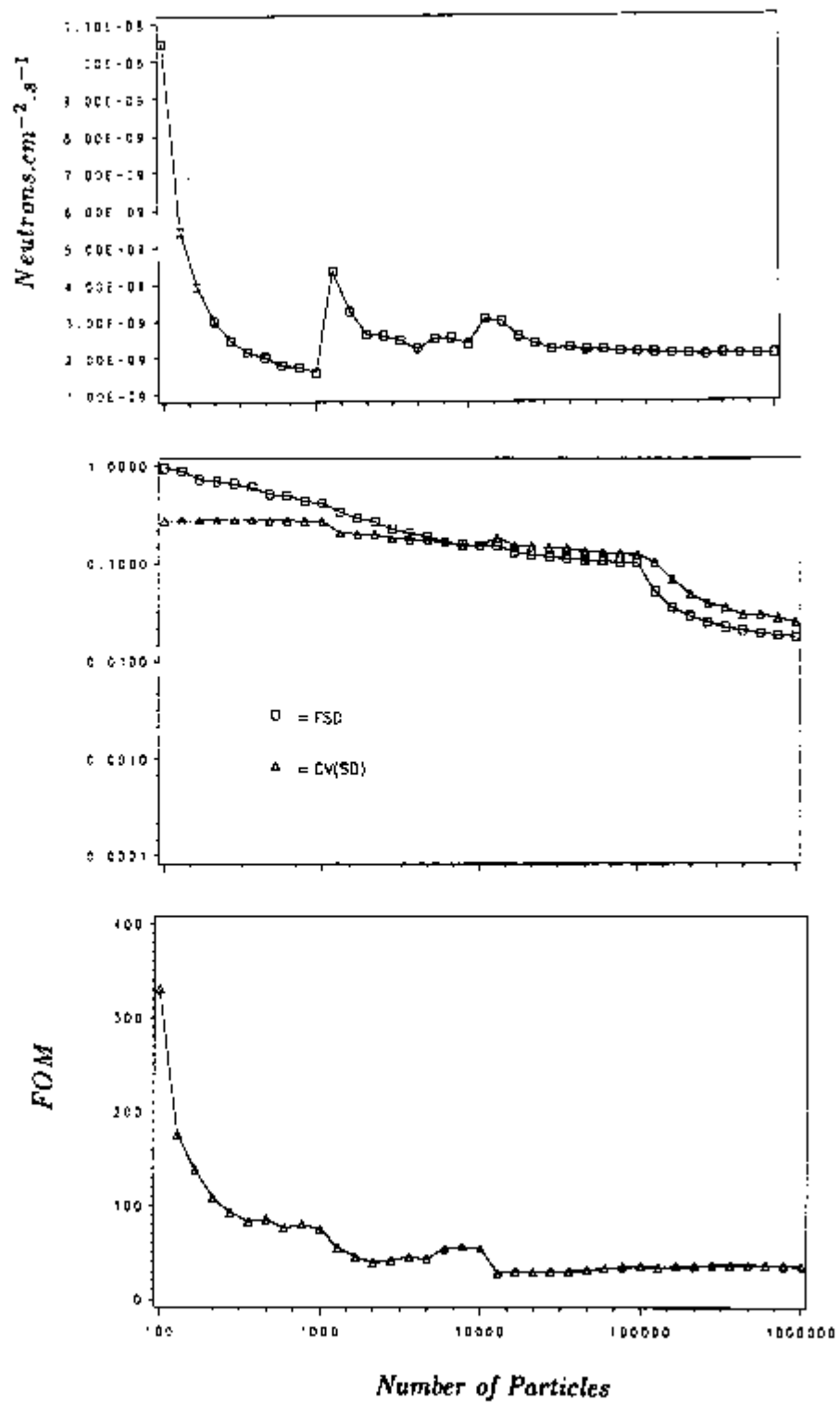


Figure 4.3: Neutron Flux, *FSD*, *CV(SD)*, and *FOM* Behavior for Detector 10 – NESXE.

Table 4.2 shows the results for three phases of the calculation. The three phases consisted of 10 batches each with 10^3 , 10^4 , and 10^5 particles per batch respectively. The F tests present some high values that indicate major differences between the group means. For example, the F value is 1.99945 for Detector 6 in the range of 10^4 to 10^5 particles. It is possible to see in Figure 4.2 that effectively there are large differences between the group means. However, it should be noted that the solution has converged to the true solution and the standard deviation is also sufficiently small. In the case of Detector 7 in the range of 10^5 to 10^6 particles the standard deviation is definitely small enough to guarantee the results — which means that this parameter can also reject perfectly acceptable solutions.

4.1.2 Point-Detector Estimator Solution

The utilization of point-detector estimators (PDE) significantly increases the degree of difficulty in the solution of this problem. In fact, the effects of undersampling can be easily seen when the point detector solutions are compared with the solutions described in Section 4.1.1.

Figures 4.4, 4.5, and 4.6 show the behavior of the neutron flux, FSD and $CV(SD)$, and the figure of merit with increasing values for the sample size for detectors 2, 6, and 10 respectively. In the case of Detector 2 the undersampling condition yielded underestimation for sample sizes up to 200,000 particles and for Detector 6 for sample sizes in the range of 2,000 to 500,000 particles. For both detectors the FOM exhibits stable plateaus in the undersampled region. In the case of Detector 10, the simulation is so undersampled that is possible to see the peaks in Figure 4.6 which are caused by contributions from individual particles. It is interesting to note from Appendix A.1.2 that the particle contribution distribution for Detector 6 contained more particles in the higher channels in batch 5 than in batch 10. This is an effect of the sampling of a few important particles that shifted the distribution and minimized the undersampling condition.

Table 4.2: F Values for Sample Problem 1 with Next-Event Estimator.

Number of Particles	Detector	Total Response	FSD Batch	FSD Accum.	F Value
$10^3 - 10^4$	1	3.9502D-04	0.01518	0.02069	0.53761
	2	4.3966D-05	0.01400	0.01480	0.89466
	3	8.6957D-06	0.01311	0.02216	0.34984
	4	2.0963D-06	0.03622	0.03055	1.40545
	5	6.2572D-07	0.02918	0.05013	0.33860
	6	1.7343D-07	0.04160	0.05967	0.48560
	7	5.7541D-08	0.11905	0.09939	1.43532
	8	2.0712D-08	0.12643	0.13236	0.91234
	9	8.9238D-09	0.26682	0.23243	1.31807
	10	2.3464D-09	0.27192	0.25963	1.09688
$10^4 - 10^5$	1	3.8398D-04	0.00394	0.00327	1.45084
	2	4.4619D-05	0.00422	0.00526	0.64334
	3	8.9053D-06	0.00626	0.00679	0.84945
	4	2.2075D-06	0.01124	0.01134	0.98125
	5	6.2544D-07	0.00921	0.01497	0.37831
	6	1.8826D-07	0.03401	0.02405	1.99945
	7	6.0974D-08	0.02165	0.03847	0.31681
	8	2.0435D-08	0.04259	0.04535	0.88189
	9	6.3437D-09	0.05786	0.06413	0.81423
	10	2.1429D-09	0.11009	0.10191	1.16697
$10^5 - 10^6$	1	3.8319D-04	0.00079	0.00122	0.42173
	2	4.4523D-05	0.00168	0.00200	0.69934
	3	8.9761D-06	0.00289	0.00343	0.70744
	4	2.2398D-06	0.00626	0.00637	0.96701
	5	6.2468D-07	0.00535	0.00572	0.87482
	6	1.8613D-07	0.00883	0.00907	0.94718
	7	5.8928D-08	0.01453	0.01125	1.66750
	8	1.9024D-08	0.01464	0.01860	0.62002
	9	6.0442D-09	0.01903	0.02137	0.79305
	10	2.0664D-09	0.02113	0.03236	0.42638

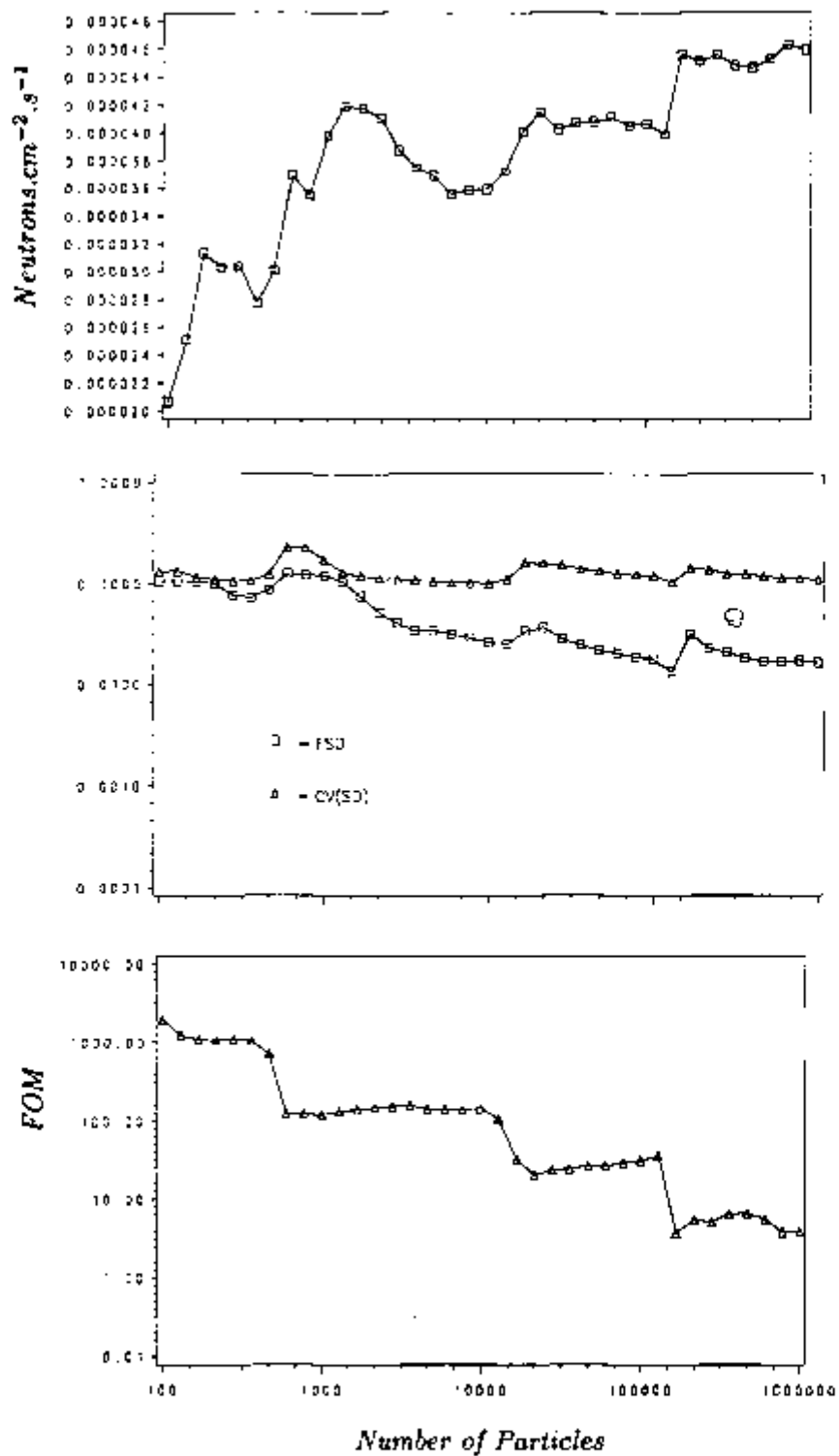


Figure 4.4: Neutron Flux, FSD , $CV(SD)$, and FOM Behavior for Detector 2 – PDE.

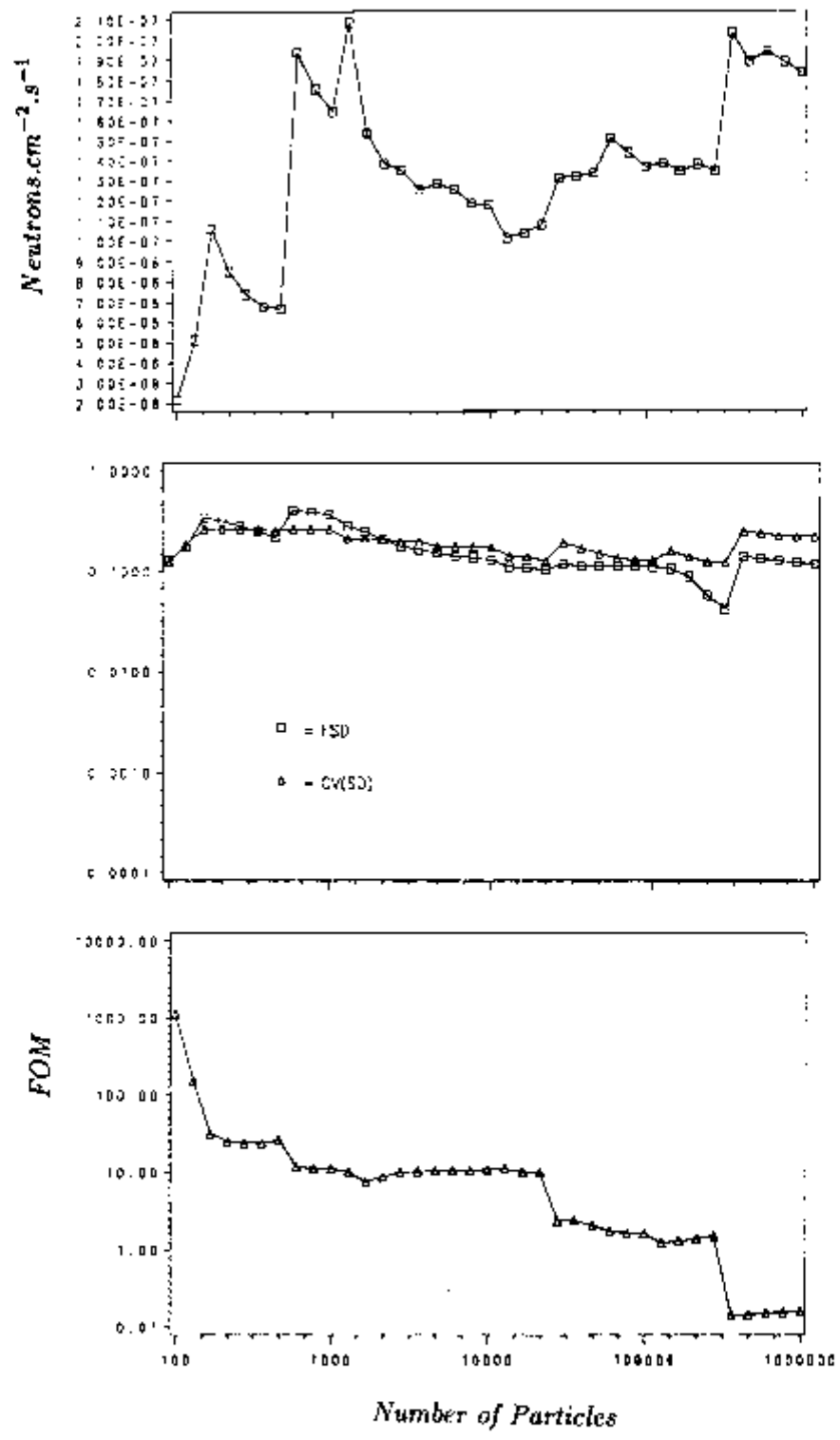


Figure 4.5: Neutron Flux, FSD , $CV(SD)$, and FOM Behavior for Detector 6 - PDE.

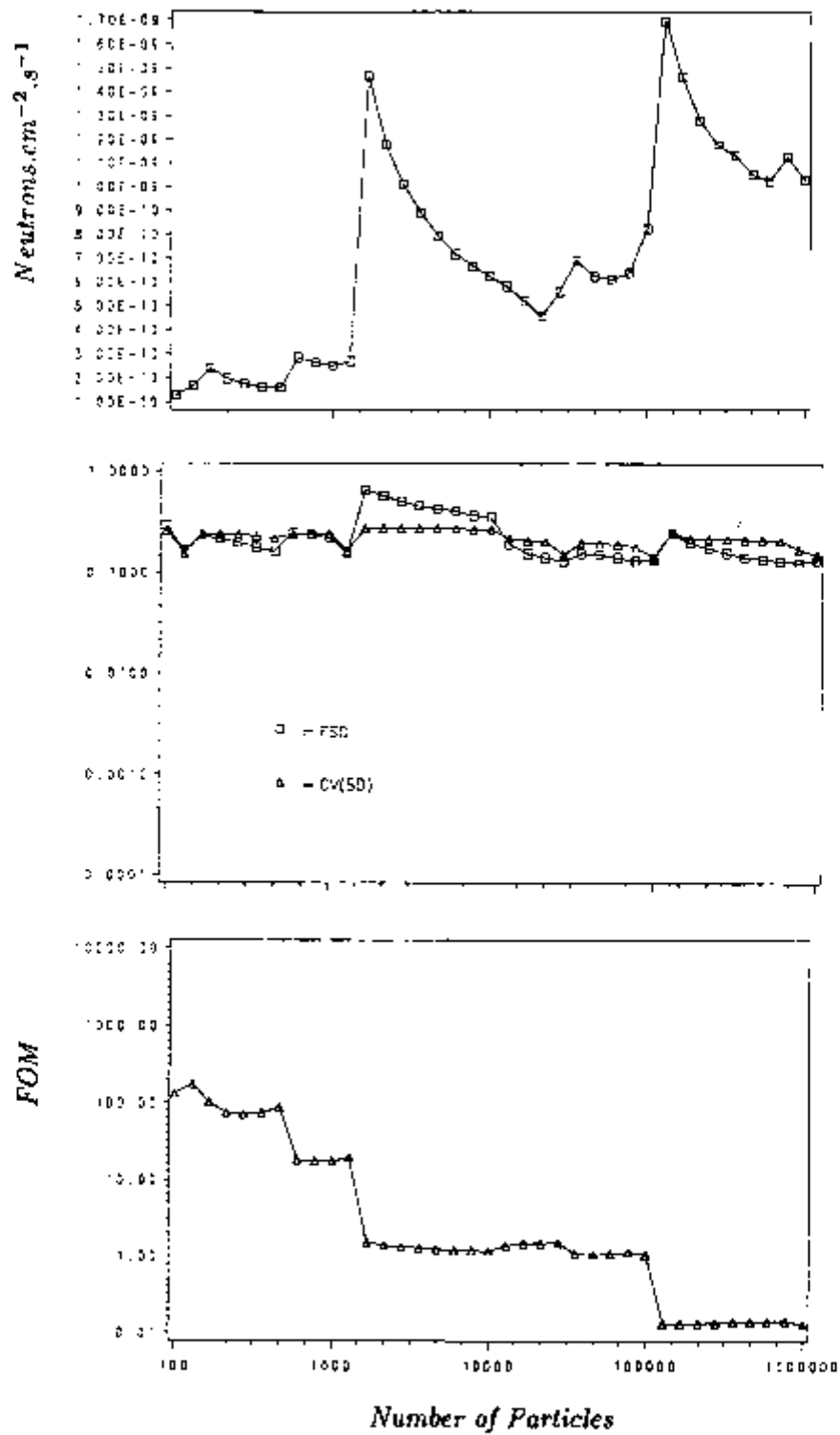


Figure 4.6: Neutron Flux, FSD , $CV(SD)$, and FOM Behavior for Detector 10 - PDE.

Appendix A.1.2 shows the output for 10 batches of 10^5 particles each. For the first batch, detectors 1 and 2 are clearly acceptable solutions on the basis of the behaviors of their standard deviations alone. Detectors 3 and 4 present peaks in their standard deviation and $CV(SD)$ and are very close to the true solutions¹ although they exhibit somewhat large standard deviations. The distribution of particle contributions for all detectors beyond Detector 2, shows that the number of particles accounting for large fractions of the solutions is becoming too small.

In Batch 4, the peaks in the standard deviation and $CV(SD)$ shifted to Detector 5. The distribution of particle contributions for this detector shows a relatively small number of particles accounting for a large fraction of the response which usually characterizes the undersampling condition. Finally, in Batch 10 the peak shifted to Detector 6 — again, a relatively small number of particles account for a large fraction of the response.

Based on these results and the discussion above, the solutions for detectors 1, 2, 3, 4 and 5 can be considered reliable. Detector 6 represents the beginning of what will be called the *breakdown region*, which is associated with a sample size that provides either only a few or no important rare event making the standard deviations — which can be very small — experience large increases. Obviously, all detectors beyond this point will be undersampled unless additional particles are processed. It is interesting to observe the behavior of the solution at Detector 7 which initially overestimates the true solution because of a highly contributing particle that was sampled early in the calculation.

An important fact, as seen in Appendix A.1.2, is that the particle contribution histogram always included a small number of particles which accounted for large fractions of the solutions for the undersampled detectors. Therefore, the histogram is able to detect the undersampling condition for both the breakdown region and the region of severe undersampling. In this problem, the explanation for this behavior is that even in the severe undersampling condition, there are some particles that make contributions only large

¹True solutions are considered the solutions obtained in Section 4.1.1 with 10^6 particles.

enough to make them stand out from the background contributions, and as the sample size increases these contributions will eventually move to the intermediary channels.

Figure 4.7 shows a three-dimensional view of the standard deviation and of the coefficient of variation of the standard deviation. It can be seen that the plot of the coefficient of variation is much more structured than that of the standard deviation providing a qualitative rather than quantitative indicator of the behavior of the solution.

Figure 4.8 shows the same calculation as in Figure 4.7 but with the last random number of that calculation used as the initial one in this calculation. A *FSD* comparison shows good agreement up to Detector 6 and a *CV(SD)* comparison shows good agreement only up to Detector 3 which demonstrates that this indicator is too sensitive to be taken as a quantitative measure of precision. Also, from figures 4.7 and 4.8, it can be assumed that Detector 10 represents the end of the breakdown region or the beginning of the region of severe undersampling. Figure 4.9 shows the calculations using the exponential transform technique with $PATH = 0.5$ and Figure 4.10 shows the results using source angular biasing, Russian roulette, splitting, and exponential transform. It is possible to see that the variance reduction techniques significantly reduce the variability of *CV(SD)* making it less structured. Because this behavior may indicate the effectiveness of a given variance reduction technique and also that the sampling distribution has become sufficiently stable, it was concluded that the use of this coefficient needs further study.

Table 4.3 shows the calculated *F* values after 10 batches are completed. The two values that flag greater differences in the batch means are for Detector 2 and Detector 6. These results illustrate the weakness of the test in discerning acceptable from unacceptable solutions. The test detected that there are significant differences in the group means of Detector 6. Therefore, the results should be checked with other indicators to determine if they are acceptable. Otherwise it is necessary to increase the batch size.

In the case of Detector 2 the explanation can be based on the fact that although it is unlikely, there are values in the tails of the normal distribution. And the null hypothesis

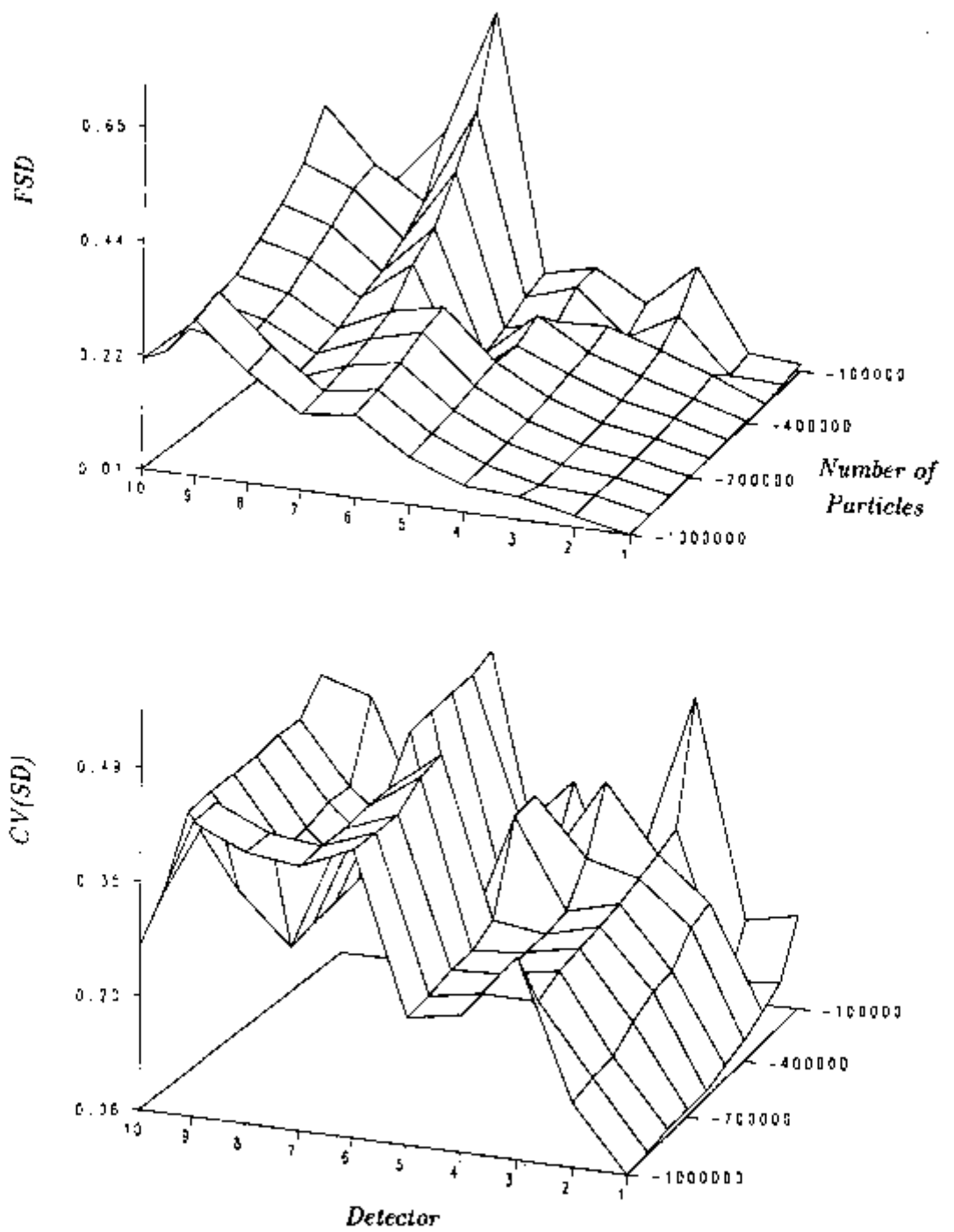


Figure 4.7: Three-Dimensional Behavior of FSD and $CV(SD)$ for Sample Problem 1 - PDE.

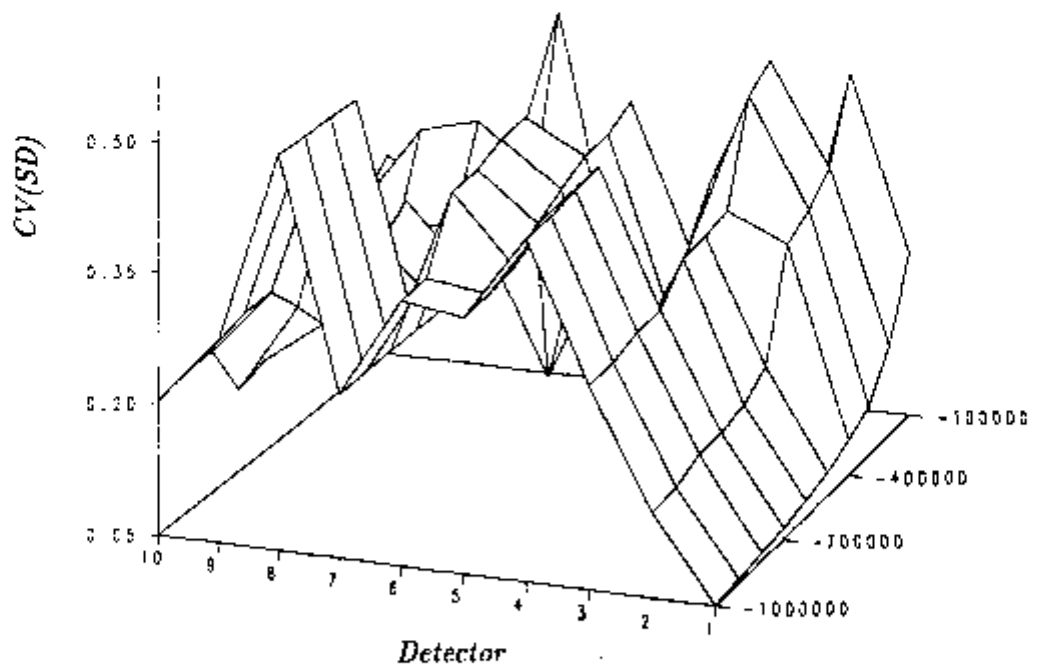
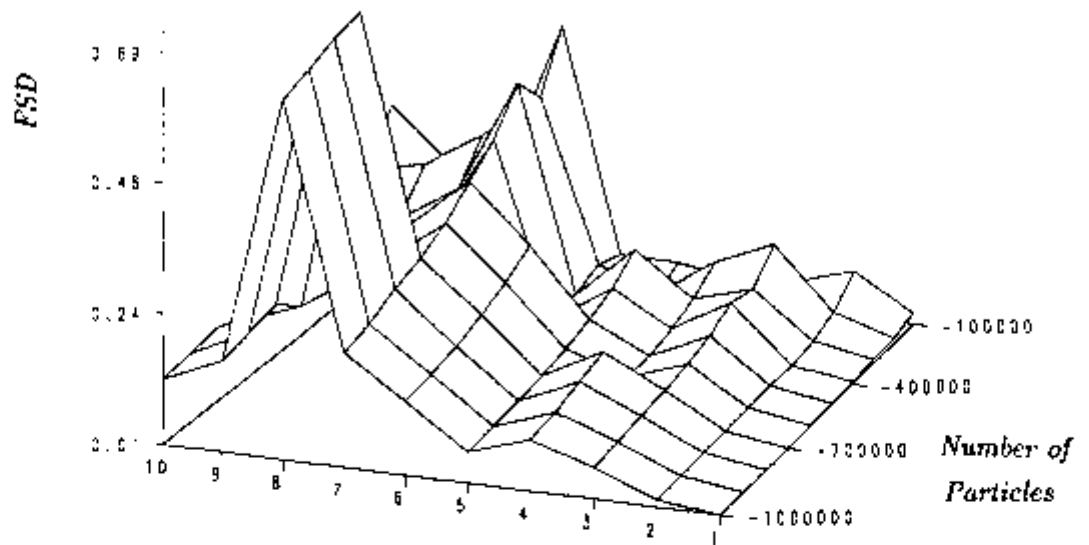


Figure 4.8: Behavior of FSD and $CV(SD)$ for Sample Problem 1 -- PDE with New Starting Random Number.

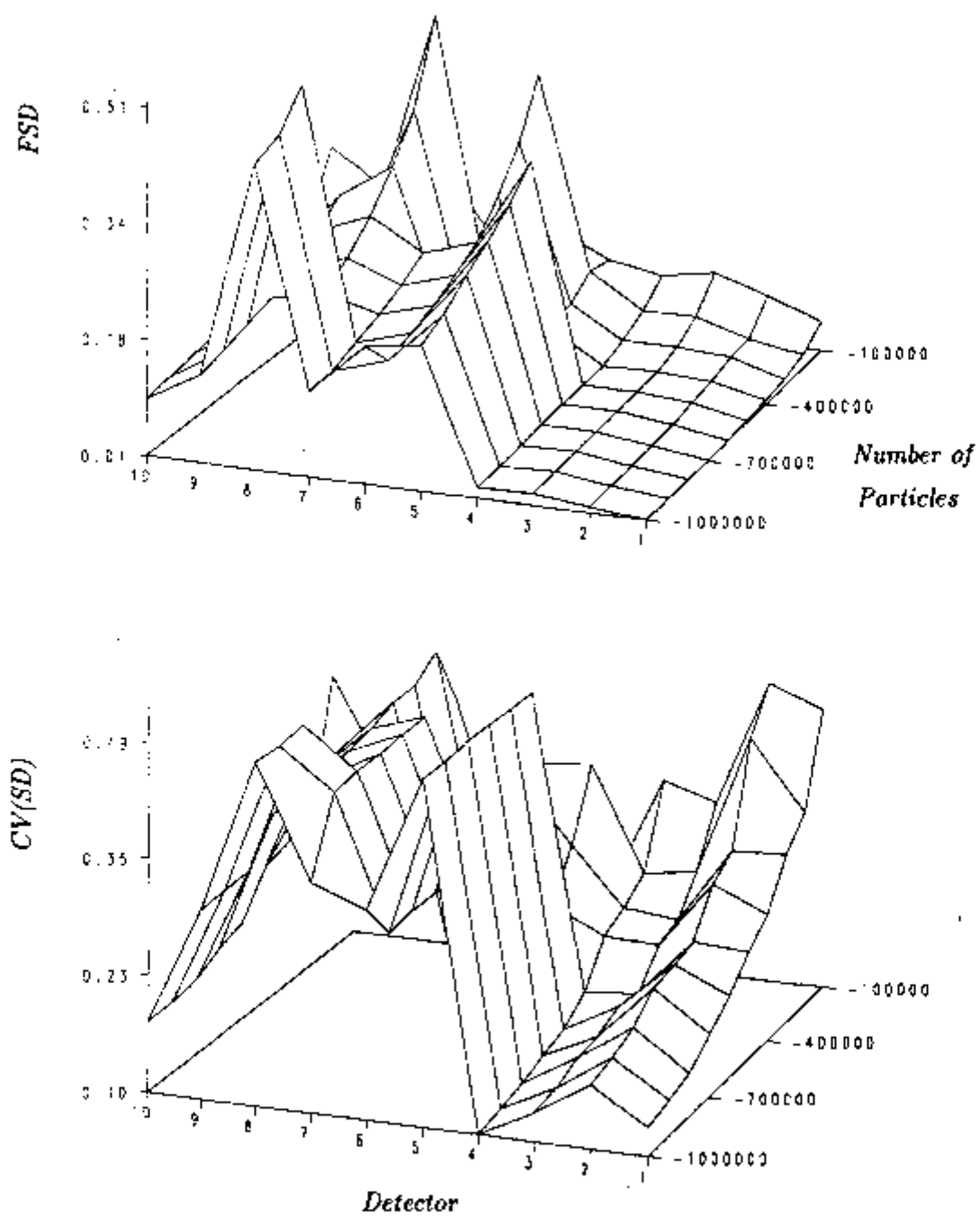


Figure 4.9: Behavior of FSD and $CV(SD)$ for Sample Problem 1 - with $PATH = 0.5$.

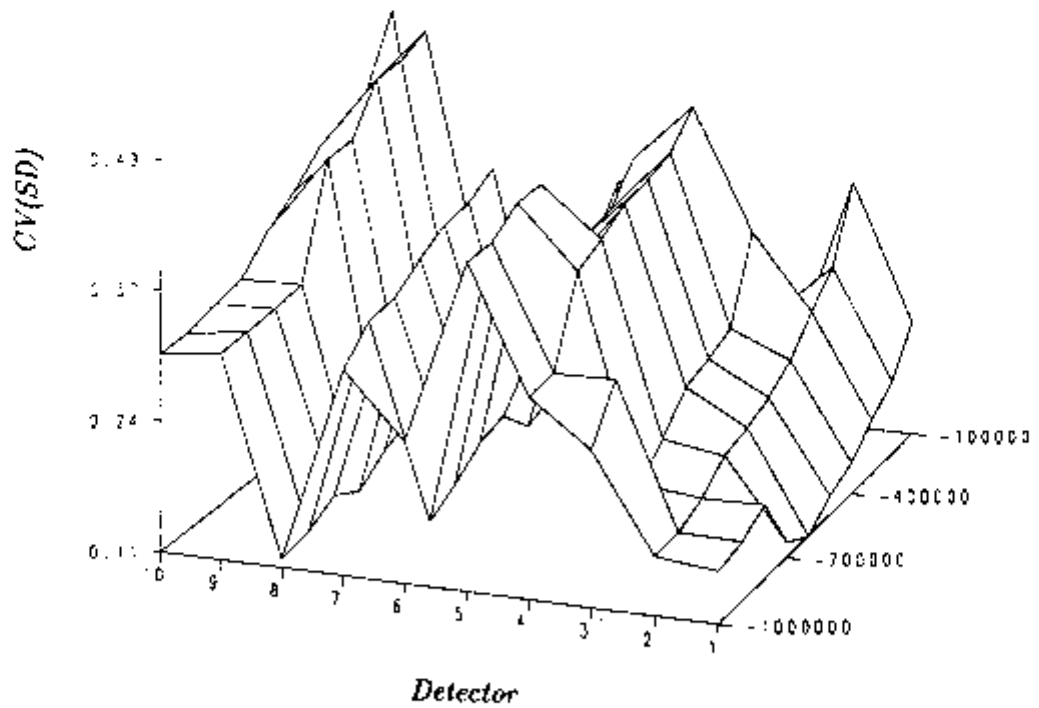
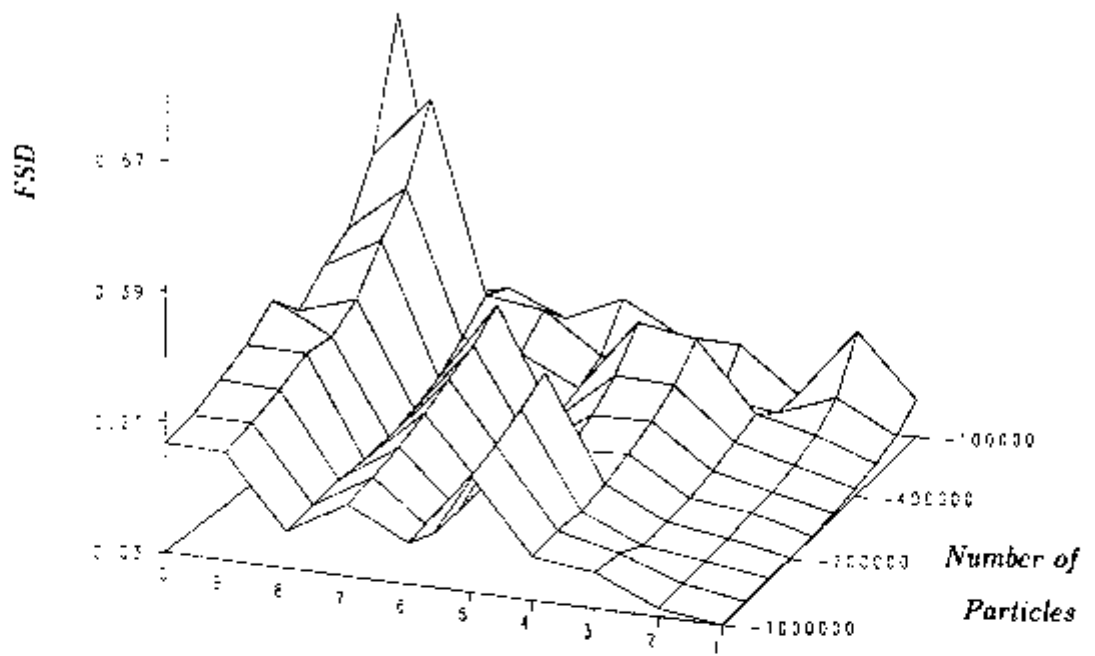


Figure 4.10: Behavior of FSD and $CV(SD)$ for Sample Problem 1 – using Russian Roulette, Splitting, and $PATH = 0.5$.

Table 4.3: F Values for Sample Problem 1 with Point-Detector Estimator.

Number of Particles	Detector	Total Response	FSD Batch	FSD Accum.	F Value
$10^3 - 10^4$	1	3.5122D-04	0.02451	0.03081	0.63240
	2	3.5908D-05	0.05013	0.04783	1.09872
	3	1.4941D-05	0.30124	0.30203	0.99466
	4	3.4210D-06	0.38488	0.39837	0.93329
	5	1.0802D-06	0.56001	0.57999	0.93216
	6	1.1766D-07	0.16116	0.20402	0.62366
	7	3.4278D-08	0.34404	0.38522	0.79743
	8	1.5081D-08	0.68582	0.69850	0.96390
	9	2.6313D-09	0.59333	0.60736	0.95422
	10	6.2342D-10	0.57851	0.59306	0.95140
$10^4 - 10^5$	1	3.8195D-04	0.01798	0.02420	0.55218
	2	4.0657D-05	0.03121	0.03220	0.93898
	3	1.0318D-05	0.19179	0.18977	1.02138
	4	2.2010D-06	0.12374	0.10484	1.39315
	5	5.8018D-07	0.16108	0.16399	0.96486
	6	1.3670D-07	0.14838	0.13992	1.12463
	7	1.0456D-07	0.71689	0.65115	1.21213
	8	3.6075D-08	0.48367	0.39992	1.46273
	9	4.4715D-09	0.30049	0.28794	1.08911
	10	8.1909D-10	0.26011	0.22073	1.38867
$10^5 - 10^6$	1	3.9006D-04	0.00957	0.00912	1.10126
	2	4.5916D-05	0.04192	0.02979	1.97938
	3	9.0757D-06	0.04628	0.05148	0.80815
	4	2.1204D-06	0.05785	0.05826	0.98588
	5	7.0483D-07	0.09354	0.09736	0.92293
	6	1.8347D-07	0.22707	0.16347	1.92943
	7	5.0838D-08	0.16119	0.15096	1.14010
	8	1.7408D-08	0.20189	0.21587	0.87468
	9	5.5855D-09	0.26034	0.29830	0.76171
	10	1.0233D-09	0.22022	0.21594	1.04000

actually claims a uniform distribution for the group means. For the last four detectors which are undersampled and exhibit some underestimation, the test fails to show any differences between the means because in the undersampling regime the group means are likely to be very close to each other. As the sample size increases and some heavy contributing particles are sampled larger differences in the group means are observed. Also, the application of F tests as mentioned in Chapter 2 requires that the sampling distribution should be normally distributed. If the kurtosis is too high the tests will tend to be too small [6] and the hypothesis of equality of the means can not be tested.

4.2 Sample Problem 2

This problem belongs to a set of sample problems that comes with the MORSE code package. It comprises of a point fission source in air and uses a surface crossing estimator in the analysis. Appendix A.2 shows the output for the problem using variance reduction techniques with the same parameters as in the MORSE manual. It is interesting to note that most of the $CV(SD)$ values are well within commonly acceptable values. Also, the distribution of particle contributions exhibits a more uniform dispersion of particles in the percentage bins.

Figure 4.11 shows the behavior of both FSD and $CV(SD)$. This figure also show that although the kurtosis of the distribution eventually becomes constant, that happens long after an acceptable solution has been achieved.

4.3 Sample Problem 3

This problem was solved to demonstrate the behavior of the solutions in a more complex geometry. The configuration consists of a concrete cylinder of 150.2-cm height and a 150.0-cm radius with a cylindrical duct of 7.62-cm radius placed along the main axis. A 14-Mev neutron source is positioned along the bottom side of the cylinder and emits neutrons with

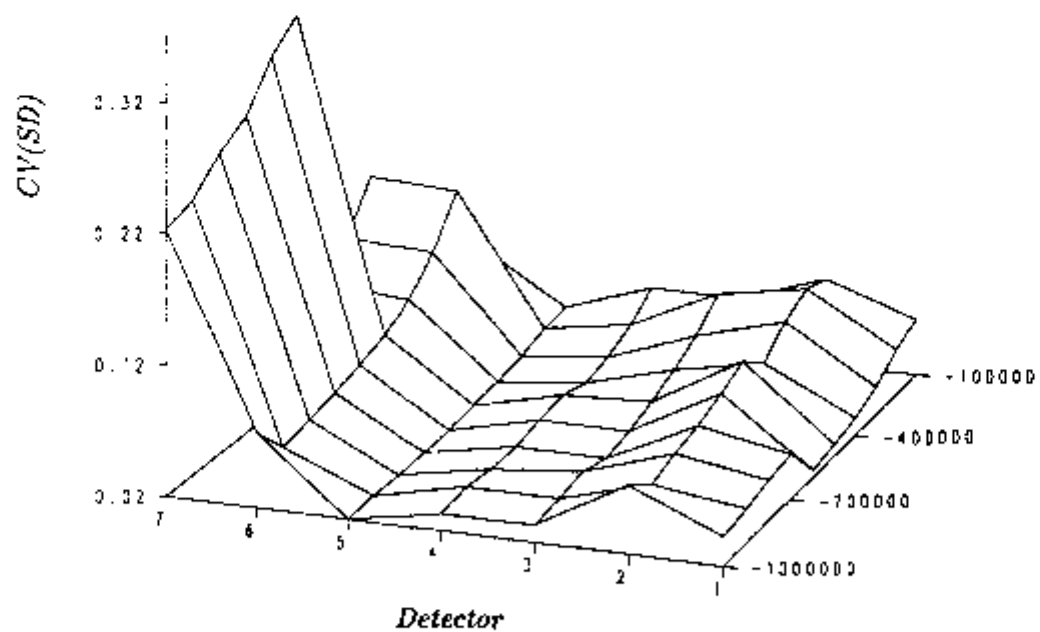
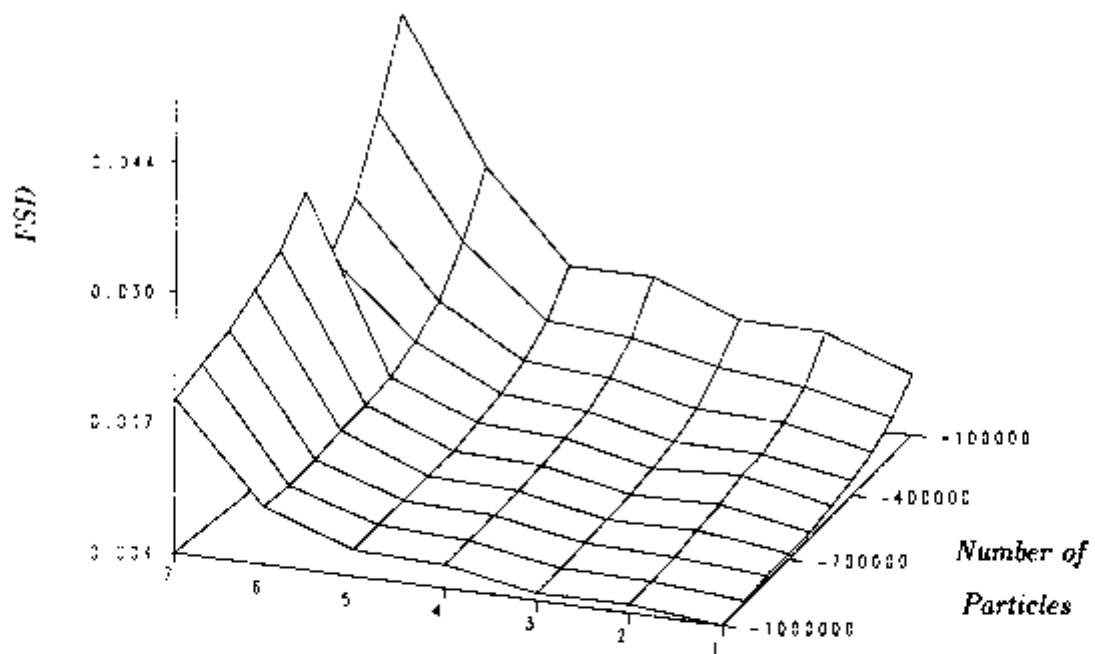


Figure 4.11: Three-Dimensional Behavior of FSD and $CV(SD)$ for Sample Problem 2.

directions uniformly distributed in the hemisphere facing the cylinder. Also, only the top fourteen groups are analyzed.

Because of the characteristics of the problem, source biasing provides large variance reductions which is accomplished using a step importance function for the position of emission which samples particles within a 10-cm radius 1000 times more often than outside this radius.

Appendix A.3.1 shows the data without source biasing and Appendix A.3.2 with source biasing. The effect of the source biasing is to decrease the size of the background contributions. It is interesting to see the behavior of the *FOM* in this problem. Figure 4.12 shows that although the step biasing procedure increased the efficiency of the calculation, the figure of merit of the problem without step biasing has a much more constant structure.

Figure 4.12 also shows that an increase in efficiency in the calculation may not reflect a smaller $CV(SD)$ which again presents very little information about the behavior of the solution.

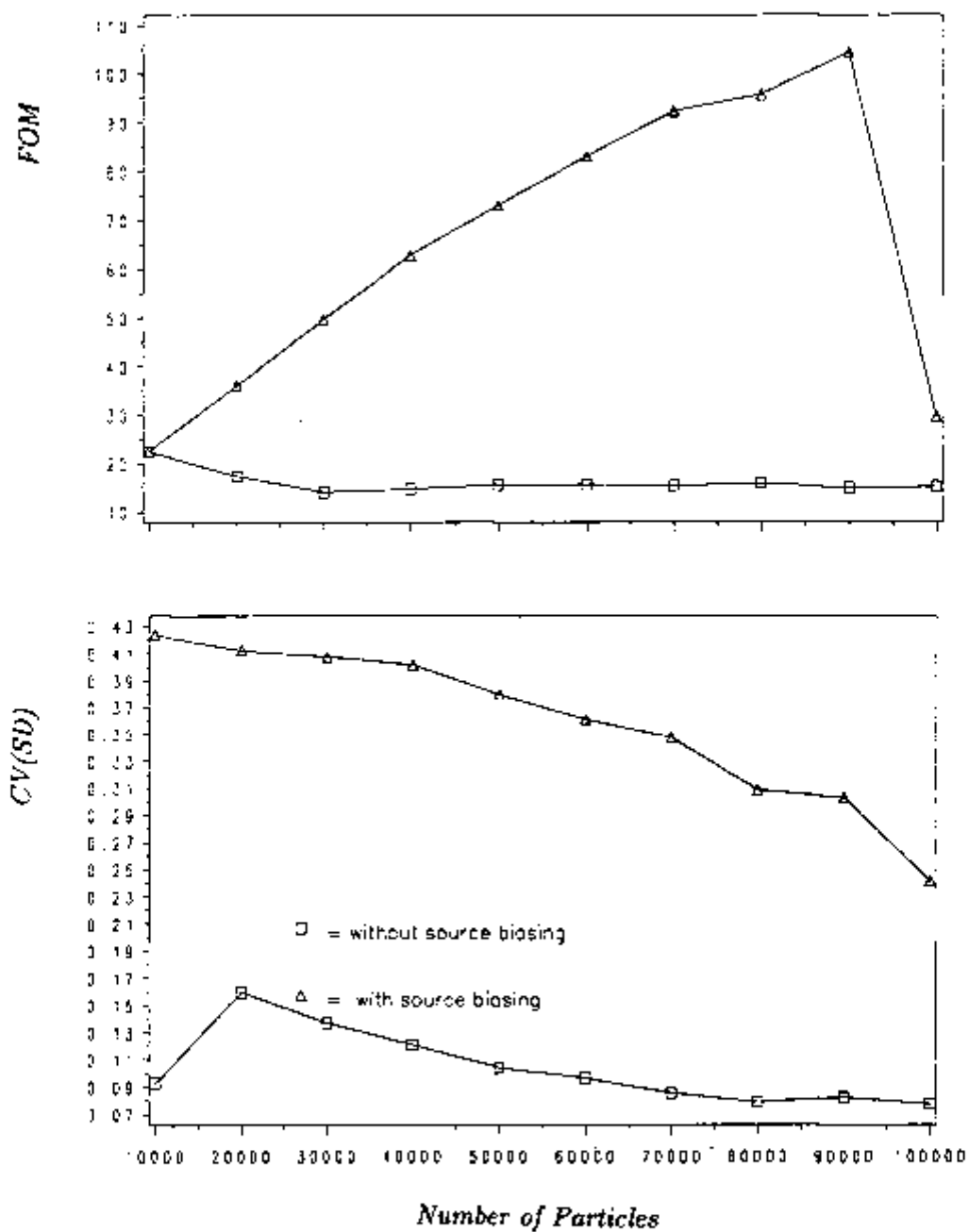


Figure 4.12: *FOM* and *CV(SD)* Behavior for Sample Problem 3.

Chapter 5

Conclusions

In this work several potential techniques to detect undersampling conditions were investigated.

The utilization of F tests failed to be conclusive because the contributions were not normally distributed. However, as a recommendation for future work, it could be used if the samples were drawn from a population of group means which have a more normal distribution. Also, problems that can be solved with a purely analog Monte Carlo calculation would have binomial distribution of the scores. In this case, F tests could be applied for other purposes rather than to detect undersampling conditions since this condition rarely occurs in such problems. For the reasons explained above, the utilization of F tests is not recommended without more study.

The calculation of the coefficient of variation of the standard deviation which provides confidence limits for the standard deviation estimate was found to be too expensive for deep penetration calculations because of its strong dependence upon the kurtosis of the contribution distribution. It also yields smaller values in the presence of undersampling which eventually increase with the sampling of important particles. Therefore, its utilization was found to be not too productive.

The benefits of calculating the figure of merit are twofold, first it allows an easy comparison of the efficiencies of different schemes and also is an indicator that the variance of the population has become stable. Although the FOM may stay essentially constant in

severe undersampling conditions, once some important particles are processed it becomes an effective means to verify the stability of the estimates. Therefore, its usage is recommended.

The particle contribution distribution histogram was found to be the most effective way of detecting undersampling. In the breakdown region and more important — under severe undersampling conditions — the number of particles accounting for large fractions of the response is very small. This condition is easily identified from the histogram. This analysis does not heavily depend upon previous observations and is much faster and more reliable than any other means. It also provides a measure of the effectiveness of variance reduction techniques — which generally have the net effect of spreading out the values of the contributions producing a smoother distribution. Its utilization is highly recommended.

From the discussion above, it became evident that the most effective means to guarantee the reliability of an estimate in problems subject to undersampling is to know and characterize the population distribution. Therefore, the ability of the Monte Carlo method to simulate detailed descriptions of the population distribution must be exploited by the user — this is greatly facilitated by the new version of the MORSE code, MORSE/STAT — developed during the course of this research. This version of the code provides much more insight into the statistical quality of the solution obtained. The observation of the behavior of the new parameters as the solution evolves is a powerful means of determining if the undersampling condition exists. Because the standard version of the code provides only the standard deviation at the end of a complete run, the user loses all the interim information that the new version now provides.

The use of graphics for the presentation of the evolution of the statistics being estimated would enormously facilitate the observation of the behavior of the solution of the problem. Therefore, for future work, the coupling of a graphics package is highly recommended.

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APPENDICES

Appendix A

Batch Output

A.1 Sample Problem 1

A.1.1 Next Event Surface Crossing Estimator

***START BATCH 1 RANDOM-13579BDFDB97

SOURCE DATA
 YOU ARE USING THE DEFAULT VERSION OF SOURCE WHICH SETS WAVE TO DDP AND PROVIDES AN ENERGY IG.
 YOU ARE USING THE DEFAULT VERSION OF GTMED WHICH ASSUMES GEOMETRY AND XSUCT MEDIA ARE IDENTICAL.
 WAVE WAVE WAVE WAVE WAVE WAVE WAVE WAVE WAVE WAVE
 1.000E+05 1.00 0.0009 0.0004 0.0013 0.0 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH	RESPONSES(DETECTOR)	NEUTRON FLUX	CV(SD)	PKM
	RESPONSE	YSD	ACCUMULATED	YSD	
1	3.8398D-04	0.00327	3.8398D-04	0.00327	0.17907
2	4.4619D-05	0.00526	4.4619D-05	0.00526	0.10571
3	8.9053D-06	0.00679	8.9053D-06	0.00679	0.04823
4	2.2075D-06	0.01134	2.2075D-06	0.01134	0.12860
5	6.2544D-07	0.01497	6.2544D-07	0.01497	0.05511
6	1.8826D-07	0.02405	1.8826D-07	0.02405	0.10014
7	6.0974D-08	0.03847	6.0974D-08	0.03847	0.21179
8	2.0435D-08	0.04535	2.0435D-08	0.04535	0.06699
9	6.3437D-09	0.06413	6.3437D-09	0.06413	0.09174
10	2.1429D-09	0.10191	2.1429D-09	0.10191	0.17910

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	66060	0	0	0	10600	10902	4821	5249	3182	186	
2	56420	0	18868	7335	6219	9137	0	0	1586	445	
3	53727	16856	18827	0	3611	2010	1460	1905	1544	60	
4	65088	17609	7038	4878	3029	0	1162	642	297	757	
5	79683	11774	4679	1275	1088	1026	0	313	102	60	
6	83737	11062	3458	453	612	286	337	0	0	55	
7	93476	4674	1255	156	103	170	76	81	0	9	
8	96354	2586	602	225	83	47	48	26	28	1	
9	98235	1351	188	100	62	26	15	8	12	3	
10	99334	521	36	52	30	0	6	7	5	1	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO EDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY GAMLOST
 100000 0 0 189483 0 98727 46 99954 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 40 SECONDS.

***START BATCH 2 RANDOM=24934D19FDAB

SOURCE DATA

WDAYE JAVE UAVE VAVE WAVE XAVE YAVE ZAVE ACEAYE
 1.000E+05 1.00 -0.0003 0.0039 0.0000 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)		NEUTRON FLUX ACCUMULATED		FSD	CV(SD)	FOM
		(SD)	(SD)	RESPONSE	RESPONSE			
1	3.8273D-04	0.00311	3.8335D-04	0.00226	0.11038	3.6803D-04		
2	4.4120D-05	0.00439	4.4370D-05	0.00343	0.06929	1.5921D-04		
3	8.8814D-06	0.00746	8.8933D 06	0.00504	0.06061	7.5797D-03		
4	2.2191D-06	0.01225	2.2133D-06	0.00835	0.08322	2.6908D+03		
5	6.0900D-07	0.01549	6.1722D-07	0.01077	0.06376	1.6179D+03		
6	1.9154D-07	0.06106	1.8990D-07	0.03302	0.38768	1.7202D+02		
7	5.7283D-08	0.03704	5.9128D-08	0.02675	0.14283	2.6218D+02		
8	1.0250D-08	0.04034	1.0430D-08	0.03340	0.05806	1.6809D+02		
9	5.6615D-09	0.06481	6.0026D-09	0.04563	0.06415	9.0066D+01		
10	2.1078D-09	0.10720	2.1253D-09	0.07393	0.10690	3.4318D+01		

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	132189	0	0	0	21311	12256	17050	10461	6386	346	
2	112859	0	26190	26281	12466	18104	0	0	3205	895	
3	107459	33677	37648	0	7256	4132	2832	3807	3068	111	
4	130292	35140	14137	9807	5953	0	2273	1274	589	535	
5	159478	23730	9132	2533	2137	2073	0	614	0	303	
6	170370	20745	5437	913	1206	650	575	0	68	36	
7	183365	10233	3218	0	551	246	192	177	0	18	
8	192784	5137	1154	502	152	88	86	42	51	4	
9	196523	2694	269	334	156	0	49	41	22	6	
10	198697	1028	67	106	58	0	16	13	12	3	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISNA GAMGEN REALCOLL ALBEDO BDRYX ESCAPES E-CYF TIMEKILL R R KILL R R SURY GAMLOST
 100000 0 0 0 189052 0 98516 53 99947 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 39 SECONDS.

***START BATCH 0 RANLXOM-3F3275BGB73D

SOURCE DATA
 WTAVE 1.000E+05 JAVE 1.00 -0.0005 VAVE -0.0004 WAVE 0.0013 XAVE 0.0 YAVE 0.0 ZAVE 0.0 ACEAVE 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR); NEUTRON FLUX ACCUMULATED										CV(SD)	FCM
		FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD		
1	3.8373D-04	0.00305	3.8317D-04	0.00141	0.16056	2.3771D+04							
2	4.4566D-05	0.00523	4.4517D-05	0.00230	0.20914	8.9237D+03							
3	9.0082D-06	0.00783	8.9607D-06	0.00282	0.05729	5.9278D+03							
4	2.2733D-06	0.01716	2.2431D-06	0.00770	0.35579	7.9330D+02							
5	6.2939D-07	0.01752	6.2615D-07	0.00657	0.11378	1.0905D+03							
6	1.9336D-07	0.02525	1.8713D-07	0.01066	0.24013	4.1411D+02							
7	6.4693D-08	0.03323	5.9307D-08	0.01278	0.06307	2.8782D+02							
8	1.9984D-08	0.04316	1.9247D-08	0.02064	0.16855	1.1039D+02							
9	6.4810D-09	0.06625	6.1403D-09	0.02373	0.03558	8.3492D+01							
10	2.0340D-09	0.10733	2.0756D-09	0.03584	0.05307	3.6615D+01							

DETECTOR PARTICLES DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	529853	0	0	0	84241	87273	30172	41805	25352	1353	
2	452633	0	150167	58858	49638	72213	0	0	12810	3681	
3	430779	133766	150331	0	28621	16754	20115	11242	7919	472	
4	521317	140381	55955	39103	24188	0	9209	5238	3340	1269	
5	638110	93931	37016	10163	8619	8565	0	2442	707	447	
6	681110	76996	27975	3767	4739	2127	2837	0	0	449	
7	740819	41476	12958	0	2239	958	769	701	0	80	
8	770882	20727	4371	2370	552	335	390	177	183	13	
9	786102	10870	1101	960	445	208	102	75	104	33	
10	794864	3347	937	398	277	0	85	43	31	18	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO BDYX ESCAPE V-CUT TIMEKILL R R KILL R R SURY GAMLOST
 100000 0 0 0 189577 0 99451 47 99953 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTRS, 39 SECONDS.

***START BATCH 0 HANIXM-2218FACF2639F

SOURCE DATA

WTAVE 1.00 UAVE 0.0022 -0.0000 WAVE 0.0022 XAVE 0.0 YAVE 0.0 ZAVE 0.0 AGEAVE 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) NEUTRON FLUX ACCUMULATED										CY(SD)	FOM
		FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD	FSD		
1	3.8472D-04	0.00348	0.00348	3.8334D-04	0.00131	0.14715	2.4404D+04						
2	4.4803D-05	0.00469	0.00469	4.4549D-05	0.00211	0.19622	9.4277D+03						
3	8.9128D-06	0.00690	0.00690	8.9554D-06	0.00262	0.05259	6.0939D+03						
4	2.2128D-06	0.00949	0.00949	2.2398D-06	0.00693	0.34775	8.6942D+02						
5	6.1276D-07	0.01534	0.01534	6.2466D-07	0.00609	0.10566	1.1285D+03						
6	1.7981D-07	0.02118	0.02118	1.8632D-07	0.00978	0.22722	4.3681D+02						
7	5.5462D-08	0.03434	0.03434	5.9057D-08	0.01200	0.05833	2.9038D+02						
8	1.7885D-08	0.05078	0.05078	1.9095D-08	0.01923	0.15596	1.1298D+02						
9	5.4812D-09	0.07087	0.07087	6.0670D-09	0.02250	0.03368	8.2513D+01						
10	1.8839D-09	0.10804	0.10804	2.0543D-09	0.03402	0.04968	3.6114D+01						

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	595879	0	0	0	94801	98081	33904	47112	28712	1510	
2	509025	0	168798	66221	56059	81330	0	0	14422	4145	
3	484478	150339	169496	0	32261	18786	22543	12673	8895	528	
4	586235	158142	63076	43886	27236	0	10347	5890	3764	1424	
5	717738	105839	41604	11408	9752	9643	0	2725	803	488	
6	754286	98561	31573	4224	4062	3646	3163	0	0	505	
7	833392	46723	11032	3572	2491	1078	849	777	0	86	
8	867238	23382	4922	2639	600	378	422	198	204	37	
9	884445	12186	1241	957	593	231	113	84	113	37	
10	894297	3734	1022	446	306	0	90	49	35	21	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) 0 FISHN 0 GAMGEN 0 KALCOLL 0 ALBEDO 0 RBYX 0 ESCAPE 55 E-CUT TIMEKILL R R KILL R R SURV GAMLOST 100000 0 0 0 189798 0 98936 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 39 SECONDS.

***START BATCH 10 RANOM=2001327470P

SOURCE DATA
 WAVE 1.00 0.0008 0.0011 0.0010 0.0 0.0 0.0 0.0
 YAVE 1.00 0.0008 0.0011 0.0010 0.0 0.0 0.0 0.0
 ZAVE 1.00 0.0008 0.0011 0.0010 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX ACCUMULATED		FSD	CV(SD)	FOM
	BATCH RESPONSE	FSD	BATCH RESPONSE	FSD			
1	3.6186D-04	0.00322	3.8319D-04	0.00172	0.00172	0.13722	2.5230D+04
2	4.4287D-05	0.00650	4.4523D-05	0.00200	0.00200	0.17752	9.3759D+03
3	9.1627D-06	0.02447	8.9761D-06	0.00343	0.00343	0.22880	3.1964D+03
4	2.2404D-06	0.01259	2.2388D-06	0.00637	0.00637	0.33420	9.2849D+02
5	6.2488D-07	0.01638	6.2469D-07	0.00572	0.00572	0.09747	1.1512D+03
6	1.8444D-07	0.02180	1.8613D-07	0.00907	0.00907	0.21428	4.5682D+02
7	5.7758D-08	0.03139	5.8928D-08	0.01125	0.01125	0.05431	2.9727D+02
8	1.8387D-08	0.06864	1.9024D-08	0.01860	0.01860	0.13949	1.0877D+02
9	5.8183D-09	0.06809	6.0442D-09	0.02137	0.02137	0.03183	8.2390D+01
10	2.1751D-09	0.10446	2.0664D-09	0.03236	0.03236	0.04605	3.5921D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	662277	0	0	0	105337	108947	37615	52237	31913	1673	
2	565774	0	187600	73302	62348	90129	0	0	15975	4583	
3	538490	167125	180134	0	35685	20868	25121	14123	9865	589	
4	651487	175594	70015	48009	30237	0	11539	6571	4183	1565	
5	797553	117404	46254	12758	10858	10711	0	3035	0	1427	
6	838013	109550	35143	4666	4526	4028	3504	0	0	570	
7	925919	52009	12262	3931	2774	1203	950	857	0	95	
8	963540	26067	5450	2954	657	412	461	221	218	20	
9	982734	13539	1486	1154	547	255	126	97	120	42	
10	903666	4160	1130	489	333	0	103	54	41	24	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) PISHN GAMGEN REALCOLL ALBEDO IDRYX ESCAPE E-CUT TIMEKILL R R KILL. R R SURV GAMLOST
 100000 0 0 0 188934 0 98992 53 99947 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 39 SECONDS.

A.1.2 Point Detector Estimator

RANDOM=13579BDFDB97

***START BATCH 1

SOURCE DATA
 YOU ARE USING THE DEFAULT VERSION OF SOURCE WHICH SETS WASTE TO DDP AND PROVIDES AN ENERGY IG.
 YOU ARE USING THE DEFAULT VERSION OF GTEMED WHICH ASSUMES GEOMETRY AND XSICM MEDIA ARE IDENTICAL.
 WTAVE IAVE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE VAWE
 1.000E+05 1.00 0.0022 -0.0005 0.0018 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CV(SD)	FOM
	HATCH RESPONSE	FSD	ACCUMULATED RESPONSE	FSD			
1	3.8195D-04	0.02420	3.8195D-04	0.04420	0.16360	9.6140D+01	
2	4.0657D-05	0.03220	4.0657D-05	0.03220	0.17042	5.4278D+01	
3	1.0318D-05	0.18977	1.0318D-05	0.18977	0.45750	1.5631D+00	
4	2.2010D-06	0.10484	2.2010D-06	0.10484	0.24872	5.1215D+00	
5	5.8018D-07	0.16399	5.8018D-07	0.16399	0.24418	2.0932D+00	
6	1.3670D-07	0.13992	1.3670D-07	0.13992	0.20058	2.8754D+00	
7	1.0456D-07	0.65115	1.0456D-07	0.65115	0.49116	1.3276D-01	
8	3.6075D-08	0.39992	3.6075D-08	0.39992	0.31527	3.5196D-01	
9	4.4715D-09	0.26794	4.4715D-09	0.26794	0.26414	6.7894D-01	
10	8.1909D-10	0.22073	8.1909D-10	0.22073	0.24052	1.1553D+00	

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	82140	0	0	0	0	6767	7358	717	795	251	49
2	69700	0	14634	7215	3000	1316	1316	971	68	103	5
3	78956	13447	1962	1753	289	144	144	23	13	1	0
4	81208	12320	2213	405	198	43	43	21	6	5	0
5	90177	4818	1100	165	76	18	18	7	3	1	1
6	88529	6765	885	246	37	34	34	2	4	2	0
7	96335	288	15	3	1	0	0	0	0	0	0
8	96700	30	0	1	1	1	1	0	0	0	0
9	96124	619	63	10	0	1	1	2	0	1	0
10	96140	703	86	21	0	3	3	2	0	1	0

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO

BDRYX ESCAPE

R-CUT TIMKILL R R KILL R R SURY GARLOST

100000 0 0 0 188986 0 98169 48 99952 0 0 0 0 0 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 45 SECONDS.

RANDOM=EG6GF32896.147

***START BAY2H 2

SOURCE DATA
 WFAVE 1.000E+05

IAVE 1.00 0.0012 0.0013 -0.0041 0.0 0.0 0.0
 YAVE 0.0 0.0 0.0 0.0 0.0 0.0
 ZAVE 0.0 0.0 0.0 0.0 0.0 0.0
 AGEAVE 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CV(SD)	FCM
	BATCH RESPONSE	ACCUMULATED RESPONSE	FSD	RESPONSE			
1	3.8376D-04	0.02215	3.8786D-04	0.01640	0.11907	1.0453D+02	
2	3.9041D-05	0.02885	3.9849D-05	0.02167	0.11323	5.9872D+01	
3	1.0062D-05	0.16319	1.0190D-05	0.12539	0.30288	1.7883D+00	
4	1.9870D-06	0.08756	2.0940D-06	0.06900	0.18091	5.9046D+00	
5	6.1231D-07	0.26090	5.9624D-07	0.15592	0.35056	1.1564D+00	
6	1.4004D-07	0.20385	1.3837D-07	0.12417	0.28457	1.8236D+00	
7	3.9161D-08	0.29061	7.1859D-08	0.48030	0.47789	1.2188D-01	
8	1.6220D-08	0.28986	2.6147D-08	0.29016	0.28698	3.3394D-01	
9	6.8172D-09	0.54999	5.6443D-09	0.35118	0.43483	2.2798D-01	
10	2.5654D-09	0.60292	1.6923D-09	0.46012	0.45654	1.3280D-01	

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	164540	0	0	0	13448	14540	1483	1387	617	71	
2	139619	0	29245	12846	7456	2592	1562	563	156	40	
3	158315	26555	3992	3536	554	274	50	19	2	0	
4	156810	29433	4799	1350	415	145	64	7	12	0	
5	180518	10233	1634	356	126	37	11	4	2	0	
6	178712	12468	1426	384	90	51	4	6	2	1	
7	191744	3422	153	21	4	2	1	0	0	0	
8	193308	223	18	0	.	2	1	0	0	0	
9	193073	643	21	10	5	2	1	1	0	0	
10	193791	173	5	5	1	1	0	0	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL
 100000 0 0 0 89185

ESCAPE 45
 RDRYX 98732
 R-CUT TIMEKILL R R KILL R SURV GAMLOST
 99955 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 48 SECONDS.

***START BATCH 3 RANDOM=6A5E9CFC0C63

SOURCE DATA

WTAVE LAVE UAVE VAVE WAVE XAVE YAVE ZAVE AGEAVE
 1.00E+05 1.00 -0.0026 -0.0011 -0.0049 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)		NEUTRON FLUX ACCUMULATED RESPONSE		CV(SD)	FCM
		FSD	FSD	FSD	FSD		
1	3.6996D-04	0.01881	3.7856D-04	0.01264	0.10199	0.10199	1.1718D+02
2	5.7066D 05	0.12868	4.5588D-05	0.05516	0.23556	0.23556	6.1556D+00
3	8.3233D-06	0.06395	9.5679D-06	0.09094	0.29039	0.29039	2.2647D+00
4	2.7789D-06	0.29318	2.3223D-06	0.12408	0.37712	0.37712	1.2165D+00
5	6.1005D-07	0.18697	6.0085D-07	0.12137	0.27644	0.27644	1.2714D+00
6	1.2668D-07	0.13773	1.3447D-07	0.09553	0.23163	0.23163	2.0523D+00
7	3.4557D-08	0.19707	5.9425D-08	0.38908	0.47330	0.47330	1.2372D-01
8	9.9329D-09	0.24349	2.0743D-08	0.24692	0.28005	0.28005	3.0717D-01
9	6.2381D-09	0.68128	5.8422D-09	0.33160	0.33411	0.33411	1.7033D-01
10	1.0023D-09	0.49815	1.4623D-09	0.37279	0.41650	0.41650	1.3476D 01

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	247165	0	43915	0	19974	21772	2183	2061	890	158	
2	209621	0	16993	30314	2570	3398	1046	275	19	4	
3	237775	28522	6569	5227	441	801	42	63	8	0	
4	244352	36525	1903	1379	459	120	49	23	1	1	
5	273349	13344	2318	593	149	37	13	7	2	0	
6	267957	18414	448	721	125	84	6	8	4	1	
7	286616	2900	448	27	17	5	3	0	0	0	
8	289571	691	53	13	0	3	1	1	0	0	
9	289756	841	32	13	4	2	0	1	0	0	
10	290482	465	38	10	3	0	1	0	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) PISRN GAMGEN REACOLL ALBEDO RDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 0 0 0 189879 0 99126 55 99945 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 49 SECONDS.

***START BATCH 4 RANDOM-CL9F64C8B3EF

SOURCE DATA
 WTAVE IAVE UAVE VAWE WAVE XAVE YAVE ZAVE AGEAVE
 1.000E+05 1.00 -0.0006 -0.0027 0.0006 0.0 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CV(SD)	FOM
	BATCH RESPONSE	ACCUMULATED RESPONSE	FSD	RESPONSE			
1	3.9975D-04	0.02955	3.0386D-04	0.01211	0.08932	0.08932	9.5714D+01
2	4.3695D-05	0.03807	4.5115D-05	0.04281	0.22480	0.22480	7.6597D+00
3	7.9846D-06	0.06284	9.1721D-06	0.07245	0.28023	0.28023	2.6741D+00
4	2.5077D-06	0.20961	2.3686D-06	0.10678	0.29830	0.29830	1.2310D+00
5	9.0974D-07	0.42952	6.7897D-07	0.16511	0.37187	0.37187	5.1487D-01
6	1.4804D-07	0.13330	1.3786D-07	0.07851	0.18837	0.18837	2.2771D+00
7	4.7006D-08	0.17820	5.6320D-08	0.31013	0.46651	0.46651	1.4594D-01
8	1.0194D-08	0.15543	1.8195D-08	0.21329	0.27711	0.27711	3.0853D-01
9	2.5654D-09	0.13361	5.0230D-09	0.28976	0.33295	0.33295	1.6718D-01
10	7.1483D-10	0.15417	1.2754D-09	0.32129	0.41462	0.41462	1.3598D-01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	329383	0	0	0	26758	29111	2845	2969	1045	139	
2	279176	0	58615	40614	3386	4215	1424	580	112	10	
3	316751	31761	26433	7785	2501	789	274	116	21	2	
4	329392	45013	6839	1833	610	184	66	19	2	1	
5	366931	15938	2285	605	62	44	6	6	1	0	
6	359588	22629	2929	751	174	110	16	9	7	1	
7	382177	3856	522	131	45	4	5	3	0	0	
8	385734	1235	174	21	8	2	2	1	0	0	
9	385546	1862	156	35	11	4	2	1	0	0	
10	387066	878	94	9	8	2	1	0	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R SURY GAMLOST
 100000 0 0 0 189773 0 99096 59 99941 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 50 SECONDS.

RANDOM-DC641RDKA4AP

***START BATCH 5

SOURCE DATA

WAVE 1.000E+05 WAVE 1.00 WAVE 0.0009 WAVE 0.0035 WAVE 0.0044 WAVE 0.0 YAVN 0.0 ZAVR 0.0 ZAVR 0.0 ZAVR 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH	RESPONSES:(DETECTOR);		NEUTRON FLUX		CY(SD)	FOM
		FSD	ACCUMULATED	RESPONSE	FSD		
1	3.8594D-04	0.02529	3.8427D-04	0.01093	0.07949	0.07949	9.3948D+01
2	4.7310D-05	0.09346	4.5554D-05	0.03908	0.19146	0.19146	7.3487D+00
3	8.3560D-06	0.06706	9.0089D-06	0.06031	0.26855	0.26855	3.0857D+00
4	2.6277D-06	0.23210	2.4205D-06	0.09761	0.25087	0.25087	1.1779D+00
5	5.4350D-07	0.11686	6.5116D-07	0.13893	0.36455	0.36455	5.8148D-01
6	1.2134D-07	0.08476	1.3456D-07	0.06614	0.17845	0.17845	2.5652D+00
7	3.3158D-08	0.22320	5.1608D-08	0.27186	0.46134	0.46134	1.5185D-01
8	1.0061D-08	0.43582	1.6496D-08	0.19468	0.25836	0.25836	2.9613D-01
9	3.1820D-09	0.38605	4.6548D-09	0.25565	0.31928	0.31928	1.7171D-01
10	7.7008D-10	0.29357	1.1743D-09	0.28179	0.40696	0.40696	1.4133D-01

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	41146	0	0	51120	0	33573	36822	3569	3713	1290	171
2	348547	0	73254	9785	4290	4290	5595	1424	763	105	9
3	395456	39924	33235	2890	3145	201	893	421	140	35	4
4	415652	54026	9262	2890	201	23	254	77	23	2	2
5	45252	22537	3636	613	208	65	20	12	2	1	1
6	446245	30955	3986	1200	193	129	44	44	26	13	1
7	477683	4892	575	213	74	19	7	3	3	0	0
8	482198	1554	184	45	18	1	1	1	1	1	0
9	481923	2282	268	42	12	6	2	0	0	1	0
10	483851	1036	138	34	14	5	1	1	1	0	0

NUMBER OF COLLISIONS OF TYPE NCDULL

SOURCE SPLIT(D) 0 FISH 0 GAMEN REALCOLL. 0 ALBEDO 0 BDRYX 0 ESCAPE 51 E CUT TIMEKILL R R KILL R R SURV GAMLOST 00000 0 0 169793 0 98928 51 99949 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 51 SECONDS.

***START BATCH 6 RANDOM-3C2EC9BRCBAB

SOURCE DATA
 WAVE IAVE UAVE VAVE WAVE XAVE YAVE ZAVE ACEAVE
 1.000E+05 1.00 0.0020 0.0012 0.0014 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CY(SD)	FOM
	BATCH RESPONSE	FSD	ACCUMULATED RESPONSE	FSD			
1	4.0937D-04	0.03452	3.8846D 04	0.01086	0.06968	7.9325D+01	
2	4.1039D-05	0.03509	4.4801D-05	0.03354	0.18672	8.3148D+00	
3	8.6497D-06	0.05580	8.9490D-06	0.05138	0.26036	3.5432D+00	
4	1.9491D-06	0.11055	2.3419D-06	0.08546	0.24309	1.2810D+00	
5	1.2141D-06	0.36437	7.4498D-07	0.14155	0.25251	4.6696D-01	
6	5.4674D-07	0.51612	2.0326D-07	0.23425	0.45784	1.7050D-01	
7	9.3560D-08	0.28522	5.8667D-08	0.21351	0.40497	2.0523D-01	
8	1.4453D-08	0.16652	1.6156D-08	0.16750	0.25272	3.3345D-01	
9	3.6859D-09	0.18078	4.4933D-09	0.22208	0.31534	1.8969D-01	
10	9.1095D-10	0.19769	1.1304D-09	0.24539	0.40221	1.5537D-01	

DETECTOR PART(CLR DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	493545	0	0	0	40204	44033	4260	4706	1309	207	
2	418609	0	87715	61190	5141	6336	2076	865	192	15	
3	474818	47695	39771	11181	4351	1078	500	166	44	6	
4	493592	67864	13228	2644	1046	269	115	50	1	3	
5	555655	19530	2746	676	112	52	15	4	3	0	
6	562898	13980	1978	343	112	17	11	3	1	0	
7	523180	5878	940	76	42	13	5	3	1	0	
8	572035	3424	222	71	18	10	3	2	1	0	
9	574294	2760	304	78	19	10	4	1	1	0	
10	580614	1257	161	46	22	7	3	1	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMEN REALCOLL AIRBDO BDRYX ESCAPE E CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 0 0 0 188636 0 98973 47 99953 0 0 0 0 0 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 47 SECONDS.

***START BATCH 7 RANDOM-C9F1F9A47EAD

SOURCE DATA
 WTAVE 1.000E+05 IAVE 1.000E+16 VAVS 0.0003 WAVE 0.0004 XAVE 0.0 YAVE 0.0
 ZAVE 0.0 AGRAVE 0.0

PARTICLES PER CH**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES (DETECTOR)										NEUTRON FLUX			FOM
		ADJUSTED										FSD	CV(SD)	FOM	
1	3.9492D-04	0	0	0	0.03325	0	0	0	0	0	0	0.01046	0.07045	7.3247D+01	
2	4.3649D-05	0	0	0	0.07922	0	0	0	0	0	0	0.03094	0.17686	8.3766D+00	
3	8.6719D-06	49149	0	0	0.04958	0	0	0	0	0	0	0.04477	0.25421	3.9992D+00	
4	1.7172D-06	90717	0	0	0.05357	0	0	0	0	0	0	0.07638	0.24167	1.3744D+00	
5	6.6371D-07	22695	0	0	0.28177	0	0	0	0	0	0	0.12852	0.23500	4.8540D-01	
6	1.0434D-07	23861	0	0	0.42497	0	0	0	0	0	0	0.21837	0.44716	1.6812D-01	
7	4.0285D-08	6838	0	0	0.15088	0	0	0	0	0	0	0.19232	0.40234	2.1698D-01	
8	1.1255D-08	4369	0	0	0.23298	0	0	0	0	0	0	0.15202	0.24644	3.4691D-01	
9	2.6400D-09	4502	0	0	0.14657	0	0	0	0	0	0	0.20270	0.31403	1.9513D-01	
10	5.4344D-10	2906	0	0	0.23364	0	0	0	0	0	0	0.22784	0.39989	1.5443D-01	

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DETECTOR	PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS										
	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	57573	0	0	0	0	46873	51419	4982	1526	245	
2	488250	0	102341	71537	6007	7400	2424	1016	227	19	
3	553868	49149	52998	13059	4007	2319	599	186	64	10	
4	560939	90717	16617	5130	1155	545	181	40	13	3	
5	648353	22695	3237	776	123	68	14	7	3	0	
6	649229	23861	2316	366	124	50	14	3	1	0	
7	668738	6838	1079	75	70	8	11	5	1	0	
8	672824	4369	244	98	36	14	1	4	1	0	
9	673264	4502	496	83	34	7	7	2	1	0	
10	675952	2906	158	91	20	14	3	1	0	0	

NUMBER OF COLLISIONS OF TYPE NCOIL
 SOURCE SPLIT(D) FISH GAMGEN REACCOLL ALBEDO DDYX ESCAPE L-CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 0 0 0 189060 0 96413 48 99952 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 50 SECONDS.

***START BATCH 0 RANX3M-B0648D2C4417

SOURCE DATA

WAVE 1.00 HAVR -0.0021 WAVE -0.0007 WAVE 0.0024 XAVE 0.0 YAVE 0.0
 ZAVE 0.0 ACWAVE 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)		NEUTRON FLUX ACCUMULATED RESPONSE		FSD	CV(SD)	FCM
		FSD	RESPONSE	RESPONSE	RESPONSE			
1	3.9315D-04	0.03379	3.8985D-04	0.01009	0.06970	6.8916D+01		
2	4.9785D-05	0.10155	4.5280D-05	0.03011	0.15079	7.7312D+00		
3	7.9145D-06	0.05531	8.7851D-06	0.04022	0.28815	4.3349D+00		
4	1.8952D-06	0.09951	2.2080D-06	0.06901	0.23591	1.4721D+00		
5	5.4595D-07	0.07778	7.0994D-07	0.11654	0.23347	5.1622D-01		
6	2.2764D-07	0.33281	1.9394D-07	0.19262	0.41951	1.8896D-01		
7	4.3906D-08	0.23969	5.4521D-08	0.17455	0.39471	2.3013D-01		
8	1.3283D-08	0.25663	1.5184D-08	0.13827	0.24668	3.6670D-01		
9	3.8514D-09	0.35037	4.1814D-09	0.18384	0.29964	2.0745D-01		
10	8.2293D-10	0.27035	1.0186D-09	0.20665	0.39295	1.6419D-01		

DETECTOR

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	658062	0	0	0	0	53486	58798	5697	6104	1747	274
2	557855	0	117020	81862	6880	8414	8414	2793	1207	226	20
3	632771	56397	60570	13962	5503	2483	2483	850	187	93	11
4	640882	103804	18966	5551	1628	606	606	215	36	24	4
5	737559	28696	3853	1259	126	109	109	9	13	3	0
6	741932	27199	2654	433	143	52	52	22	3	2	0
7	764194	7823	1085	240	107	8	8	11	7	1	0
8	768331	5580	255	147	33	21	21	2	1	2	0
9	769421	5169	574	88	44	10	10	8	1	1	0
10	772134	3464	395	126	21	16	16	1	3	0	0

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISIN GAMESFN REACCOLL ALARFD) BDRYX ESCAPE E-DUT TIMEKILL R R KILL R R SURV GAMCOST
 100000 0 0 189675 0 99466 54 99946 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 53 SECONDS.

***START BATCH 9 RANDOM-F82DR70E05FF

SOURCE DATA
 WAVE IAVE UAVE VAVE WAVE XAVE YAVE XAVE YAVE XAVE YAVE XAVE YAVE
 1.000E+05 1.00 -0.0014 -0.0059 6.0008 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)										NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CV(SD)	FOM
		10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0				
1	4.0154D-04	0.03399	0.03399	0	0	0	60023	66136	6371	7417	1748	227	0.06437	6.5685D+01	
2	5.4195D-05	0.13317	0.14952	73934	73934	0	7733	10378	2670	788	193	10	0.14705	6.2514D+00	
3	8.4099D-06	0.09029	60168	15730	15730	6169	6169	2788	955	209	104	13	0.23244	4.5057D+00	
4	1.7494D-06	0.07466	21391	6219	6219	1831	1831	606	321	39	25	4	0.23352	1.5646D+00	
5	7.2271D-07	0.20346	4735	1007	1007	147	147	125	15	10	1	2	0.22280	5.5515D-01	
6	1.4888D-07	0.13352	2972	463	463	194	194	53	28	2	3	0	0.41761	2.0084D-01	
7	3.8305D-08	0.12517	1182	303	303	95	95	31	17	10	1	1	0.39315	2.4113D-01	
8	4.0050D-08	0.83420	303	85	85	32	32	2	4	1	1	0	0.40162	1.1628D-01	
9	1.8052D-08	0.85224	118	33	33	12	12	1	2	0	0	0	0.43233	6.0227D-02	
10	1.9662D-09	0.53664	271	59	59	32	32	0	5	0	0	0	0.31167	1.6148D-01	

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	740468	0	0	0	60023	66136	6371	7417	1748	227	
2	627553	0	14952	73934	7733	10378	2670	788	193	10	
3	711802	63459	60168	15730	6169	2788	955	209	104	13	
4	704967	132823	21391	6219	1831	606	321	39	25	4	
5	829883	32207	4735	1007	147	125	15	10	1	2	
6	834804	30599	2972	463	194	53	28	2	3	0	
7	859764	8801	1182	303	95	31	17	10	1	1	
8	867854	2824	303	85	32	2	4	1	1	0	
9	870112	1914	118	33	12	1	2	0	0	0	
10	870879	1882	271	59	32	0	5	0	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO RDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 0 0 189195 0 99061 51 99949 0 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 49 SECONDS.

RANDOM=ACF312D08E0B

***START BATCH 10

SOURCE DATA

WPAVE IAVE UAVE VAVE WAVE XAVE YAVE ZAVE AGEAVE
 1.000E+05 1.00 -0.0019 0.0022 0.0032 0.0 0.0 0.0 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)										NEUTRON FLUX	
		FSD	ACCUMULATED RESPONSE	FSD	CV(SD)	FOM							
1	3.8024D-04	0.03493	3.9006D-04	0.00912	0.06178	6.7442D+01							
2	4.2527D-05	0.08825	4.5916D-05	0.02979	0.14028	6.3208D+00							
3	1.2067D 05	0.30180	9.0757D-06	0.05148	0.30909	2.1171D+00							
4	7.7908D-06	0.08807	2.1204D-06	0.05826	0.22978	1.6529D+00							
5	6.4603D-07	0.10061	7.0483D-07	0.09736	0.21780	5.9187D-01							
6	2.3432D-07	0.11396	1.8347D 07	0.16347	0.41652	2.0995D-01							
7	3.3903D-08	0.24804	5.0838D-08	0.15096	0.38844	2.4621D-01							
8	1.2554D-08	0.29338	1.7408D 08	0.21587	0.39772	1.2044D-01							
9	4.3514D-09	0.40431	5.5855D-09	0.29830	0.42753	6.3056D-02							
10	1.1817D-10	8.17964	1.0233D-09	0.21594	0.26580	1.2032D-01							

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	3.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	822591	0	0	0	66835	73435	7097	8228	1069	333	
2	696963	0	146884	102572	8582	11123	3570	870	201	18	
3	790633	80272	66264	19674	6252	1790	840	281	73	9	
4	782995	147859	23780	6410	2527	667	362	30	38	4	
5	922034	35882	4794	1585	161	140	19	1	1	2	
6	927492	33989	3311	456	270	43	48	1	4	0	
7	953274	9730	1164	469	101	39	19	8	3	1	
8	964274	3122	424	95	34	4	4	1	1	0	
9	965562	2324	125	40	15	1	1	1	1	0	
10	967635	2078	295	65	27	8	4	2	0	0	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISRN GAMGEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIME KILL R R SURV GAMLOST
 100000 0 0 0 189336 0 98637 56 99944 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 17 MINUTES, 46 SECONDS.

A.2 Sample Problem 2

***START BATCH 1 RANDOM=000012FA731A

SOURCE DATA
 YOU ARE USING THE DEFAULT VERSION OF SOURCE WHICH SMTS WATE TO DPF AND PROVIDES AN ENERGY IG.
 WAVE IAVE WAVE
 9.1687E-04 10.23 0.0007 -0.0001 -0.0027 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

4 PT R**2 FLUENCE

DETECTOR	BATCH	RESPONSES(DETECTOR)		NEUTRON FLUX		PSD	CV(SD)	FOM
		FSD	ACCUMULATED	RESPONSE	RESPONSE			
1	1.9356D+00	0.01002	1.9356D+00	0.01002	0.01002	0.06790	1.5650D+03	
2	2.1357D+00	0.01358	2.1357D+00	0.01358	0.01358	0.09257	8.5118D+02	
3	1.8077D+00	0.01382	1.8077D+00	0.01382	0.01382	0.06930	8.2183D+02	
4	6.6802D-01	0.01746	6.6802D-01	0.01746	0.01746	0.07040	5.1510D+02	
5	4.3622D-01	0.01763	4.3622D-01	0.01763	0.01763	0.04574	5.0528D+02	
6	1.7872D-01	0.02763	1.7872D-01	0.02763	0.02763	0.08732	2.0563D+02	
7	4.2268D-02	0.04378	4.2268D-02	0.04378	0.04378	0.12017	8.1923D+01	

64

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	54507	23578	0	6594	5412	3180	2963	0	676	298	
2	53277	17817	6512	5591	3485	1430	0	599	399	334	
3	52490	13827	5429	4839	2998	2862	0	525	351	283	
4	38218	11400	0	2219	1946	1115	948	0	212	128	
5	33332	5916	3919	1514	819	991	785	0	146	74	
6	23365	3780	3779	0	638	304	434	189	31	35	
7	12721	898	1170	966	0	118	85	71	26	9	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISH GAMEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R KILL R SURV GAMLOST
 100000 1960 0 1917108 0 1084495 0 90000 0 11960 832 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 6 MINUTES, 22 SECONDS.

RANDOM-195E7A62575A

***START BATCH 4

SOURCE DATA

WAVE 10.23 IAVE -0.0007 WAVE 0.0045 WAVE 0.0007 XAVE 0.0 YAVE 0.0 ZAVE 0.0 ACRAVE 0.0

4 0) R**2 PLURANCE

DETECTOR	RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CV(5D)	NOM
	BATCH RESPONSE	ACCUMULATED RESPONSE	RESPONSE	RESPONSE			
1	1.9364D+00	0.00965	1.9323D+00	0.00509	0.003785	0.03785	1.5200D+03
2	2.0632D+00	0.01234	2.0821D+00	0.00669	0.07246	0.07246	8.8054D+02
3	1.7538D+00	0.01129	1.7815D+00	0.00678	0.05849	0.05849	8.5936D+02
4	6.5784D-01	0.01681	6.5927D-01	0.00886	0.04088	0.04088	5.0220D+02
5	4.3723D-01	0.01896	4.3334D-01	0.00960	0.03323	0.03323	4.2843D+02
6	1.7664D 01	0.02762	1.7415D-01	0.01414	0.08946	0.08946	1.9727D+02
7	4.1097D-02	0.03931	4.0930D-02	0.02236	0.09756	0.09756	7.8876D+01

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	218391	93707	0	26647	21541	12808	11736	0	2675	1185	
2	212557	71346	26538	14053	19413	16649	0	2393	1582	1192	
3	209494	55161	22094	19438	11965	11508	0	2140	1409	1044	
4	152410	45703	0	8688	7537	4354	3793	0	904	479	
5	123567	32732	15823	6192	3144	3996	2974	0	542	271	
6	92951	15200	15051	0	2432	1170	1453	967	133	128	
7	50402	3695	4646	2052	1627	503	352	240	87	46	

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISIN GAMBIN REACCOLL ALIBFO UDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY GAMLOST
 100000 1764 0 0 1910548 0 1082420 0 89976 0 11788 0 11788 877 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 6 MINUTES, 20 SECONDS.

***START BATCH B RANDOM-E18DB/3979A2

SOURCE DATA
 WTAVE 9.687E+04 YAVE 10.24 UAVE -0.0006 VAVE 0.0023 WAVE -0.0008 XAVE 0.0 YAVE 0.0 ZAVE 0.0 AGEAYK 0.0

4 PI R**2 PLUNNCE

DETECTOR	RESPONSES(DETECTOR)		NEUTRON MIX		CY(SD)	FOM
	BATCH RESPONSE	PSD	ACCUMULATED RESPONSE	FSD		
1	1.4682D+00	0.01336	1.9363D+00	0.00395	0.05527	1.2603D+03
2	2.0506D+00	0.01050	2.0677D+00	0.00474	0.06635	8.7580D+02
3	1.7800D+00	0.01507	1.7806D+00	0.00481	0.04436	8.5148D+02
4	6.5762D-01	0.01868	6.5702D-01	0.00636	0.03780	4.8643D-02
5	4.3619D-01	0.02124	4.5198D-01	0.00685	0.02481	4.1995D+02
6	1.6936D-01	0.02359	1.7512D-01	0.00991	0.05817	2.0069D+02
7	3.9773D-02	0.04340	4.0704D-02	0.03215	0.35553	4.0139D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	437702	186731	0	53153	43326	25502	23435	0	5417	2349	
2	425354	142808	52742	27985	39041	33274	0	4796	3099	2332	
3	420041	110018	43804	39639	18221	28678	0	4138	2754	2138	
4	305183	91018	0	37699	15086	8620	7538	0	1801	933	
5	247532	65714	31791	12246	6246	7958	5858	0	1078	526	
6	186051	30806	29902	0	4812	2417	3202	1554	281	264	
7	100953	7476	9302	4107	3358	1038	438	629	240	82	

NUMBER OF COLLISIONS OF TYPE NCULL

SOURCE SPLIT(D) 1791 0
 100000 1791 0 1901602 0 1082298 0
 ESCAPE 0 89847 0 11944 849 0
 8-CUVY TIMEXKILL R R KILL R R SURV GAMLOST

TIME REQUIRED FOR THE PRECEDING BATCH WAS 6 MINUTES, 20 SECONDS.

***START BATCH 9 4ANDMOM=30.35.3005586A

SOURCE DATA
 WAVE 9.687E-04 JAVE 10.23 JAVE 0.0044 WAVE 0.0034 WAVE 0.0008 XAVE 0.0 YAVE 0.0 ZAVE 0.0 AGEAVE 0.0

1 P1 R**2 FIJENCE

DETECTOR	BATCH		RESPONSES(DETECTOR)		NEUTRON FLUX		FSD	CV(SD)	POM
	RESPONSE	RESPONSE	FSI	ACCUMULATED	RESPONSE	RESPONSE			
1	1.9292D+00	0.01005	0.01005	1.9355D+00	0.00369	0.05057	1.2876D+03		
2	2.1031D+00	0.01235	0.01235	2.0716D+00	0.00443	0.06004	8.9132D+02		
3	1.7628D+00	0.01144	0.01144	1.7786D+00	0.00446	0.04096	8.7957D+02		
4	6.6494D-01	0.02153	0.02153	6.5790D-01	0.00614	0.04018	4.6374D+02		
5	4.3820D 01	0.02111	0.02111	4.3267D-01	0.00653	0.02528	4.1115D+02		
6	1.7186D 01	0.02725	0.02725	1.7476D-01	0.00931	0.05359	2.0186D+02		
7	3.9749D-02	0.05783	0.05783	4.0598D-02	0.02072	0.23381	4.0779D+01		

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	492473	210126	0	59699	48725	28672	26386	0	6104	2635	
2	478452	160782	59350	31469	43961	37351	0	5374	3505	2649	
3	472611	123689	49149	43934	26885	25905	0	4673	3124	2403	
4	343184	102559	0	19949	16905	9682	8490	0	2044	1038	
5	278473	73966	35804	13712	7017	8913	6642	0	1227	595	
6	209353	34641	33618	0	5427	2715	3676	1746	318	295	
7	113378	8439	10468	4628	3778	1172	485	690	270	91	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 1699 0 0 1907716 0 1081844 0 89972 0 11727 811 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 6 MINUTES, 20 SECONDS.

***START BATCH 10 RANXOM=6ARAAJFC1202

SOURCE DATA
 WTAVE 10.23 CAVE -D.0008 WAVE -0.0001 XAVE 0.0029 YAVE 0.0000 ZAVE 0.0000 AGWAVE 0.0

4 PJ R**2 ETHENCE

DETECTOR	RESPONSES(DIRECTOR)		NEUTRON FLUX		FSD	CY(5D)	PDM
	BATCH	PSD	ACCUMULATED	RESPONSE			
1	1.9493D+00	0.01053	1.9360D+00	0.00348	0.00348	0.04639	1.2998D+03
2	2.1167D+00	0.01896	2.0762D+00	0.00442	0.00442	0.07557	8.0439D+02
3	1.7697D+00	0.01374	1.7777D+00	0.00424	0.00424	0.03745	8.7482D+02
4	6.6807D-01	0.01736	6.5892D-01	0.00580	0.00580	0.03690	4.6913D+02
5	4.3582D-01	0.02043	4.3298D-01	0.00622	0.00622	0.02446	4.0742D+02
6	1.7285D-01	0.04121	1.7457D-01	0.00933	0.00933	0.08119	1.8099D+02
7	3.7749D-02	0.03733	4.0313D-02	0.01910	0.01910	0.22601	4.3177D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	547397	233200	0	66455	54167	31751	29356	0	6761	2952	
2	531797	178649	65945	34897	48774	41508	0	5868	3934	2967	
3	525358	137393	54507	48902	23747	35862	0	5154	3475	2652	
4	381496	113951	0	22222	18850	10745	9453	0	2284	1154	
5	309433	82274	39828	15236	7791	9984	7363	0	1363	652	
6	232767	38494	37346	0	6042	2991	4070	1982	331	318	
7	126159	9453	9125	7702	4160	1308	535	753	298	100	

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGRN KALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURV GAMLOST
 100000 1765 0 0 1914825 0 1084431 0 89874 0 11891 811 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 6 MINUTES, 21 SECONDS.

A.3 Sample Problem 3

A.3.1 Without Source Step Biasing

RANDOM-115798D5UB97

***START BATCH 1

SOURCE DATA

YOU ARE USING THE DEFAULT VERSION OF GTMED WHICH ASSUMES GEOMETRY AND XSECT MEDIA ARE IDENTICAL.

WTAVE WAVE UAVE WAVE YAVE XAVE YAVE ZAVE AGEAVE
1.000E+04 1.00 0.0050 -0.0036 0.4944 2.392E 01 1.607E-01 9.996E-05 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CV(SD)	FOM
1	3.3598D-09	0.16022	3.3598D 09	0.16022	0.09256	2.2377D+01

DETECTOR	PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS										
1	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
	9281	23	0	0	0	5	0	5	0	0	0

NUMBER OF COLLISIONS OF TYPE NCOLL													
SOURCE SPLIT(D)	FLSHN	GAMGEN	REALCOLL	ALRTO	RDYX	ESCAPE	E-CUT	TIMEKILL	R	R	R	SURY	GAMLOST
10000	0	0	112485	0	12841	6122	3878	0	0	0	0	0	0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 1 MINUTE, 44 SECONDS.

RANUKM-F56A1E7C7747

***START BATCH 4

SOURCE DATA

IAVE UAVE VAVE WAVE XAVE YAVE ZAVE AGEAVE
 1.000E+04 1.00 0.0005 0.0072 0.5050 -5.0968-01 5.352R-01 9.976E-05 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) PSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CY(SD)	FOM
1	2.9534D-09	0.16513	3.5668D-09	0.09836	0.12074	1.4634D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

1	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	37191	103	0	0	0	0	0	21	0	2	3

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D)	FISH	GAMGEN	REALCOLL	AUREDO	HDRYX	ESCAPE	E-CUT	TIMEKILL	R	R	R	SURY	GAMJOST
10000	0	0	114911	0	12950	6109	3891	0	0	0	0	0	0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 1 MINUTE, 46 SECONDS.

RANDOM=8E6E7EC9C6CF

***START BATCH 8

SOURCE DATA

WAVE 1AVE UAVE VAVE WAVE XAVE YAVE ZAVE AGRAYE
 1.000E+04 1.00 0.0012 0.0040 0.4985 2.509E-01 1.348E+00 9.996E-05 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CY(SD)	FCM
1	3.0809D-09	0.16312	3.3484D-09	0.06688	0.07893	1.5792D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	74328	212	0	0	0	0	24	5	5	5

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D)	FISHN	GAMCEN	REALCOLL.	ALRDCO	RDRYX	ESCAPE	E-CUT	TIMEKILL	R	R	R	SURY	GAMLOST
10000	0	0	113448	0	32917	6103	3887	0	0	0	0	0	0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 1 MINUTE, 45 SECONDS.

***START BATCH 9 RANDOM-B2C9287DB8BF

SOURCE DATA

WAVE IAVE UAVE VAVE WAVE XAVE YAVE ZAVE ASAVE
 1.000E+04 1.00 -0.0063 -0.0054 0.4925 4.844E-01 6.450E-01 9.996E-05 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CV(SD)	FORM
1	3.3047D-09	0.23897	3.3436D-09	0.06507	0.08243	1.4B27D-01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	33616	225	0	0	0	0	48	0	6	6

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) FISHN GANGEN REALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY GANLOST
 10000 0 0 0 114571 0 32820 6084 3916 0 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 1 MINUTE, 46 SECONDS.

RANDOM-3A171C30B4V7

***START BATCH 10

SOURCE DATA
 WPAVE JAVE IAVE VAVE WAVE XAVE YAVE ZAVE AGEAVE
 1.000E+04 1.00 -0.0021 0.0031 0.4982 -5.126E-01 1.146E+00 9.996E-05 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CV(SD)	FOM
1	2.9991D-09	0.17266	3.3091D 09	0.06120	0.07737	1.5070D+01

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	92914	246	0	0	0	0	0	56	0	6	6

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMSEN KRALCOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY CAMLOST
 10000 0 0 113350 0 13177 6062 3938 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 1 MINUTE, 47 SECONDS.

A.3.2 With Source Step Biasing

***START BATCH 1 RANDOM=1357980PDR97

SOURCE DATA
 YOU ARE USING THE DEFAULT VERSION OF, GIMED WHICH ASSUMES GEOMETRY AND XSPECT MEDIA ARE IDENTICAL.
 WAVE 1 WAVE 2 WAVE 3 WAVE 4 WAVE 5 WAVE 6 WAVE 7 WAVE 8 WAVE 9 WAVE 10
 1.051E+04 1.00 0.0049 0.0008 0.4940 -1.962E+00 -1.798E+00 1.001E-04 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR)		NEUTRON FLUX		CV(SD)	FOM
		FSD	ACCUMULATED RESPONSE	FSD	FSD		
1	3.6444D-09	0.14482	3.6444D-09	0.14482	0.14482	0.42367	2.2735D+01

PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

DETECTOR	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	8896	0	0	0	0	636	212	52	1	0	0

NUMBER OF COLLISIONS OF TYPE SCULL
 SOURCE SPLIT(0) FISH GAMSEN REALX(0) ALBFCO BDRYX ESCAPE F-CUT TIMEKILL R R KILL R R SURV GAMLOST
 10000 0 0 13997 0 25875 4895 5105 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 5 SECONDS.

RANDOM-CR8R9810R42B

***START BATCH 4

SOURCE DATA

WTAVE 1.00 UAVE 0.0087 VAVE -0.0100 WAVE 0.5000 XAVE 1.636E+00 YAVE 1.488E-00 ZAVE 1.001E-04 AGEAVE 0.0

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(PSD)	RESPONSES(DETECTIVE)	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CY(SD)	POM
1	2.9534D-09	0.02186	3.1261D 09	0.04334	0.40199	6.2B40D+01	

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

1	35475	0	0	0	1167	1278	255	30	890	70.0	80.0	90.0	100.0
---	-------	---	---	---	------	------	-----	----	-----	------	------	------	-------

NUMBER OF COLLISIONS OF TYPE NCOLL

SOURCE SPLIT(D) 10000 0 FISHN 0 GANGEN REALCOLL 0 ALBEDO 0 BDRYX 26247 ESCAPE 4888 R-CUT TIMEKILL R R KILL R R SURY GAMLOST 5112 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 7 SECONDS.

RANDOM- /AVEEDRADA3M

***START BATCH 6

SOURCE DATA
 WAVE 1AVE 1AVE 1AVE 1AVE 1AVE 1AVE 1AVE 1AVE 1AVE 1AVE
 9.718E+03 1.00 0.0196 0.0123 0.4962 -1.058E+00 5.241E+00 1.001E 04 0.0

PARTICLES PER CM**2 PPR SECOND

DETECTOR	BATCH RESPONSE	RESPONSE/(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CY(SD)	FORM
1	3.4362D-09	0.06156	3.1387D-09	0.02471	0.30883	9.5769D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	70879	0	0	0	0	2374	2538	1836	580	40

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GANGEN REALCOLL ALBRDO RDRYX ESCAPE E CUT TIMEKILL R R KILL R R SURY GAMLOST
 10000 0 0 143372 0 26648 4737 5263 0 0 0 0 0

TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 9 SECONDS.

***START BATCH 9 RANDOM-7AA14V712B1F

SOURCE DATA

WAVE 1.00 IAVE 0.0058 WAVE 0.0070 WAVE 0.5098 XAVE 9.696E-01 YAVE 1.667E+00 ZAVE 1.001E-04 AGRAVE 0.0
 1.064E+04

PARTICLES PER CM**2 PER SECOND

DETECTOR	BATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CV(SD)	FOM
1	2.9282D-09	0.02840	3.1153D-09	0.02233	0.30345	1.0446D+02

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	79739	0	0	0	0	2650	2863	2080	612	72

NUMBER OF COLLISIONS OF TYPE NCDLL

SOURCE SPLIT(D) 0 FISH 0 GAMGEN REALCOLL 0 ALBEDO 0 UDRYX 26042 ESCAPE 4881 R-CUT TIMEKILL R R KILL R R SURY GAMLOST 0
 10000 0 0 140324 0 26042 4881 5119 0 0 0 0

79 TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 6 SECONDS.

***START BATCH 10 RANDOM-2E3CF58136FF

SOURCE DATA
 WAVE 1.00 UAVE 0.0109 VAVE -0.0012 WAVE 0.4969 XAVE -2.111E+00 YAVE 3.172E+00 ZAVE 1.00JE-04 ACHAVE 0.0

PARTICLES PER CH**2 PER SECOND

DETECTOR	DATCH RESPONSE	RESPONSES(DETECTOR) FSD	NEUTRON FLUX ACCUMULATED RESPONSE	FSD	CY(SD)	POM
1	4.7195D-09	0.24259	3.2757D-09	0.03984	0.24139	2.9548D+01

DETECTOR PARTICLE DISTRIBUTION IN PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF CONTRIBUTIONS

0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	90.0	100.0
1	88620	0	0	0	0	2940	5474	457	387	4

NUMBER OF COLLISIONS OF TYPE NCOLL
 SOURCE SPLIT(D) FISHN GAMGPN REAICOLL ALBEDO BDRYX ESCAPE E-CUT TIMEKILL R R KILL R R SURY GAMLAST
 10000 0 0 141903 0 26173 4843 5157 0 0 0 0 0 0

80 TIME REQUIRED FOR THE PRECEDING BATCH WAS 2 MINUTES, 7 SECONDS.

Appendix B

Another Approach to the Monte Carlo Point-Estimator Concept

The usual formulation of the point-detector estimator is given by:

$$CON = W \times P_s \times P(\Omega \rightarrow \Omega') \frac{e^{-\Sigma_s r}}{r^2}, \quad (\text{B.1})$$

where W is the particle current weight, P_s the non-absorption probability, $P(\Omega \rightarrow \Omega')$ the probability per steradian of scattering into the detector direction, $e^{-\Sigma_s r}$ the probability of hitting the detector, and r the distance between the collision point and the detector position.

The approach proposed in this work is based on the fact that instead of using $P(\Omega \rightarrow \Omega')$ on a steradian basis, $P(\Omega \rightarrow \Omega')$ is interpreted in terms of a probability that the particle hits a sphere of unit cross section area placed in the detector position as shown in Figure B.1-a. This eliminates the need for the $1/r^2$ factor and the contribution becomes

$$CON = W \times P_s \times P'(\Omega \rightarrow \Omega') e^{-\Sigma_s r}. \quad (\text{B.2})$$

This is accomplished by calculating the solid angle formed by the sphere of unit cross section area at the detector position and the collision point, i.e

$$SA = \frac{1}{4\pi} \int_0^{2\pi} d\varphi \int_0^\theta \sin \theta d\theta = \frac{1}{2}(1 - \cos \theta) \quad (\text{B.3})$$

Table B.1: Comparison of the Calculated Results.

Detector	SXE	SPD	FSD	NPD	FSD
1	3.8269E-04	3.6421E-04	0.0071	3.9522E-04	0.0164
2	4.4637E-05	3.9779E-05	0.0228	4.3999E-05	0.0512
3	8.9468E-06	8.1489E-06	0.0363	8.7902E-06	0.0754
4	2.2423E-06	2.1442E-06	0.0822	2.1719E-06	0.0865
5	6.2343E-07	7.0446E-07	0.1363	7.1119E-07	0.1392
6	1.8914E-07	1.9343E-07	0.2276	1.9432E-07	0.2301
7	5.9068E-08	5.5311E-08	0.2102	5.5492E-08	0.2118
8	1.9177E-08	1.4919E-08	0.1699	1.4935E-08	0.1699
9	6.2713E-09	4.2579E-09	0.2194	4.2640E-09	0.2195
10	2.0408E-09	1.0450E-09	0.2492	1.0464E-09	0.2490

and the new probability $P'(\Omega \rightarrow \Omega')$ is given by

$$P'(\Omega \rightarrow \Omega') = 4\pi P(\Omega \rightarrow \Omega') \frac{1}{2} (1 - \cos \theta). \quad (\text{B.4})$$

The factor 4π eliminates the per steradian basis of $P(\Omega \rightarrow \Omega')$ and the angle θ is shown in Figure B.1-b.

It can be seen from Figure B.1-b that whenever r is less than r' , θ assumes the value $\pi/2$ so that the emergent particle will be normally incident to a unit area in the plane that contains the detector and the collision point and the contribution becomes simply $W/2$.

Table B.1 shows the results of the calculations for Sample Problem 1 but with the first three groups being analyzed. The results for the standard point detector estimator (SPD) were obtained using Equation B.1 with a unboundness correction scheme which uses an average contribution when particles collide within a distance of 0.5642 cm off the detector position. The calculations for Detectors 1 and 2 show a very good agreement for results with acceptable standard deviations. However, the accuracy of the new formalism (NPD) is better when compared with the results obtained with a surface crossing estimator (SXE). The results for the outer detectors, although with unacceptable standard deviations ($FSD > 0.5$), are presented to illustrate the excellent agreement between the two point detector estimators.

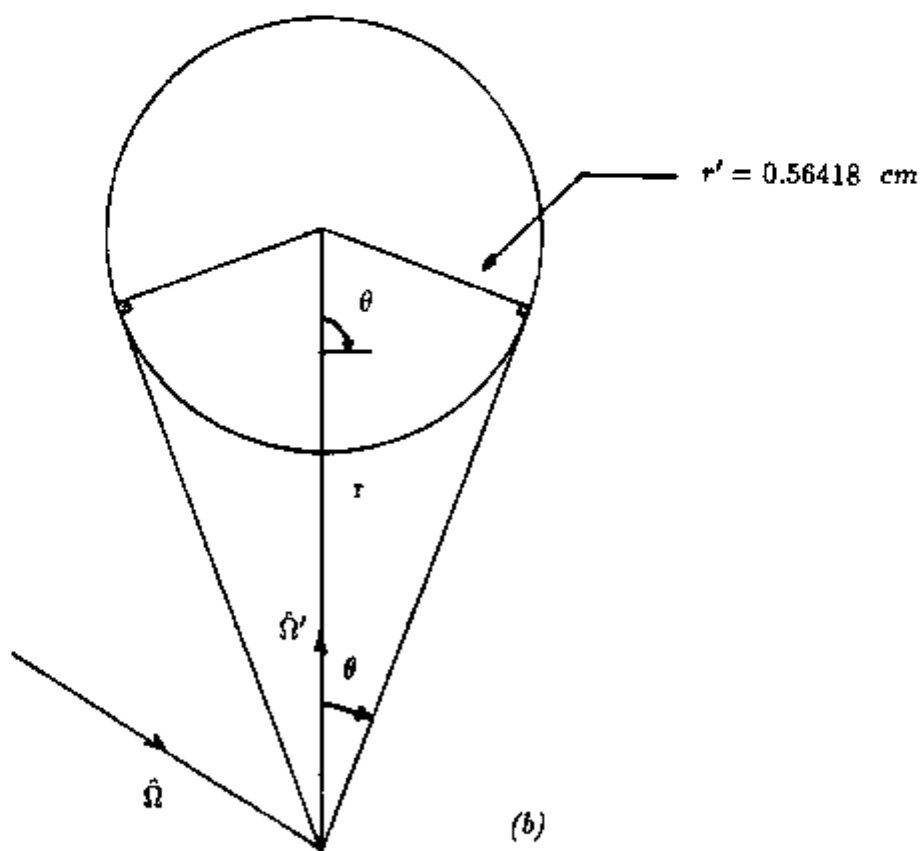
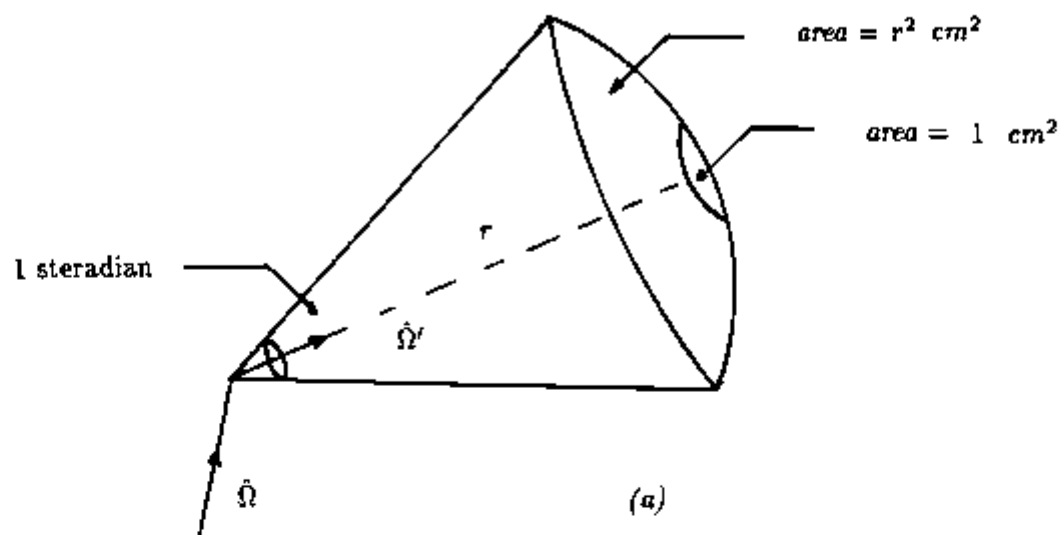


Figure B.1: Schemes of the New Point Detector Estimator.

Appendix C

Modified and Added Subroutines

The subroutines listed in this appendix are meant to be used as a guideline for the reader if he wants to implement the same modifications in his or her version of the MORSE code.

```
C**** WILSON   MAY 11, 1989 ****                                MCR 1150
C ** THIS IS THE MAIN ROUTINE * * * * *
C **
C ** THE FOLLOWING CARD DETERMINES THE SIZE ALLOWED FOR BLANK COMMON * * * * *
C ** (REGION SIZE NEEDED IS ABOUT 150K + 4*(SIZE OF BLANK COMMON IN WORDS) ) *
C ** NOTE - THE ORDER OF COMMONS IN THIS ROUTINE IS IMPORTANT AND MUST CORRES-
C ** POND TO THE ORDER USED IN DUMP ROUTINES SUCH AS HELP, ISCHLP, AND USRHP
C **
C ** LABELLED COMMONS FOR WALK ROUTINES * * * * *
    REAL * 8 SS
    COMMON NC( 50000)
    COMMON /APOLLO/ AGSTRT,DDF,DEADWT(26),ITOUT,ITIN
    COMMON /FISBTK/ MFISTP
    COMMON /EUTRON/ NAME
C **
C ** LABELLED COMMONS FOR CROSS-SECTION ROUTINES * * * * *
    COMMON /LOCSIG/ ISCCOG
    COMMON /NEARS/ RN
    COMMON /MOMENT/ NMDM
    COMMON /QAL/ Q
    COMMON /RESULT/ POINT
C **
C ** LABELLED COMMONS FOR GEOMETRY INTERFACE ROUTINES * * * * *
    COMMON /NORMAL/ UNORM
C **
C ** LABELLED COMMONS FOR USER ROUTINES * * * * *
    COMMON /PDET/ ND
    COMMON /USER/ AGST
C **
C ** COMMON /DUMMY/ WILL NOT BE FOUND ELSEWHERE IN THE PROGRAM * * *
    COMMON /DUMMY/ DUM
    COMMON /SSS/ SS(1000)
C **
    DATA JUNK/Z48484848/
```

```

NLFT = (LOC(DUM) - LOC(NC(1)))/4
DO 10 I=1,NLFT
10 NC(I) = JUNK
ITOUT = 6
ITIN = 6
NLFT = (LOC(AGSTRT) - LOC(NC(1)))/4
CALL MORSE(NLFT)
STOP
END
SUBROUTINE RELCOL                                RELCO 10
C * * THIS VERSION IS FOR USE WITH MORSE-CGA * * * * *
C                                                    RELCO 20
C THIS VERSION IS FOR POINT DETECTORS LOCATED AT (XD,YD,ZD) RELCO 30
C                                                    RELCO 40
COMMON /USER/ AGSTAT,WTSTRT,XSTRT,YSTRT,ZSTRT,DFP,EBOTM,EBOTG, RELCO 50
1 TCUT,IO,I1,IADJM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTW,NITS,MLAST, RELCO 51
2 NLEFT,NMGP,NMTG,NSTRT RELCO 52
COMMON /PDET/ ND,NNE,NE,NT,NA,NRESP,NEI,NEIND,NEHD,NDR,NTR,NTE, RELCO 60
1 NAME,NTMONR,NTWHD,NAWHD,LOCASP,LOCID,LOCIB,LOCCD,LOCT,LOCUD, RELCO 61
2 LOCSD,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EFIRST,EGTOP RELCO 62
COMMON /NEUTRON/ NAME,NAMEX,IG,IGO,NMED,MEOLD,NREG,U,V,W,UOLD,VOLD,RELCO 70
1 ,WOLD,K,Y,Z,XOLD,YOLD,ZOLD,WATE,OLDWT,WTBC,BLZBT,BLZON,AGE,OLDAGERELCO 71
COMMON BL(I) RELCO 80
DIMENSION BL(1) RELCO 90
EQUIVALENCE (BL(1),NL(1)) RELCO 100
DATA NEST /1/, FNEST /1./ RELCO 110

C NEST + FNEST ARE THE NO. OF ESTIMATES TO BE MADE TO EACH DETECTOR RELCO 130
C * * * ISTAT MUST BE EQUAL TO 1. * * *
C * * * NEI MUST BE AT LEAST 1 * * *
C * * * NEIND MUST BE AT LEAST 1 * * *
DO 30 I=1,ND RELCO 160
IA=LOCID+I RELCO 170
KE = BL(IA) RELCO 180
YE = BL(IA+ND) RELCO 190
ZE = BL(IA+2*ND) RELCO 200
C * * PTPT CALCULATES DISTANCE TO DETECTOR USING GLOBAL COORD. * *
CALL PTPT(XE,YE,ZE,A,B,C,THETA,BL,BL)
C A = XE - X - CALCULATED IN PTPT * * RELCO 210
C B = YE - Y - CALCULATED IN PTPT * * RELCO 220
C C = ZE - Z - CALCULATED IN PTPT * * RELCO 230
SD2=A*A+B*B+C*C RELCO 240
DS=SQRT (SD2) RELCO 250
C * * * COS DEPENDS ON THE ANGLE OF INTEREST * * *
COS=C/DS RELCO 270
C THETA = (A*UOLD + B*VOLD + C*WOLD)/DS RELCO 280
IGOLD = IGO RELCO 290
IGQ = NGPQT3 RELCO 300
IF (IGO.LE.NGPQT1) IGQ=NGPQT1 RELCO 310
IA = LOCASP + NRESP*NMTG + 1 RELCO 320
CALL PTHETA(NMED,IGOLD,IGQ,THETA,BL(IA),NMTG) RELCO 330
NES = 0 RELCO 340

```



```

C      NIBATCH      "
C      NIPART      ADDED
C      NINPRI      ADDED
C      - NIBRUN    MODIFIED
C      OUTPT       MODIFIED
C      SCORIN      "
C      STBTCH      "
C      STPART      ADDED
C      VAR2        MODIFIED
C      VAR3        MODIFIED
C      VAR4        ADDED
C
C
C
C*****
SUBROUTINE FLUXST(I, IGE, FLUX, AGE, CDS, SWITCH)
REAL * 8 SS, SCORE, FLUX
INTEGER*4 SWITCH
C * * SWITCH = 1 -- STORE IN ALL RELEVANT ARRAYS
C * * SWITCH = 0 -- STORE IN ALL RELEVANT ARRAYS EXCEPT UD
C * * SWITCH = -1 -- STORE IN ARRAY UD ONLY
COMMON /USER/ AGSTRT, WTSTRT, ISTRT, YSTRT, ZSTRT, DFF, EBOTW, EBOTG,
1 TCUT, IO, I1, IADJM, NGPQT1, NGPQT2, NGPQT3, NGPQTG, NGPQTW, NITS, NLAST,
2 NLEFT, NMGF, NMTG, NSTRT
COMMON /PDET/ ND, NNE, NE, NT, NA, NRESP, NEX, NREND, NEND, NDWR, NTR, NTNE,
1 NAME, NTNDR, NTNEND, NANEND, LOCRSP, LOCXD, LOCIB, LOCCO, LOCT, LOCUD,
2 LOCSO, LOCQE, LOCQT, LOCQTE, LOCQAE, LMAX, EFIRST, EGTOP
COMMON BC(1)
COMMON /SSS/ SS(1)
DIMENSION BC(1)
EQUIVALENCE (BC(1), NC(1))
DATA K/1/
IF (IGE.GT.NMTG) GO TO 40
IF (SWITCH) 170, 10, 10
10 IF (NE) 60, 60, 20
20 J=NC(LOCIB+3*NE+IGE)
IF (J.LE.0) RETURN
50 IB = LOCQE + (I-1)*NE + J
SS(IB) = SS(IB) + FLUX
60 IF (NT) 90, 90, 70
70 IA = LOCT + (I-1)*NT + 1
DO 80 K=1, NT
IF (AGE-BC(IA)) 90, 90, 80
80 IA = IA + 1

K = NT
IA=IA-1
BC(IA)=AGE
IDT = LOCT + (ND+I)*NT
BC(IDT) = BC(IA) - BC(IA-1)
90 IF (NA) 120, 120, 100
100 IA = LOCCD + 1

```

	DO 110 L=1,NA	FLUX 330
	IF (COS-BC(IA)) 120,120,110	FLUX 340
110	IA = IA + 1	FLUX 350
40	CALL HELP(4HFYST,1,1,-1,1)	FLUX 160
	CALL ERRDR	FLUX 190
120	IF (NE) 170,170,130	FLUX 370
130	IF (NT) 150,150,140	FLUX 380
140	ID = LOCQTE + (I-1)*NTNE + (J-1)*NT + K	FLUX 390
	SS(ID) = SS(ID) + FLUX	FLUX 400
150	IF (NA) 170,170,160	FLUX 410
160	IE = LOCQAE + (I-1)*NAWE + (J-1)*NA + L	FLUX 420
	SS(IE) = SS(IE) + FLUX	FLUX 430
170	IS = (I-1)*NRESP + 1	FLUX 440
	IU = LOCUD + IS	FLUX 450
	IS = LOCSO + IS	FLUX 460
C****	WILSON MAY 11, 1989 ****	MOR 1150
	IW = LOCSO + (I-1)*NRESP + 3*MDNR + 1	FLUX 480
	IC = LOCQT + (I-1)*NTR + (K-1)*NRESP + 1	FLUX 470
	IB = LDCRSP + IGE - NMTG	FLUX 480
	DO 220 IR = 1,NRESP	FLUX 490
	IB = IB + NMTG	FLUX 500
	SCORE = FLUX*BC(IB)	FLUX 510
	IF (SWITCH) 180,200,180	FLUX 520
180	SS(IU) = SS(IU) + SCORE	FLUX 530
	IU = IU + 1	FLUX 540
190	IF (SWITCH) 220,200,200	FLUX 550
200	SS(IS) = SS(IS) + SCORE	FLUX 560
	SS(IW) = SS(IW) + SCORE	FLUX 560
	IS = IS + 1	FLUX 570
	IW = IW + 1	FLUX 570
C****	WILSON MAY 11, 1989 ****	MOR 1150
	IF (NT) 220,220,210	FLUX 580
210	SS(IC) = SS(IC) + SCORE	FLUX 590
	IC = IC + 1	FLUX 600
220	CONTINUE	FLUX 610
	RETURN	FLUX 620
	END	FLUX 630
	SUBROUTINE GSTORE(WBG,IGG)	GSTOR 10
C * *	THIS VERSION OF GSTORE IS FOR MORSE-CGA * * * *	
C	THIS ROUTINE CHECKS TO SEE IF THERE IS ROOM IN THE BANK AND IF SO GSTOR *	
C	STORES DATA FOR THE GENERATED GAMMA	GSTOR *
C	IT ASSUMES THAT THE GAMMA IS EMITTED UNIFORMLY IN DIRECTION	GSTOR *
	COMMON /NUTRON/ NAKE,NAKEX,IG,IGO,IMED,MEOLD,NREG,U,V,W,UOLD,VOLDGSTOR 20	
1	,WOLD,X,Y,Z,XOLD,YOLD,ZOLD,WATE,OLDWT,WTBC,BLZFT,BLZON,AGE,OLDAGEGSTOR 21	
	COMMON /APOLLO/ AGSTRT,DDF,DEADWT(5),ETA,ETATH,ETAUSD,VINP,VINP, GSTOR 30	
1	VINP,WTSTRT,XSTRT,YSTRT,ZSTRT,TCUT,ITRA(10),	GSTOR 31
2	IO,I1,MEDIA,IADJN,ISBIAS,ISOUR,ITERS,ITIME,ITSTR,LOCWTS,LOCFWL,GSTOR 32	
3	LOCEPR,LOCNSC,LOCPSN,MAXGP,MAXTIM,MEALB,MGPREG,MXREG,WALB, GSTOR 33	
4	NHEAD(5),NEWMN,MGEOM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTE,NITS, GSTOR 34	
5	NKCALC,NKILL,NLAST,NMEM,NMGP,NMOST,NMTG,NOLEAK,NORMF,NPAST, GSTOR 35	
6	NPSCL(13),NQUIT,NSIGL,NSOUR,NSPLT,NSTRT,NXTRA(10)	GSTOR 36

```

C**** WILSON   MAY 11, 1989 ****                                NOR 1150

      COMMON /NS/ NS                                           GSTOR 40
C**** WILSON   MAY 11, 1989 ****                                NOR 1150
      COMMON BC(1)                                             GSTOR 40
      DIMENSION NC(1)                                          GSTOR 50
      EQUIVALENCE (BC(1),NC(1))                                GSTOR 60
      IF (NROST-NS) 10,10,15                                    GSTOR 70
10  IF (NPSCL(13) .EQ. 0) WRITE (10,1010)                      GSTOR 80
1010 FORMAT ('WARNING * * * NO ROOM IN BANK FOR SECONDARIES * * * '/') GSTOR 90
      NPSCL(13) = NPSCL(13) + 1                                GSTO 100
      RETURN                                                    GSTO 110
15  NS = NS + 1                                               GSTO 120
      NEWNH = NEWNH + 1                                         GSTO 130
      NNS = NNS + 1                                             GSTO 140
      WTS = WATE                                                 GSTO 150
      IGS = IG                                                   GSTO 160
      NAME = NEWNH                                               GSTO 170
      WATE = WBG                                                 GSTO 180
      IG = IGG                                                  GSTO 190
      US=0                                                       GSTO 200
      VS=V                                                       GSTO 210
      WS=W                                                       GSTO 220
      CALL GTISD(U,V,W)                                          GSTO 230
      CALL STORNT(NS,0)                                          GSTO 240
C  CALL BANKR(4) FOR GAMMA GENERATION ANALYSIS                 * * * *
      CALL BANKR(4)                                             GSTO 245
      NAME = NNS                                                 GSTO 250
      WATE = WTS                                                 GSTO 260
      IG = IGS                                                  GSTO 270
      U=US                                                       GSTO 280
      V=VS                                                       GSTO 290
      W=WS                                                       GSTO 300
      ISCT = LOCNSC + 5*NMTG*NIREG + (NIREG-1)*NMTG + IG      GSTO 310
      NC(ISCT) = NC(ISCT) + 1                                    GSTO 320
      ISCT = ISCT + IGG - IG                                     GSTO 330
      NC(ISCT) = NC(ISCT) + 1                                    GSTO 340
      ISCT = ISCT + NMTG*NIREG                                  GSTO 350
      BC(ISCT) = BC(ISCT) + WBG                                  GSTO 360
      ISCT = ISCT + IG - IGG                                    GSTO 370
      BC(ISCT) = BC(ISCT) + WATE                                 GSTO 380
      NPSCL(4) = NPSCL(4) + 1                                    GSTO 390
      RETURN                                                    GSTO 410
      END                                                        GSTO 420
      SUBROUTINE INPUT1
C * * THIS VERSION OF INPUT1 IS FOR MORSE-CGA * * *
C  THIS ROUTINE READS THE RANDOM WALK DATA AND CALLS ROUTINES TO READ * * * *
C  SOURCE DATA AND GEOMETRY DATA.      INITIALIZES SOME VARIABLES * * * *

C**** WILSON   MAY 11, 1989 ****                                NOR 1150
1041 FORMAT (2I,16,9I5,F5.0,2I5)

```

```

1040 FORMAT (10I6,F8.0,2I5)
C**** WILSON MAY 11, 1989 **** MOR 1150
WRITE(10,1050)NSTRT,NMOST,NITS,NQUIT,NGPQTN,NGPQTG,WMGP,WNTG,WCOLTIPU 860
1P,IADJM,AXTIM,MEDIA,MEDALB INPU
1060 FORMAT('0',3X,'NSTRT',3X,'NMOST',4X,'NITS',3X,'NQUIT',2X, INPU
1'NGPQTN',2X,'NGPQTG',4X,'WMGP',4X,'WNTG',2X,'WCOLTP',3X,'IADJM' INPU
2,2X,'MAXTIM',3X,'MEDIA',2X,'MEDALB',/1X,10I8,F8.2,2I8) INPU

SUBROUTINE MORSE(NLFT) MORSE 10
C THIS IS THE EXECUTIVE ROUTINE FOR THE RANDOM WALK PROCESS * * * MORSE *

C IT CONTROLS THE SUCCESSION OF EVENTS WHICH COMPRISE THE MORSE *
C * * MONTE CARLO PROCESS * * * * * MORSE *
C **** THIS VERSION OF SUBROUTINE MORSE KILLS JOBS ON IO REQUESTS*****
C *** THIS VERSION OF MORSE IS FOR MORSE-CGA * * * *

REAL*8 RANDDM, SS MORSE 15
COMMON /APOLLO/ AGSTRT,DOF,DEADWT(6),ETA,ETATH,ETAUSD,UINP,VIMP, MORSE 20
1 WIMP,WTSTRT,XSTRT,YSTRT,ZSTRT,TCUT,XTRA(10), MORSE 21
2 IO,I1,MEDIA,IADJM,ISBIAS,ISOUR,ITERS,ITIME,ITSTR,LOCWTS,LOCFWL,MORSE 22
3 LOCEPR,LOCWSC,LOCPSH,MAXGP,MAXTIM,MEDALB,NGPREG,MXREG,WALB, MORSE 23
4 WDEAD(6),NEWNM,NGEOM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTN,NITS, MORSE 24
5 NKCALC,NKILL,WLAST,WHEM,WNGP,WNMOST,WNTG,WOLEAK,WORMF,WFAST, MORSE 25
6 WPSCL(13),NQUIT,NSIGL,YSOUR,WSPLT,WSTRT,WITRA(10) MORSE 26
COMMON /PDET/ ND,NE,WE,WT,WA,WRESP,WEX,WKIND,WEND,WDRR,WTR,WTNE,
1 WANE,WTHDR,WTHEND,WANEND,LOCNSP,LOCXD,LOCIB,LOCCD,LOCT,LOCUD,
2 LOCSD,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EFIRST,EGTOP
COMMON /NUTRON/ NAME,WANEX,IG,IGO,WMED,MEDOLD,WREG,U,V,W,UOLD,VOLDMORSE 30
1 ,VOLD,X,Y,Z,WOLD,YOLD,ZOLD,WATE,OLDWT,WTRC,BLZET,BLZON,AGE,OLDAGEMORSE 31
COMMON /FISBK/ WFISTP,WFISB,WFISH,FTOTL,FWATE,WATEF MORSE 40
C**** WILSON MAY 11, 1989 **** MOR 1150
COMMON /NS/ NS GSTOR 40
COMMON /SSS/ SS(1) GSTOR 40
COMMON /OUTB/ SWATE,XAVE,YAVE,ZAVE,EAVE,UAVE,WAVE,AGEAVE GSTOR 40
C**** WILSON MAY 11, 1989 **** MOR 1150
DIMENSION WTS(1) MORSE 50
COMMON WTS(1) MORSE 60
EQUIVALENCE(WTS(1),NITS(1)) MORSE 70
CALL MSGR(IG) MORS
C BEGIN NEW PROBLEM MORSE 80
10 WLAST=NLFT MORSE 80
CALL TIMER(-2,ITRA) MORS 100
WXT = ICLOCK(0) MORS 110
CALL INPUT MORS 120
C READS CARDS A THRU D - CALLS SORIN FOR CARDS E IF ISOUR .LE. ZERO 140
C READS CARDS F THRU Q - CALLS JWIN, ISEC AND SCORIN MORS 150
CALL IOLEFT(NIO)
C ** A DUMMY IOLEFT IS PROVIDED FOR SITES NOT HAVING THIS CAPABILITY*
C NIO IS TOTAL NO. IO'S LEFT AFTER INPUT ROUTINES FINISH
WRITE(10,1001) NIO
1001 FORMAT(1X,'NUMBER OF IO REQUESTS LEFT AFTER INPUT IS ',I10)
NIOB=NIO
NIO=0

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	ISIG=1	
	WTSTW=#KILL+#SPLT	MORS 150
	NGPREG = NMTG+MIREG	MORS 160
	XTRA(6) = NGPREG	
	NCOMB = NGPQTW+NGPQTG	MORS 170
	IA = LOCFWL + 1	MORS 180
	IU = LOCFWL + MIREG	MORS 190
	DO 15 I=IA,IU	MORS 200
	IB = I + MIREG	MORS 210
15	WTS(IB) = WTS(I)	MORS 220
	IAW = LOCWTS + 1	MORS 230
	IUW = LOCWTS + 3+NGPREG	MORS 240
	DO 20 I=IAW,IUW	MORS 250
	IB = I + 12+NGPREG	MORS 260
20	WTS(IB) = WTS(I)	MORS 270
	INITS = NITS	MORS 280
	IRUNS = NQUIT	
	INDX=0	
	CALL TIMER(INDX,XTRA)	MORS 310
	WRITE (IO,1010) (XTRA(I),I=1,INDX)	MORS 320
	1010 FORMAT (29H0TIME REQUIRED FOR INPUT WAS ,10A4)	MORS 330
C	BEGIN NEW RUN	MORS 320
25	NITS = INITS	MORS 350
	CALL BANKR(-1)	MORS 360
	DO 30 I=IA,IU	MORS 370
	IB = I + MIREG	MORS 380
30	WTS(I) = WTS(IB)	MORS 390
	DO 35 I=IAW,IUW	MORS 400
	IB = I + 12+NGPREG	MORS 410
35	WTS(I) = WTS(IB)	MORS 420
	ITERS=NITS	MORS 430
	ITSTR=0	MORS 440
C****	WILSON APRIL 19,1989 ****	MOR 1150
	ITIMEI=ICLOCK(0)	MORS 470
C	BEGIN NEW BATCH	MORS 420
40	NMEM=NSTRT	MORS 460
	SWATE=0.	OUTP 220
	XAVE=0.	OUTP 230
	YAVE=0.	OUTP 240
	ZAVE=0.	OUTP 250
	UAVE=0.	OUTP 260
	VAVE=0.	OUTP 270
	WAVE=0.	OUTP 280
	AGEAVE=0.	OUTP 290
	EAVE=0.	OUTP 300
C****	WILSON APRIL 19,1989 ****	MOR 1150
	IF (ITSTR) 45,50,45	MORS 470
45	NMEM = NFISH	MORS 480
50	CALL BANKR(-2)	MORS 490
C	CALLS STBTCH	* * * *
	NBATCH=NITS-ITERS+1	MORS 500

CALL RNDOUT(RANDOM)	MORS 601
WRITE (10,1015) NBTACH,RANDOM	MORS 602
1015 FORMAT (15H1***START BATCH ,I4,25X,7HRANDOM=,Z12/12HOSOURCE DATA)	MORS 603
60 CALL MSOUR	MORS 610
C BEGIN NEW HISTORY	MORS 610
NS = 1	
NMEM = NMEM - 1	MORS 660
61 CALL GETWT(NS,1)	MORS 650
NS = NS - 1	MORS 660
NALB = 0	MORS 670
NGPQT = NGPQT1	MORS 680
65 IF (WATE) 70,165,70	MORS 690
70 IF(IG-NGPQT)90,90,75	MORS 600
75 IF(IG-NGPQT2)160,160,90	MORS 610
80 IF(IG-NGPQT3)85,85,160	MORS 620
85 NGPQT=NGPQT3	MORS 630
90 IGO=IG	MORS 640
UOLD=U	MORS 650
VOLD=V	MORS 660
WOLD=W	MORS 670
OLDWT=WATE	MORS 680
XOLD=X	MORS 690
YOLD=Y	MORS 700
ZOLD=Z	MORS 710
BLZON=BLZNT	MORS 720
NEDOLD=NKED	MORS 730
OLDAGE=AGE	MORS 740
IF(WTSTW.GT.0) CALL TESTW	MORS 750
IF(WATE)100,95,100	MORS 760
95 NDEAD(1)=NDEAD(1)+1	MORS 770
DEADWT(1)=DEADWT(1)+OLDWT	MORS 780
C R R KILL	MORS 750
GO TO 165	MORS 800
100 CALL WITCOL	MORS 810
IF (WREG-MXREG) 102,102,101	MORS
101 WRITE (10,1016) WREG,MXREG	MORS
1016 FORMAT (6HWRREG=,I5,8H, MXREG=,I5,61H, MXREG ON CARD I MUST BE GENMORS	
1 TO THE NUMBER OF REGIONS DESCRIBED IN GEOMETRY INPUT)	MORS
CALL EXIT	MORS
102 IF (TCUT.LE.0..OR.AGE.LT.TCUT) GO TO 110	MORS
NDEAD(4)=NDEAD(4) +1	MORS 840
DEADWT(4) =DEADWT(4)+OLDWT	MORS 850
C AGE KILL	MORS 820
NPSCL(10) = NPSCL(10) + 1	MORS 870
C CALL BANKR(10) FOR TIME-KILL ANALYSIS	MORS 840
GO TO 165	MORS 890
110 IF(WATE)120,115,120	MORS 900
115 NDEAD(2)=NDEAD(2)+1	MORS 910
DEADWT(2)=DEADWT(2)+WTBC	MORS 920
C ESCAPE	MORS 890
GO TO 165	MORS 940

120	IF(WALB)130,130,126	NORS 950
125	ISCT = LOCNSC + 2*WGPREG + (WREG-1)*WMTG + IG	NORS 960
	WTS(ISCT) = WTS(ISCT) + 1	NORS 970
	ISCT = ISCT + WGPREG	NORS 980
	WTS(ISCT) = WTS(ISCT) + WATE	NORS 990
	CALL ALBDO(IG,U,V,W,WATE,WMED,WREG)	NOR 1000
	WPSCL(6) = WPSCL(6) + 1	NOR 1010
	CALL BANKR(6)	NOR 1020
	GO TO 65	NOR 1030
130	CALL GTMED(WMED,IMED)	NOR 1040
	IF (MFISTP) 140,140,135	NOR 1050
135	IF (WTS(LOCFSH+(IMED-1)*WMTG+IG)) 140,140,136	NORS
136	CALL FPROB	NORS
140	IF (WCONB) 155,155,145	NOR 1070
145	IF(WTS(LOCFSH+(2*MEDIA+IMED-1)*WMTG+IG))155,155,150	NOR 1080
150	CALL GPROB	NOR 1090
C		NOR 1020
155	ISCT = LOCNSC + (WREG-1)*WMTG + IG	NOR 1110
	WTS(ISCT) = WTS(ISCT) + 1	NOR 1120
	ISCT = ISCT + WGPREG	NOR 1130
	WTS(ISCT) = WTS(ISCT) + WATE	NOR 1140
	ISCT = LOCNSC + 8*WGPREG + IMED	NOR 1150
	WTS(ISCT) = WTS(ISCT) + 1	NOR 1160
	CALL COLISH(IG,U,V,W,WATE,WMED,WREG)	NOR 1170
C		NOR 1060
	WPSCL(5) = WPSCL(5) + 1	NOR 1180
	CALL BANKR(5)	NOR 1200
C	CALLS BELCOL	NOR 1090
	GO TO 65	NOR 1220
160	WDEAD(3)=WDEAD(3)+1	NOR 1230
	DEADWT(3)=DEADWT(3)+WATE	NOR 1240
	WPSCL(9) = WPSCL(9) + 1	NOR 1250
C	CALL BANKR(9) FOR E-CUT ANALYSIS	NOR 1140
C	ENERGY CUTOFF	NOR 1150
C****	WILSON APRIL 18,1989 ****	NOR 1150
165	IF (NS.GT.0) GO TO 61	NOR 1280
	CALL NPART	NOR 1280
	CALL STPART	NOR 1280
	IF (WHEM) 170,170,60	NOR 1280
C****	WILSON APRIL 18,1989 ****	NOR 1150
C	END OF HISTORY	NOR 1170
170	CALL BANKR(-3)	NOR 1300
C	CALLS WBTCH	NOR 1190
C****	WILSON APRIL 18,1989 ****	NOR 1150
	IF (ITERS) 195,195,55	NORS 520
55	CALL OUTPT(1)	NORS 530
	CALL WNPRI(ITIMEI,WBTCH)	NOR 1410
C****	WILSON APRIL 18,1989 ****	NOR 1150
	CALL OUTPT(2)	NOR 1320
	IF(ICLOCK(0)-MIT-MAXTIM) 181,181,175	NOR 1330
181	CALL IOLEFT(WIO)	NOR


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C   NIO IS NO. IO'S LEFT AFTER CURRENT BATCH COMPLETED      MOR
      NIOB=NIOB-NIO      MOR
C   NIOB IS NO. IO'S IN BATCH JUST COMPLETED      MOR
      IF(NIOB.GT.NTIO) NTIO=NIOB      MOR
      IF(NIO.GT.NTIO) GO TO 180      MOR
      ISIG=2      MOR
175  NITS = NITS - ITERS + 1      MOR 1340
      ITERS = 0      MOR 1350
      NQUIT = NQUIT - IRUNS      MOR 1360
      IRUNS = -NQUIT      MOR 1370
      IF(ISIG.EQ.1) WRITE(IO,1020) IRUNS,INITS,NITS
1020 FORMAT(1H0/39HORUN TERMINATED BY EXECUTION TIME LIMIT      MOR 1390
      1 /18,8H RUNS OF,13,8H BATCHES,16H AND 1 RUN MOR 1391
      20F,13,19H BATCHES COMPLETED./)      MOR 1392
      IF(ISIG.EQ.2) WRITE(IO,1050) IRUNS,INITS,NITS      MOR
1050 FORMAT(1H0/39HORUN TERMINATED BY LIMIT ON IO      MOR
      1 /18,8H RUNS OF,13,8H BATCHES,16H AND 1 RUN MOR
      20F,13,19H BATCHES COMPLETED./)      MOR
180  ITERS = ITERS - 1      MOR 1400
      IF(ITERS)195,195,185      MOR 1410
185  IF(NSOUR)40,40,190      MOR 1420
190  ITSTR=1      MOR 1430
C   END OF BATCH      MOR 1320
      GO TO 40      MOR 1450
195  CALL BANKR(-4)      MOR 1450
C   CALLS WRUN      MOR 1350
      NQUIT=NQUIT-1      MOR 1480
      INDX = -1      MOR 1490
      CALL TIMER(INDX,XTRA)      MOR 1500
      WRITE (IO,1030) NITS,(XTRA(I),I=1,INDX)      MOR 1510
1030 FORMAT (32H0TIME REQUIRED FOR THE PRECEDING,14,13H BATCHES WAS ,10MOR 1520
      1A4)      MOR 1521
      CALL TIMER(-2,XTRA)      MOR 1530
C   END OF NITS BATCHES      MOR 1370
      IF (NQUIT) 200,200,25      MOR 1550
200  CALL OUTPT(3)      MOR 1560
C   END OF RUN      MOR 1400
      FTIME = ICLOCK(0) - NKT      MOR 1580
      FTIME=FTIME/8000.      MOR 1590
      WRITE(IO,1040) FTIME      MOR 1600
1040 FORMAT (37H0TOTAL CPU TIME FOR THIS PROBLEM WAS ,F6.2,9H MINUTES.)MOR 1610
      GO TO 10      MOR 1620
      END      MOR 1630

      SUBROUTINE MSOUR      MS000100
C      * * * * *
C   THIS IS THE EXECUTIVE ROUTINE FOR THE GENERATION AND STORAGE OF MSOUR *
C   SOURCE PARAMETERS AT THE START OF EACH BATCH *      MSOUR *
C * * * * *
C *** THIS VERSION OF MSOUR IS DESIGNED FOR THE COMBGEOM PKG WITH MARS MSOUR *
      REAL*8 IDUM,DIST,UDUM
      COMMON /FISBKK/ MFISTP,RFISBN,RFISE,PTOTL,FWATE,WATEP      MS000200

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COMMON /NUTRON/ NAME,NAMEX,IG,IGO,WMED,WMEDOLD,WREG,U,V,W,UOLD,VOLDMS000300
1 ,WOLD,X,Y,Z,WOLD,YOLD,ZOLD,WATE,OLDWT,WTBC,BLZWT,BLZOM,AGE,OLDAGENMS000400
COMMON /APOLLO/ AGSTRT,DDF,DEADWT(5),ETA,ETATE,ETAUSD,UINP,VINP, MS000500
1 WIMP,WTSTRT,ISTRT,YSTRT,ZSTRT,TCUT,XTRA(10), MS000600
2 IO,I1,MEDIA,IADJM,ISBIAS,ISOUR,ITERS,ITIME,ITSTR,LOCWTS,LOCFWL,MS000700
3 LOCEPR,LOCESC,LOCFSM,MAKGP,MAITM,MEDALS,MGPREG,MIREG,WALB, MS000800
4 NDEAD(5),NEWEM,NGEOM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTE,WITS, MS000900
5 NKCALC,NKILL,NLAST,NMEM,NMGP,NMOST,NMTG,NOLEAK,NORMF,NPAST, MS001000
6 NPSC(19),NQUT,NSIGL,NSOUR,NSPLT,NSTRT,NXTRA(10) MS001100
COMMON/GONLOC/ KMA,KFPD,KLCR,KNSD,KIOR,KRIZ,KACZ,KNIZ,KMCZ, MS001300
1 KKR1,KKR2,KNSR,KVOL,WADD,LDATA,LTMA,LFPD,NUMR,IRTRU,NUMB,NIR MS001400
2 ,KBIZ,KBCZ MS00
COMMON /ORGI/ DIST ,MARK,WMEDG,WBLZ MS00
COMMON/ARAB/EBY,BLEV,NAR,NQ,IAY,IAY,NF,NX1(3) MS00
COMMON/REPEAT/ JP(20) MS00
COMMON /KGMV/ MUS,MUZ,LL,IPRET,IFLOW,IECT,NLD,IGX MS00
COMMON /OUTB/ SWATE,XAVE,YAVE,ZAVE,EAVE,UAVE,VAVE,WAVE,AGEAVE GSTOR 40
COMMON ESTOR(1) MS001500
DIMENSION IDUM(3),UDUM(3) MS00
INTEGER BLZWT MS001600
VOLD=0. MS001700
YOLD=0. MS001800
WOLD=0. MS001900
ETA=0. MS002000
XOLD=0. MS002100
YOLD=0. MS002200
ZOLD=0. MS002300
BLZOM=0. MS002400
OLDWT=WTSTRT MS002500
ETA=0. MS002600
IGO=0 MS002700
WMEDOLD=0. MS002800
OLDAGE=0. MS002900
WATE=WTSTRT MS003700
I=ISTRT MS003800
Y=YSTRT MS003900
Z=ZSTRT MS004000
AGE=AGSTRT MS004100
NAMEX=1 MS004200
CALL SOURCE(IG,UINP,VINP,WIMP,I,Y,Z,WATE,WMED,AGE,ISOUR,ITSTR,MGP MS004300
1QTS,DDF,ISBIAS,NMTG) MS004400
C *** DEFINE SOURCE ANGLE BEFORE CALLING CALI - LOOKZ ** MS004500
IF(ABS(UINP)+ABS(VINP)+ABS(WIMP)) 35,35,30 MS005400
30 U1=UINP MS005500
V1=VINP MS005600
W1=WIMP MS005700
GO TO 40 MS005800
35 CALL GTISO(U1,V1,W1) MS005900
C SELECT ISOTROPIC DIRECTION COSINES * * MS006000
40 U=U1 MS006000
V=V1 MS006100

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W=W1	MS006200
UDUM(1)=U	MS004600
UDUM(2)=V	MS004800
UDUM(3)=W	MS004700
XDUM(1)=X	MS004600
XDUM(2)=Y	MS004600
XDUM(3)=Z	MS004700
NI1 = 6*NLEV+4	MS00
IF(NLEV.LE.0) GO TO 110	MS00
DO 100 I=1,NI1	MS00
IX1 = JP(12)+I-1	MS00
100 NSTOR(IX1) = 0	MS00
110 CONTINUE	MS00
JP4 = JP(4)	MS00
JP5 = JP(5)	MS00
JP7 = JP(7)	MS00
JP8 = JP(8)	MS00
JPD = JP(10)	MS00
LL = 0	MS00
JL = 0	MS00
JLU = 0	MS00
C SUBROUTINE CALI WILL CALL LOOKZ	MS00
C THIS CALL TO LOOKZ CORRESPONDS TO THE COMBGEOM VERSION OF LOOKZ	MSOUR *
CALL CALI(JL,JLU,XDUM,UDUM,JP,NSTOR(JP4),NSTOR(JP5),NSTOR(JP7),	MS004800
1 NSTOR(JP8),NSTOR(JPD),NSTOR(KFPD),NSTOR(KNA),NSTOR(KLGR),	MS004800
. NSTOR,NSTOR)	MS004900
BLZNT=NBLZ	MS00
NREG=NSTOR(KRIZ+NMEDG-1)	MS005100
NMED=NSTOR(KMIZ+NMEDG-1)	MS005200
NAME=1	MS005300
IF(ISOUR)50,50,45	MS006300
45 IG=ISOUR	MS006400
50 CALL STORNT(1,0)	MS006500
C PLACE SOURCE PARAMETERS IN PARTICLE BANK * *	MSOUR *
NPSCL(1) = NPSCL(1) + 1	MS006600
C ** PARTICLE POSITION MUST BE IN LOCAL COORDINATES WHEN SDATA CALLED *	MS00
C ** GETNT SELECTS X,Y,Z FROM BANK AND CONVERTS TO LOCAL COORD	MS00
CALL GETNT(1,1)	MS00
SWATE=SWATE+WATE	OUTP 330
XAVE=XAVE+WATE*X	OUTP 340
YAVE=YAVE+WATE*Y	OUTP 350
ZAVE=ZAVE+WATE*Z	OUTP 360
EAVE=EAVE+WATE*IG	OUTP 370
UAVE=UAVE+WATE*U	OUTP 380
VAVE=VAVE+WATE*V	OUTP 390
WAVE=WAVE+WATE*W	OUTP 400
AGEAVE=AGEAVE+WATE*AGE	OUTP 410
CALL BANKR(1)	MS006700
NEWNM=1	MS006900
RETURN	MS007300
END	MS007400

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SUBROUTINE WPART                                NBATC 10
REAL * 8 F, BC
C THIS ROUTINE IS CALLED AT THE END OF EACH HISTORY TO DO THE SUMS NBATC *
C   NEEDED FOR ESTIMATED MEANS AND FOR CALC. OF BATCH STATISTICS NBATC *
COMMON /PDET/ ND, NFE, NE, NT, NA, NRESP, NEX, NEXND, NEND, NDR, NTR, NTRN, NBATC 20
1 NAME, NTRND, NTRND, NTRND, LOCRSP, LOCKD, LOCIB, LOCCO, LOCT, LOCUD, NBATC 21
2 LOCSD, LOCQE, LOCQT, LOCQTE, LOCQAE, LMAX, EFIRST, EGTOP NBATC 22
C COMMON BC(1) NBATC 30
COMMON /FRE/ W(189), NFREQ(10, 188)
COMMON /SSS/ BC(1) NBATC 30
DIMENSION IW(9), JW(21)
DATA IW/1,2,3,4,5,6,7,8,9/, JW/~19,-18,-17,-16,-15,-14,-13,
*-12,-11,-10,-9,-8,-7,-6,-5,-4,-3,-2,-1,0,1/
DATA IFLA/0/

IF(IFLA.GT.0) GO TO 301
IFLA=1
K=0
DO 303 J=1,21
DO 302 I=1,9
K=K+1
W(K)=IW(I)*10.**JW(J)
302 CONTINUE
303 CONTINUE
301 DO 70 I=1,ND NBATC 40
IU = LOCUD+(I-1)*NRESP NBATC 50
IS = LOCSD + (I-1)*NRESP NBATC 60
IF = LOCQE + (I-1)*NE NBATC 70
IT = LOCQT + (I-1)*NTR NBATC 80
IE = LOCQTE + (I-1)*NTRN NBATC 90
IA = LOCQAE + (I-1)*NAME NBAT 100
IF (NE) 15,15,5 NBAT 110
5 DO 10 J=1,NE NBAT 120
ISUB = IF + J NBAT 130
F = BC(ISUB) NBAT 140
ISUB = ISUB + NEND NBAT 150
BC(ISUB) = BC(ISUB) + F NBAT 160
IF (DABS(F) .LT. 1.0E-35) F = 0.0 NBAT 170
ISUB = ISUB + NEND NBAT 180
10 BC(ISUB) = BC(ISUB) + F*F NBAT 190
15 DO 30 M=1,NRESP NBAT 200
C *****THIS PART FOR THE UNCOLL***** NBAT 300
ISUB = IU + M NBAT 280
F = BC(ISUB) NBAT 290
ISUB = ISUB + NDR NBAT 300
BC(ISUB) = BC(ISUB) + F NBAT 310
IF (DABS(F) .LT. 1.0E-35) F = 0.0 NBAT 320
ISUB = ISUB + NDR NBAT 330
BC(ISUB) = BC(ISUB) + F*F NBAT 340
C *****THIS PART FOR THE BATCH ***** NBAT 300
ISUB = IS + M NBAT 280
ISUB = ISUB + 3*NDR NBAT 300

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BC(ISUB) = BC(ISUB) + F                                NBAT 540
IF (DABS(F) .LT. 1.0E-35) F = 0.0                      NBAT 550
ISUB = ISUB + NTHEND                                    NBAT 560
45 BC(ISUB) = BC(ISUB) + F*F                            NBAT 570
60 IF (NA) 66,66,66                                     NBAT 580
65 DO 60 L=1,NA                                         NBAT 590
ISUB = IAE + L                                          NBAT 600
F = BC(ISUB)                                           NBAT 610
ISUB = ISUB + MANEND                                    NBAT 620
BC(ISUB) = BC(ISUB) + F                                NBAT 630
IF (DABS(F) .LT. 1.0E-35) F = 0.0                      NBAT 640
ISUB = ISUB + MANEND                                    NBAT 650
60 BC(ISUB) = BC(ISUB) + F*F                            NBAT 660
65 CONTINUE                                             NBAT 670
70 CONTINUE                                             NBAT 680
RETURN                                                  NBAT 690
END                                                    NBAT 700

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SUBROUTINE YBATCH(NSORC)                                YBATCH 10
C THIS ROUTINE IS CALLED AT THE END OF EACH BATCH TO DO THE SUMS YBATCH *
C   NEEDED FOR ESTIMATED MEANS AND FOR CALC. OF BATCH STATISTICS YBATCH *
REAL * 8 F ,BC
COMMON /PDET/ ND, NNE, NE, NT, NA, NRESP, NEX, NEXND, NEND, NDNR, NTHR, NTHE, NBATC 20
1 NANE, NTHDR, NTHEND, NANEEND, LOCRSP, LOCXD, LOCIB, LOCCO, LOCT, LOCUD, NBATC 21
2 LOCSD, LOCQE, LOCQT, LOCQTE, LOCQAE, LMAX, EPIRST, EGTOP NBATC 22
COMMON /SSS/ BC(1)                                     NBATC 30
DO 70 I=1,ND                                           NBATC 40
IS = LOCSD + (I-1)*NRESP                               NBATC 60
DO 30 M=1,NRESP                                       NBAT 200
ISUB = IS + M                                          NBAT 280
F = BC(ISUB)                                           NBAT 290
ISUB = ISUB + NDNR                                     NBAT 300
BC(ISUB) = BC(ISUB) + F                                NBAT 310
IF (DABS(F) .LT. 1.0E-36) F = 0.0                      NBAT 320

ISUB = ISUB + NDNR                                     NBAT 330
BC(ISUB) = BC(ISUB) + F*F/NSORC                       NBAT 340
30 CONTINUE                                             NBAT 440
70 CONTINUE                                             NBAT 680
RETURN                                                  NBAT 690
END                                                    NBAT 700

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SUBROUTINE WRNPRI(ITIMEI, NBATCH)                      WRUN 10
C THIS ROUTINE IS CALLED AT THE END OF EACH BATCH     WRUN * *
C IT NORMALIZES AND OUTPUTS CALCULATED QUANTITIES ALONG WITH WRUN * *
C FRACTIONAL STANDARD DEVIATIONS                     WRUN * *
REAL * 8 FN1, FN2, FSAVE1, FSAVE2, E, ANUMB, FOM, FTIMEO
COMMON /USER/ AGSTRT, WTSTRT, XSTRT, YSTRT, ZSTRT, DFF, EBOTY, EBOTG, WRUN 20
1 TCUT, IO, I1, IADJN, NGPQT1, NGPQT2, NGPQT3, NGPQTG, NGPQTN, NITS, NLAST, WRUN 21
2 NLEFT, NMGP, NMTG, NSTRT WRUN 22
COMMON /PDET/ ND, NNE, NE, NT, NA, NRESP, NEX, NEXND, NEND, NDNR, NTHR, NTHE, WRUN 30
1 NANE, NTHDR, NTHEND, NANEEND, LOCRSP, LOCXD, LOCIB, LOCCO, LOCT, LOCUD, WRUN 31

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2 LOCSD,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EFIRST,EGTOP      NRUN 32
COMMON /SSS/ E(1)
COMMON /FRE/ W(188),WFREQ(10,188)
COMMON A(1)                                             NRUN 40
DIMENSION NUMB(1),IHOLL(10),ANUMB(1),P(10),PP(10),NSUM(20,10) NRUN 50
EQUIVALENCE (A(1),NUMB(1)), (IHOLL(1),STR)             NRUN 60
EQUIVALENCE (E(1),ANUMB(1))                           NRUN 60
DATA IH1/IH1/, IH2/IH2/, IHO/IHO/                     NRUN 70
DATA P/0.1,0.2,0.3,0.4,0.5,0.6,0.7,0.8,0.9,0.999/     NRUN 70
DATA PP/10.,20.,30.,40.,50.,60.,70.,80.,90.,100./      NRUN 70
NPART1= NSTRT                                          NRUN 80
IFL = 1
IF(NITS.EQ.NBATCH) IFL = -1
NPART2= NBATCH*NSTRT                                  NRUN 80
C NPART = NBATS*NSTRT                                  NRUN 80
DO 350 K=1,188
WRITE(60,670)W(K),(WFREQ(I,K),I=1,ND)
670 FORMAT(1E ,1PE9.2,10(1X,I6))
350 CONTINUE
FN1= 1.0/NPART1                                       NRUN 90
FN2= 1.0/NPART2                                       NRUN 90
IF (IADJM) 10,10,5                                    NRUN 100
5 FN1= FN1*DFP                                        NRUN 110
FN2= FN2*DFP                                        NRUN 110
10 IX = LOCSD + 4*NDNR + 1                             NRUN 170
IX2 = IX + NDNR                                       NRUN 180
CALL VAR2(E(IX),E(IX2),NRESP,ND,1,NSTRT)              NRUN 190
IX1 = LOCSD + 6*NDNR                                  NRUN 190
IX3 = IX1 + NDNR                                       NRUN 190
IX = IX3 + NDNR                                       NRUN 170
IX2 = IX + NDNR                                       NRUN 180
DO 300 I=1,NDNR
E(IX+I) = E(IX1+I)
E(IX2+I) = E(IX3+I)
300 CONTINUE
IX = LOCSD + 8*NDNR + 1                               NRUN 190
IX2 = IX + NDNR                                       NRUN 190
IX3 = IX2 + NDNR                                       NRUN 190
IX4 = IX3 + NDNR                                       NRUN 190
IX5 = IX4 + NDNR                                       NRUN 190
IX6 = IX5 + NDNR                                       NRUN 190
CALL VAR4(E(IX),E(IX2),E(IX3),E(IX4),E(IX5),E(IX6),
*NRESP,ND,1,NPART2,IFL)
C * * THE STATEMENTS IN THE FOLLOWING LOOP NORMALIZE ALL ARRAYS TO BE OUTPUT
FSAVE1= FN1                                           NRUN 380
FSAVE2= FN2                                           NRUN 380
DO 120 I=1,ND                                         NRUN 380
FN1= FSAVE1*A(LOCSD+5*ND+I)                          NRUN 400
FN2= FSAVE2*A(LOCSD+5*ND+I)                          NRUN 400
IA = LOCSD + (I-1)*NRESP + 4*NDNR                   NRUN 420
IB = LOCSD + (I-1)*NRESP + 8*NDNR                   NRUN 420

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DO 76 M=1,NRESP	NRUN 470
E(IA+M) = E(IA+M)*FW1	NRUN 490
E(IB+M) = E(IB+M)*FW2	NRUN 490
76 CONTINUE	NRUN 490
120 CONTINUE	NRUN 490
IHP = IEO	NRUN 890
C * * OUTPUT SBD, SBD2, SAD AND SAD2 ARRAYS IN THE FOLLOWING LOOP	NRUN 870
DO 125 M=1,NRESP	NRUN 910
IHOL = NLAST + (M-1)*20 + 1	NRUN 920
IHOL2 = IHOL + 19	NRUN 830
WRITE (IO,1020) IHP,(A(I),I=IHOL,IHOL2)	NRUN 840
1020 FORMAT (A1,20A4)	NRUN 850
IHP = IS2	NRUN 860
IST = LOCQE - 9	NRUN 870
WRITE (IO,1030) (ANUMB(I),I=IST,LOCQE)	NRUN 880
1030 FORMAT (1H0,32X,20HRESPONSES(DETECTOR) ,10A8,/,5X,8EDETECTOR,9X,	NRUN 890
1 8HBATCH ,12X,3HFSD,10X,11HACCUMULATED,10X,3HFSD,11X,6HCV(SD),	NRUN 891
2 11X,3HFOM,/,	
3 21X,8HRESPONSE,26X,8HRESPONSE)	NRUN 892
C1030 FORMAT (1H0,32X,20HRESPONSES(DETECTOR) ,10A8,/,5X,8EDETECTOR,7X,	NRUN 890
C 1 8HBATCH ,10X,3HFSD, 8X,11HACCUMULATED, 6X,3HFSD, 9X,7HCV(SDI),	NRUN 891
C 2 8X,6HCV(SD),9X,3HFOM,/,	
C 3 19X,8HRESPONSE,24X,8HRESPONSE)	NRUN 892
WRITE(40,222) NPART2	
222 FORMAT (1H ,/,14X,' NUMBER OF PARTICLES ',18,/))	
WRITE(30,232) NPART2	
232 FORMAT (1H ,/,20X,18,/))	
DO 125 I=1,ND	NRU 1000
IA = LDCSD + 4*NDNR + (I-1)*NRESP + M	NRU 1030
IB = IA + NDNR	NRU 1040
IC = LDCSD + 8*NDNR + (I-1)*NRESP + M	NRU 1030
ID = IC + NDNR	NRU 1040
IL = LDCSD + 12*NDNR + (I-1)*NRESP + M	NRU 1030
IF = IL + NDNR	NRU 1040
ITIME0 = ICLOCK(0)-ITIMEI	NRU 1040
FTIME0 = ITIME0/6000.0	NRU 1040
FOM = 1./(E(ID)**2*FTIME0)	NRU 1040
C125 WRITE (IO,1040) I,E(IA),E(IB),E(IC),E(ID),E(IL),FOM	NRU 1050
WRITE (30,1051) I,E(IA),E(IB),E(IC),E(ID),E(IF),FOM	NRU 1050
WRITE (40,1041) I,E(IA),E(IB),E(IC),E(ID),E(IF),FOM	NRU 1050
1051 FORMAT (2X,I3,'*',1PE11.4,'*',OPF7.4,'*',	NRU 1060
1PE11.4,'',OPF7.4,'*',OPF7.4,'*',	NRU 1060
*1PE11.4)	
1041 FORMAT (I3,1PE13.4,OPF10.4,1PE13.4,OPF10.4,OPF10.4,	NRU 1060
*1PE13.4)	
125 WRITE (IO,1040) I,E(IA),E(IB),E(IC),E(ID),E(IF),FOM	NRU 1050
1040 FORMAT (I10,1PE20.4,OPF15.5,1PE19.4,OPF15.5,OPF16.5,1PE18.4)	NRU 1060
C1040 FORMAT (I10,1PE18.4,OPF13.5,1PE17.4,OPF13.5,OPF13.5,	NRU 1060
C +OPF13.5,1PE16.4)	NRU 1060
DO 414 I=1,ND	
NPA=0	


```

SUB=0.0
TSUM=0.0

DO 408 K=2,188
DEL=(W(K)+W(K+1))/2.
TSUM=TSUM+WFREQ(I,K)*DEL
408 CONTINUE
J=1
DO 412 K=2,188
WPA=WPA+WFREQ(I,K)
DEL=(W(K)+W(K+1))/2.
SUM=SUM+DEL*WFREQ(I,K)
TEST=SUM/TSUM
IF(TEST.LT.P(J)) GO TO 412
406 NSUM(I,J)=WPA
J=J+1
WPA=0
IF(J.GT.10) GO TO 414
IF(TEST.GT.P(J)) GO TO 406
412 CONTINUE
414 CONTINUE
WRITE(10,634)
634 FORMAT(1H ,//,5X,'DETECTOR',10X,' PARTICLE DISTRIBUTION IN',
*' PERCENTAGE BINS RELATIVE TO INCREASING VALUE OF',
*' CONTRIBUTIONS',/)
PR=0.0
WRITE(10,636)PR,(PP(J),J=1,10)
636 FORMAT(1E ,10X,11(5X,F5.1)/)
DO 422 I=1,ND
WRITE(10,644) I,(NSUM(I,J),J=1,10)
644 FORMAT(1H ,I9,4X,10(3X,I7))
422 CONTINUE
RETURN
END
NRU 3170
NRU 3180

SUBROUTINE NRUN(NBATS,NRUNS)
C THIS ROUTINE IS CALLED AT THE END OF EACH RUN
C IT NORMALIZES AND OUTPUTS CALCULATED QUANTITIES ALONG WITH
C FRACTIONAL STANDARD DEVIATIONS
REAL * 8 FM, FSAVE,E,ANUMB
COMMON /USER/ AGSTRT,WTSTRT,KSTRT,YSTRT,ZSTRT,DFP,EBOTM,EBOTG,
1 TCUT,I0,I1,IADJM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTM,NITS,NLAST,
2 NLEFT,NMGP,NMTG,NSTRT
COMMON /PDET/ ND,NNE,NE,NT,NA,NRESP,NEX,NEXED,NEND,NDMR,NTRB,NTRN,NRUN
1 NAME,NTNDER,NTHEND,NAMEHD,LOCASP,LOCID,LOCIB,LOCCO,LOCT,LOCUD,
2 LOCSO,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EFIRST,EGTOP
COMMON /SSS/ E(I)
COMMON A(1)
DIMENSION NUMB(1),ANUMB(1),IHOLL(10)
EQUIVALENCE (A(1),NUMB(1)), (IHOLL(1),STR)
EQUIVALENCE (E(1),ANUMB(1))
DATA IH1/IH1/, IH2/IH2/, IHO/IHO/
NRUN 10
NRUN * *
NRUN * *
NRUN * *
NRUN 20
NRUN 21
NRUN 22
NRUN 30
NRUN 31
NRUN 32
NRUN 40
NRUN 50
NRUN 60
NRUN 60
NRUN 70

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NPART = NBATS*NBSTRT                                FROM 80
FN = 1.0/NPART                                       FROM 90
IF (IADJM) 10,10,6                                   FROM 100
5  FN = FN*DFP                                       FROM 110
  WRITE (IO,1000)                                     FROM 120
1000 FORMAT (82H2THIS IS AN ADJOINT PROBLEM - ADJOINT ENERGY DEPENDENT FROM 130
1FLUENCE IS NOT DIFFERENTIAL)                       FROM 131
10  IX = LOCUD + NDNR + 1                             FROM 140
    IX2 = II + NDNR                                   FROM 150
    CALL VAR2(E(IX),E(IX2),WRESP,ND,1,NPART)         FROM 160
C*****WILSON SEPT/26/89*****

    IX = LOCSD + 2*NDNR + 1
    IZ = LOCSD + 6*NDNR + 1
    IY = IZ + NDNR                                     FROM 150
    CALL FTST(E(IX),E(IY),E(IZ),WRESP,ND,NBATS,NPART) FROM 190
C*****WILSON SEPT/26/89*****

    IX = LOCSD + NDNR + 1                             FROM 170
    IX2 = IX + NDNR                                   FROM 180
    CALL VAR2(E(IX),E(IX2),WRESP,ND,NBATS,NPART)     FROM 190
    IF (NE) 20,20,15                                  FROM 200
15  IX = LOCQE + NEND + 1                             FROM 210
    IX2 = IX + NEND                                   FROM 220
    CALL VAR2(E(IX),E(IX2),WE,ND,1,NPART)            FROM 230
20  IF (NT) 35,35,25                                  FROM 240
25  IX = LOCQT + NTNDNR + 1                           FROM 250
    IX2 = IX + NTNDNR                                 FROM 260
    CALL VAR3(E(IX),E(IX2),WRESP,NT,ND,1,NPART)     FROM 270
    IF (NE) 45,45,30                                  FROM 280
30  IX = LOCQTE + NTNEED + 1                         FROM 290
    IX2 = IX + NTNEED                                 FROM 300
    CALL VAR3(E(IX),E(IX2),NT,NE,ND,1,NPART)        FROM 310
35  IF (NA) 45,45,40                                  FROM 320
40  IX = LOCQAE + NAREND + 1                          FROM 330
    IX2 = IX + NAREND                                FROM 340
    CALL VAR3(E(IX),E(IX2),NA,NE,ND,1,NPART)        FROM 350
45  IF = LOCIB + 2*NE                                 FROM 360
C * * THE STATEMENTS IN THE FOLLOWING LOOP NORMALIZE ALL ARRAYS TO BE OUTPUT
  FSAVE = FN                                          FROM 380
  DO 120 I=1,ND                                       FROM 390
  FN = FSAVE*A(LOCXD+6*ND+I)                         FROM 400
  IA = LOCUD + (I-1)*WRESP+NDNR                     FROM 410
  IB = LOCSD + (I-1)*WRESP + 6*NDNR                 FROM 420
  IC = LOCQE + (I-1)*NE + NEND                      FROM 430
  IF (NE) 60,60,50                                   FROM 440
50  DO 55 J=1,NE                                       FROM 450
55  E(IC+J) = E(IC+J)/A(IF+J)*FN                   FROM 460
60  DO 75 M=1,WRESP                                    FROM 470
    E(IA+M) = E(IA+M)*FN                             FROM 480
    E(IB+M) = E(IB+M)*FN                             FROM 490
    IF (NT) 75,75,65                                  FROM 500
65  IE = LOCQT + (I-1)*NTRR + NTNDR                FROM 510

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	IDT = LOCT + ND*NT + (I-1)*NT	NRUN 520
	DO 70 K=1,NT	NRUN 530
	IQE = IE + (K-1)*NRESP + M	NRUN 540
	IDT = IDT + 1	NRUN 550
70	E(IQE) = E(IQE)*FN/A(IDT)	NRUN 560
75	CONTINUE	NRUN 570
	IF (NE) 120,120,80	NRUN 580
80	IQTE = LOQTE + (I-1)*NTE + NTEEND	NRUN 590
	IQAE = LOQAE + (I-1)*NAE + NAEEND	NRUN 600
	DO 115 J=1,NE	NRUN 610
	IF (NT) 95,95,85	NRUN 620
85	IQT = IQTE + (J-1)*NT	NRUN 630
	IDT = LOCT + ND*NT + (I-1)*NT	NRUN 640
	DO 90 K=1,NT	NRUN 650
	IQ = IQT + K	NRUN 660
	IDT = IDT + 1	NRUN 670
90	E(IQ) = E(IQ)/A(IDT)/A(IF+J)*FN	NRUN 680
95	IF (NA) 115,115,100	NRUN 690
100	IQA = IQAE + (J-1)*NA	NRUN 700
C	THE DA ARRAY IS BEING STORED IN THE FIRST NA CELLS IN QAE	NRUN 690
	IDA = LOQAE + 1	NRUN 720
	IC = LOCCO + 1	NRUN 730
	E(IDA) = (A(IC) + 1.0)*6.2832	NRUN 740
	DO 105 L=2,NA	NRUN 750
	IDA = IDA + 1	NRUN 760
	IC = IC + 1	NRUN 770
105	E(IDA) = (A(IC) - A(IC-1))*6.2832	NRUN 780
	IDA = LOQAE	NRUN 790
	DO 110 L=1,NA	NRUN 800
	IQ = IQA + L	NRUN 810
	IDA = IDA + 1	NRUN 820
110	E(IQ) = E(IQ)/A(IDA)/A(IF+J)*FN	NRUN 830
115	CONTINUE	NRUN 840
120	CONTINUE	NRUN 850
	CALL DATE (IHOLL,I)	NRUN 860
	WRITE (10,1010) (IHOLL(J),J=1,I)	NRUN 870
1010	FORMAT (22H1THIS CASE WAS RUN ON ,10A4)	NRUN 880
	IHP = IEO	NRUN 890
C * *	OUTPUT SUD, SUD2, SSD AND SSD2 ARRAYS IN THE FOLLOWING LOOP	NRUN 870
	DO 125 M=1,NRESP	NRUN 910
	IHOL = NLAST + (M-1)*20 + 1	NRUN 920
	IHOL2 = IHOL + 19	NRUN 930
	WRITE (10,1020) IHP, (A(I),I=IHOL,IHOL2)	NRUN 940
1020	FORMAT (A1,20A4)	NRUN 950
	IHP = IH2	NRUN 960
	IST = LOCQE - 9	NRUN 970
	WRITE (10,1030) (ANUMB(I),I=IST,LOCQE)	NRUN 980
1030	FORMAT (1H0,32X,20HRESPONSES(DETECTOR) ,10A6,/,5X,8HDETECTOR,9X,	NRUN 990
	1 6HUNCOLL,12X,3HPSD,13X,5HTOTAL,13X,3HPSD,12X,3HPSD,10X,	NRUN 991
	3 7HF VALUE,/,21X,8HRESPONSE,26X,8HRESPONSE,10X,5HBTCH)	NRUN 992
	DO 125 I=1,ND	NRUN 1000

IA = LOCUD + NDNR + (I-1)*NRESP + M	NRU 1010
IB = IA + NDNR	NRU 1020
IC = LOCSD + NDNR + (I-1)*NRESP + M	NRU 1030
ID = IC + NDNR	NRU 1040
IC = LOCSD + 8*NDNR + (I-1)*NRESP + M	NRU 1030
IF = IC + NDNR	
IE = LOCSD + 9*NDNR + (I-1)*NRESP + M	NRU 1030
125 WRITE (IO,1040) I,E(IA),E(IB),E(IC),E(ID),E(IE),E(IF)	NRU 1050
1040 FORMAT (I10,1PE20.4,OPF15.5,1PE19.4,OPF15.5,OPF15.5, *OPF15.5)	NRU 1060
IF (NE) 210,210,130	NRU 1070
130 NDM = (ND-1)/10 + 1	NRU 1080
NEM = (NE-1)/17 + 1	NRU 1090
IHP = IE1	NRU 1100
C * + OUTPUT SQE AND SQE2 IN THE FOLLOWING LOOP	NRU 1180
DO 205 IND = 1,NDM	NRU 1120
ID1 = (IND-1)*10 + 1	NRU 1130
IF (IND-NDM) 135,140,140	NRU 1140
135 ID2 = ID1 + 9	NRU 1150
GO TO 145	NRU 1160
140 ID2 = ND	NRU 1170
145 DO 205 INE=1,NEM	NRU 1180
IE1 = (INE-1)*17 + 1	NRU 1190
IF (INE-NEM) 150,155,155	NRU 1200
150 IE2 = IE1 + 16	NRU 1210
GO TO 160	NRU 1220
155 IE2 = NE	NRU 1230
160 IF (INE-1) 165,165,170	NRU 1240
165 ETOP = EFIRST	NRU 1250
GO TO 175	NRU 1260
170 ETOP = A(LOCIB+NE+IE1-1)	NRU 1270
175 IST = LOCQT - 9	NRU 1280
WRITE (IO,1050) IHP,(ANUMB(I),I=IST,LDCQT),(I,I=ID1,ID2)	NRU 1290
1060 FORMAT (A1,27X,24HFLUENCE(ENERGY,DETECTOR),1X,10A6,/,16H0 DETECTNRU 1300 IGR NO.,18,9I10)	NRU 1301
IF (NE-7) 180,180,185	NRU 1310
180 IHP = IE2	NRU 1320
185 WRITE (IO,1060) ETOP	NRU 1330
1060 FORMAT (9H ENERGIES,/,1X,1PE11.3)	NRU 1340
DO 205 IE = IE1,IE2	NRU 1350
IF (NNE) 190,200,190	NRU 1360
190 IF (IE-NNE-1) 200,195,200	NRU 1370
195 WRITE (IO,1060) EGTOP	NRU 1380
200 IEP = LOCIB + NE + IE	NRU 1390
ID11 = LOCQE + (ID1-1)*NE + NEND + IE	NRU 1400
ID12 = ID11 + (ID2-ID1)*NE	NRU 1410
WRITE (IO,1070) (E(I),I=ID11,ID12,NE)	NRU 1420
1070 FORMAT (17X,1P10E10.3)	NRU 1430
ID11 = ID11 + NEND	NRU 1440
ID12 = ID12 + NEND	NRU 1450
WRITE (IO,1080) (E(I),I=ID11,ID12,NE)	NRU 1460

1080	FORMAT (17X,10(F9.3,1X))	NRU 1470
205	WRITE (10,1090) A(IEP)	NRU 1480
1090	FORMAT (1X,1PE11.3)	NRU 1490
210	IF (NT) 375,375,215	NRU 1500
215	WRM = (WRSP-1)/10 + 1	NRU 1510
	WTM = (WT-1)/17 + 1	NRU 1520
	IHP = IB1	NRU 1530
C *	* OUTPUT SQT AND SQT2 IN THE FOLLOWING LOOP	NRU 1580
	DO 275 I=1,ND	NRU 1550
	DO 275 INR=1,WRM	NRU 1560
	IR1 = (INR-1)*10 + 1	NRU 1570
	IF (INR-WRM) 220,225,225	NRU 1580
220	IR2 = IR1 + 9	NRU 1590
	GO TO 230	NRU 1600
225	IR2 = WRSP	NRU 1610
230	DO 275 INT=1,WTM	NRU 1620
	IST = LOCQTE - 9	NRU 1630
	WRITE (10,1100) IHP,I,(ANUMB(IPR),IPR=IST,LOCQTE)	NRU 1640
1100	FORMAT (A1,11HDETECTOR NO,13,6X,32HRESPONSE(RESPONSE,TIME,DETECTORNRU 1650	
	1),1X,10A8)	NRU 1651
	IF (NT-8) 235,235,240	NRU 1660
235	IHP = IB2	NRU 1670
240	IT1 = (INT-1)*17 + 1	NRU 1680
	IF (INT-WTM) 245,250,250	NRU 1690
245	IT2 = IT1 + 16	NRU 1700
	GO TO 255	NRU 1710
250	IT2 = IT	NRU 1720
255	IF (INT-1) 260,260,265	NRU 1730
260	AGS = A(LOCKD + 4*ND + I)	NRU 1740
	GO TO 270	NRU 1750
265	ISUB = LOCT + (I-1)*NT + IT1 - 1	NRU 1760
	AGS = A(ISUB)	NRU 1770
270	WRITE (10,1110) (IR,IR=IR1,IR2)	NRU 1780
1110	FORMAT (4X,9H RESPONSE,10I10)	NRU 1790
	WRITE (10,1120) AGS	NRU 1800
1120	FORMAT (7H TIMES /1PE12.3)	NRU 1810
	DO 275 IT=IT1,IT2	NRU 1820
	INDT = (I-1)*NT + IT + LOCT	NRU 1830
	ITR1 = LOCQT + NTDNR + (I-1)*NTNR + (IT-1)*WRSP + IR1	NRU 1840
	ITR2 = ITR1 + IR2 - IR1	NRU 1850
	WRITE (10,1070) (E(IP),IP=ITR1,ITR2)	NRU 1860
	ITR1 = ITR1 + NTDNR	NRU 1870
	ITR2 = ITR2 + NTDNR	NRU 1880
	WRITE (10,1080) (E(IP),IP=ITR1,ITR2)	NRU 1890
275	WRITE (10,1090) A(INDT)	NRU 1900
	IF (NE) 475,475,280	NRU 1910
280	WEM = (WE-1)/10 + 1	NRU 1920
	WTM = (WT-1)/17 + 1	NRU 1930
	IHP = IB1	NRU 1940
C *	* OUTPUT SQTE AND SQTE2 IN THE FOLLOWING LOOP	NRU 1970
	DO 370 I=1,ND	NRU 1980

DO 370 INE=1,NEM	NRU 1970
IE1 = (INE-1)*10 + 1	NRU 1980
IF (INE-NEM) 285,290,290	NRU 1990
285 IE2 = IE1 + 9	NRU 2000
GO TO 295	NRU 2010
290 IE2 = NE	NRU 2020
295 IF (INE-1) 300,300,306	NRU 2030
300 ETOP = EFIRST	NRU 2040
GO TO 310	NRU 2050
305 ETOP = A(LOCIB + NE + IE1 - 1)	NRU 2060
IF (IE1.EQ.NNE+1) ETOP=EGTOP	NRU 2070
310 I1E = LOCIB + NE + IE1	NRU 2080
DO 370 INT=1,NTM	NRU 2090
I2 = LOCIB + NE + IE2 - 1	NRU 2100
IST = LOCQAE - 9	NRU 2110
WRITE (IO,1130) IHP,I,(AFUMB(IPR),IPR=IST,LOCQAE)	NRU 2120
1130 FORMAT (A1,11HDETECTOR NO,13,8X,2BHFLUENCE(TIME,ENERGY,DETECTOR),	NRU 2130
1 IX,10A8)	NRU 2131
IF (NT-8) 315,316,320	NRU 2140
315 IHP = IH2	NRU 2150
320 IT1 = (INT-1)*17 + 1	NRU 2160
IF (INT-NTM) 325,330,330	NRU 2170
325 IT2 = IT1 + 16	NRU 2180
GO TO 335	NRU 2190
330 IT2 = NT	NRU 2200
335 IX = LOCIB + NE + NNE	NRU 2210
ESAV = A(IX)	NRU 2220
IF (NNE.LT. IE1 .OR. NNE.GE. IE2) GO TO 340	NRU 2230
A(IX) = EGTOP	NRU 2240
340 IF (I1E.LE. I2) GO TO 345	NRU 2250
WRITE (IO,1140) ETOP	NRU 2260
GO TO 350	NRU 2270
345 WRITE (IO,1140) ETOP,(A(IP),IP=I1E,I2)	NRU 2280
1140 FORMAT (1E0,3X,8HENERGIES,5X,1P10E10.3)	NRU 2290
350 A(IX) = ESAV	NRU 2300
I2 = I2 + 1	NRU 2310
IF (INT-1) 355,355,360	NRU 2320
355 AGS = A(LOCXD + 4*ND + I)	NRU 2330
GO TO 365	NRU 2340
360 ISUB = LOCT + (I-1)*NT + IT1 - 1	NRU 2350
AGS = A(ISUB)	NRU 2360
365 WRITE (IO,1150) (A(IP),IP=I1E,I2)	NRU 2370
1150 FORMAT (2X,5HTIMES,10X,1P10E10.3)	NRU 2380
WRITE (IO,1160) AGS	NRU 2390
1160 FORMAT (1PE12.3)	NRU 2400
DO 370 IT=IT1,IT2	NRU 2410
INDT = (I-1)*NT + IT + LOCT	NRU 2420
ITE1 = (I-1)*NTNE + (IE1-1)*NT + IT + LOCQTE + NTWEND	NRU 2430
ITE2 = ITE1 + (IE2-IE1)*NT	NRU 2440
WRITE (IO,1070) (E(IP),IP=ITE1,ITE2,NT)	NRU 2450
ITE1 = ITE1 + NTWEND	NRU 2460

ITE2 = ITE2 + NTHEND	NRU 2470
WRITE (IO,1080) (E(IP),IP=ITE1,ITE2,NT)	NRU 2480
370 WRITE (IO,1090) A(INDT)	NRU 2490
375 IF (NA) 475,476,380	NRU 2500
380 NEM = (NE-1)/10 + 1	NRU 2510
NAM = (NA-1)/17 + 1	NRU 2520
IHP = IE1	NRU 2530
C * * OUTPUT SQAE AND SQAE2 IN THE FOLLOWING LOOP	NRU 2500
DO 470 I=1,ND	NRU 2550
DO 470 INE=1,NEM	NRU 2560
IE1 = (INE-1)*10 + 1	NRU 2570
IF (INE-NEM) 385,390,390	NRU 2580
385 IE2 = IE1 + 9	NRU 2590
GO TO 385	NRU 2600
390 IE2 = NE	NRU 2610
395 IF (INE-1) 400,400,405	NRU 2620
400 ETOP = EFIRST	NRU 2630
GO TO 410	NRU 2640
405 ETOP = A(LOCIB + NE + IE1 - 1)	NRU 2650
410 I1E = LOCIB + NE + IE1	NRU 2660
DO 470 INA=1,NAM	NRU 2670
I2 = LOCIB + NE + IE2 - 1	NRU 2680
IST = LMAX - 9	NRU 2690
WRITE (IO,1170) IHP,I,(ANUMB(IPR),IPR=IST,LMAX)	NRU 2700
1170 FORMAT (A1,11HDETECTOR NO,I3,6X,31HFLUENCE(COSINE,ENERGY,DETECTOR)	NRU 2710
1,1X,10A8)	NRU 2711
IF (NA-8) 415,415,420	NRU 2720
415 IHP = IE2	NRU 2730
420 IX = LOCIB + NE + NNE	NRU 2740
ESAV = A(IX)	NRU 2750
IF (NNE .LT. IE1 .OR. NNE .GE. IE2) GO TO 425	NRU 2760
A(IX) = EGTOP	NRU 2770
425 IF (I1E .LE. I2) GO TO 430	NRU 2780
WRITE (IO,1140) ETOP	NRU 2790
GO TO 435	NRU 2800
430 WRITE (IO,1140) ETOP,(A(IP),IP=I1E,I2)	NRU 2810
435 A(IX) = ESAV	NRU 2820
I2 = I2 + 1	NRU 2830
IA1 = (INA-1)*17 + 1	NRU 2840
IF (INA-1) 440,440,445	NRU 2850
440 FM1 = -1.0	NRU 2860
GO TO 450	NRU 2870
445 FM1 = A(LOCIB + IA1 - 1)	NRU 2880
450 WRITE (IO,1180) (A(IP),IP=I1E,I2)	NRU 2890
1180 FORMAT (5X,7HCOSINES,5X,1P10E10.3)	NRU 2900
WRITE (IO,1190) FM1	NRU 2910
1190 FORMAT (2X,F12.6)	
IF (INA-NAM) 455,460,460	NRU 2930
455 IA2 = IA1 + 16	NRU 2940
GO TO 465	NRU 2950
460 IA2 = NA	NRU 2960

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465 DO 470 IA=IA1,IA2                                FRU 2970
      ICG = LOCCO + IA                                FRU 2980
      IAE1 = (I-1)*NAME + (IE1-1)*NA + IA + LOCQAE + NAMEEND FRU 2990
      IAE2 = IAE1 + (IE2-IE1)*NA                    FRU 3000
      WRITE (IO,1070) (A(IP),IP=IAE1,IAE2,NA)
      IAE1 = IAE1 + NAMEEND                            FRU 3020

      IAE2 = IAE2 + NAMEEND                            FRU 3030
      WRITE (IO,1080) (A(IP),IP=IAE1,IAE2,NA)
470 WRITE (IO,1190) A(ICG)
475 IF (NEIND) 490,490,480                            FRU 3050
C   OUTPUT EXTRA ARRAYS OF LENGTH ND * * * * *      FRU * *
480 WRITE (IO,1200)                                FRU 3060
1200 FORMAT (26H1EXTRA ARRAYS OF LENGTH ND/)
      DO 485 I=1,NEIND                                FRU 3080
      STR = 0.0                                       FRU 3090
      CALL INSERT(STR,1,4,4HEXTR)                     FRU 3100
      CALL INTBCD(I,DUM,L)                             FRU 3110
      LP = 5 - L                                       FRU 3120
      CALL INSERT(STR,LP,L,DUM)                       FRU 3130
      IST = LOCED + (5+I)*ND + 1                      FRU 3140
485 CALL HELPER(A(IST),1,ND,STR,IO)                  FRU 3150
490 CALL ENDRUN                                       FRU 3160
      RETURN                                           FRU 3170
      END                                              FRU 3180

C*
SUBROUTINE OUTPT(KEY)                                OUTPT 10
C * * THIS VERSION OF OUTPT IS FOR MORSE-CGA * * * *
C   THIS ROUTINE CONTROLS CALCULATION AND OUTPUT OF AVERAGE VALUES OF OUTPT *
C   SOURCE PARAMETERS (KEY=1), THE COLLISION COUNTERS AT THE END OF OUTPT *
C   EACH BATCH (KEY=2), AND OUTPUTS THE COUNTERS FOR NUMBER OF OUTPT *
C   SCATTERINGS, ETC., AT END OF RUN (KEY=3)         OUTPT *
COMMON /NUTRON/ NAME,NAMEX,IG,IGO,NMED,MEDOLD,NREG,U,V,W,UOLD,VOLD,OUTPT 30
1  ,WOLD,X,Y,Z,XOLD,YOLD,ZOLD,WATE,OLDWT,WTBC,BLZNT,BLZON,AGE,OLDAGE,OUTPT 31
COMMON /APOLLO/ AGSTRT,DDF,DEADWT(6),ETA,ETATH,ETAUSD,UIMP,VIMP, OUTPT 40
1  WIMP,WTSTRT,ISTRT,YSTRT,ZSTRT,TCUT,XTRA(10), OUTPT 41
2  IO,I1,MEDIA,IADJH,ISBIAS,ISOUR,ITERS,ITIME,ITSTR,LOCWTS,LOCFWL,OUTPT 42
3  LOCEPR,LOCNSC,LOCPSM,MAXGP,MAXTIM,MEDALB,NGPREG,MYREG,NALB, OUTPT 43
4  NDEAD(6),NEWNM,NGEON,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTN,NITS, OUTPT 44
5  NKCALC,NKILL,NLAST,NMEM,NMGP,NMOST,NMIG,NOLEAK,NORMF,NPAST, OUTPT 45
6  NPSC(13),NQUIT,NSIGL,NSOUR,NSPLT,NSTRT,NXTRA(10) OUTPT 46
COMMON /FISBNK/ NFISTP,NFISBN,NFISH,FTOTL,FWATE,WATEF OUTPT 50
COMMON /OUTB/ SWATE,XAVE,YAVE,ZAVE,EAVE,UAVE,VAVE,WAVE,AGEAVE GSTR 40
COMMON WTS(1)                                         OUTPT 60
DIMENSION NC(1)                                       OUTPT 70
EQUIVALENCE (WTS(1),NC(1))                          OUTPT 80
REAL*8 RANDOM                                         OUTPT
DATA FPK/0.0/,FKSUM/0.0/,VARK/0.0/,FMKFW/0.0/,FKFW/0.0/ OUTPT 90
DATA NITSX/0/                                         OUTPT 100
GO TO (1111,2222,3333),KEY                          OUTPT 110
1111 NBTCH=NITS-ITERS+1                              OUTPT 120

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	IF (NBATCH-1) 20,15,20	OUTP 130
15	ITCUT = 1	OUTP 140
	FKFW =0.	OUTP 150
	FKFW =0.	OUTP 180
20	FNKT = NMEM	OUTP 170
	FKFW = FKFW + FNKT	OUTP 180
	IF(SWATE.EQ.0.) GO TO 30	OUTP 430
	IAVE=IAVE/SWATE	OUTP 440
	YAVE=YAVE/SWATE	OUTP 450
	ZAVE=ZAVE/SWATE	OUTP 460
	EAVE=EAVE/SWATE	OUTP 470
	UAVE=UAVE/SWATE	OUTP 480
	VAVE=VAVE/SWATE	OUTP 490
	WAVE=WAVE/SWATE	OUTP 500
	AGEAVE=AGEAVE/SWATE	OUTP 510
30	WRITE (10,1010)	OUTP
1010	FORMAT (' WTAVE IAVE UAVE VAVE WAVE XAVE	OUTP
	1 YAVE ZAVE AGEAVE')	OUTP
	WRITE (10,1011)SWATE,EAVE,UAVE,VAVE,WAVE,XAVE,YAVE,ZAVE,AGEAVE	OUTP
1011	FORMAT(1H ,1PE10.3,2X,OPF7.2,2X,3(F7.4,1X),1X,3(1PE10.3,1X),1X,	OUTP
	1E10.3)	OUTP
	RETURN	OUTP 540
2222	WRITE(10,1030)	OUTP 550
1030	FORMAT(/35#NUMBER OF COLLISIONS OF TYPE NCOLL/3X,6#SOURCE,1X,	OUTP 560
	1 SRSPLIT(D),4X,5#FISH,3X,6#GANGEM,1X,8#REALCOLL ,3X,6#ALBEDO,4X,	OUTP 561
	2 5#BDRY,3X,6#ESCAPE,4X,6#E-CUT,1X,8#TIMERILL ,1X,8#R KILL,1X,	OUTP 562
	3 8#R SURV, 2X,7#GAMLOST)	OUTP 563
	WRITE (10,1040) (NPSCL(I),I=1, 13)	OUTP 570
1040	FORMAT(13I9)	OUTP 580
	LENGTH = 0	OUTP 590
	CALL TIMER(LENGTH,XTRA)	OUTP 600
	WRITE (10,1050) (XTRA(I),I=1,LENGTH)	OUTP 610
1050	FORMAT (43#TIME REQUIRED FOR THE PRECEDING BATCH WAS ,10#4)	OUTP 620
	IF (ITCUT) 50,50,40	OUTP 630
40	IF (NPSCL(10)) 50,50,45	OUTP 640
45	ITCUT = 0	OUTP 650
50	DO 55 I=1,13	OUTP 660
55	NPSCL(I)=0	OUTP 670
	IF (NORMF) 65,65,60	OUTP 680
60	FKFW = FKFW + FNKT*FTOTL/SWATE	OUTP 690
	IF (NFISH) 65,65,65	OUTP 700
65	ESTK = PKFW/FKFW*NFISH/NSTRT	OUTP 710
	IF (ESTK) 65,65,70	OUTP 720
70	DO 75 I=1,MIREG	OUTP 730
75	WTS(LOCFWL+I) = WTS(LOCFWL+I)*ESTK	OUTP 740
	WTCRNG = FWATE/NFISH/SWATE*FNKT	OUTP 750
	NG1 = LOCWTS+1	OUTP 760
	NG2 = LOCWTS+3*NGPREG	OUTP 770
	DO 80 I=NG1,NG2	OUTP 780
80	WTS(I) = WTS(I)*WTCRNG	OUTP 790
85	IF (NKCALC) 105,105,90	OUTP 800

90	FKT = FTOTL/SWATE	OUTP 810
	IF (NBATCH .LT. NKCALC .OR. ITCUT .EQ. 0) GO TO 95	OUTP 820
	FKSUM = FKSUM + FNKT*FKT	OUTP 830
	VARK = VARK + FNKT*FKT*FKT	OUTP 840
	FNK = FNK + FNKT	OUTP 850
	NITSK = NITSK + 1	OUTP 860
	GO TO 100	OUTP 870
95	WRITE(10,1060)	OUTP 880
1060	FORMAT(83H --- K FOR THIS BATCH WILL NOT BE USED IN AVERAGE K CALCULATION)	OUTP 890
100	WRITE (10,1070) FKT ,FTOTL,FWATE,EFISH	OUTP 900
1070	FORMAT(180/3H K=,F9.5,15X,6HFTOTL=,E13.5,5X,6HFWATE=,E13.5,15X,6HNFISH=,15)	OUTP 910
106	RETURN	OUTP 920
3333	WRITE (10,1080) (NDEAD(I),DEADWT(I),I=1,4)	OUTP 930
1080	FORMAT(16H1NEUTRON DEATHS,20X,6HNUMBER,16X,6HWEIGHT/127HOKILLED BY RUSSIAN ROULETTE,8X,16, 9X,E13.5/26H ESCAPED,27X,16, 9X,E13.5/322H REACHED ENERGY CUTOFF,13X,16, 9X,E13.5/20H REACHED TIME CUTOFF,4 15X,16, 9X,E13.5)	OUTP 940
	IF(MEDIA)125,125,117	OUTP 945
117	WRITE(10,1090)	OUTP 950
1090	FORMAT(180/22HNUMBER OF SCATTERINGS)	OUTP 960
C		OUTP 960
	WRITE(10,1100)	OUTP 980
1100	FORMAT(7HONMEDIUM 13X,6HNUMBER)	OUTP 990
	N123=0	OUTP 995
	DO 115 NMED=1,MEDIA	OUT 1000
	N1 = LDCNSC + 8*NMTG*MIREG + NMED	OUT 1010
	N123=N123+NC(N1)	OUT
115	WRITE(10,1110)NMED,WTS(N1)	OUT 1020
1110	FORMAT (15,10X,17)	OUT 1030
	WRITE (10,1112) N123	OUT
1112	FORMAT (' TOTAL', 9X,17)	OUT
120	WRITE (10,1120)	OUT 1050
1120	FORMAT ('1REAL SCATTERING COUNTERS')	OUT 1060
	N1 = LDCNSC + 1	OUT 1070
	CALL OUTPT2(WTS(N1),NC(N1),NMTG,MIREG,10)	OUT 1080
125	IF (MEDALB-7777) 130,135,130	OUT 1090
130	WRITE (10,1130)	OUT 1100
1130	FORMAT ('1ALBEDO SCATTERING COUNTERS')	OUT 1110
	N1 = LDCNSC + 2*NMTG*MIREG + 1	OUT 1120
	CALL OUTPT2(WTS(N1),NC(N1),NMTG,MIREG,10)	OUT 1130
135	IF (MFISTP) 145,145,140	OUT 1140
140	WRITE (10,1140)	OUT 1150
1140	FORMAT ('1FISSION PRODUCTION COUNTERS')	OUT 1160
	N1 = LDCNSC + 4*NMTG*MIREG + 1	OUT 1170
	CALL OUTPT2(WTS(N1),NC(N1),NMTG,MIREG,10)	OUT 1180
145	IF (NGPQTN*NGPQTG) 160,155,150	OUT 1190
150	WRITE (10,1150)	OUT 1200
1150	FORMAT ('1SECONDARY PRODUCTION COUNTERS (BOTH THE GROUPS CAUSING POUT	OUT 1210

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1PRODUCTION AND RESULTING FROM PRODUCTION')          OUT 1211
  N1 = LOCWSC + 6*NMTG*MXREG + 1                      OUT 1220
  CALL OUTPT2(WTS(N1),NC(N1),NMTG,MXREG,IO)           OUT 1230
155 IF (RSPLT) 165,165,160                            OUT 1240
160 WRITE(IO,1160)                                     OUT 1250
1160 FORMAT(21H1NUMBER OF SPLITTINGS)                 OUT 1260
  N1 = LOCWTS+4*NGPREG+1                              OUT 1270
  CALL OUTPT2(WTS(N1),NC(N1),MAXGP,MXREG,IO)         OUT 1280
  WRITE (IO,1170)                                     OUT 1290
1170 FORMAT(47H1NUMBER OF SPLITTINGS PREVENTED BY LACK OF ROOM) OUT 1300
  N1 = N1 + 2*NGPREG                                  OUT 1310
  CALL OUTPT2(WTS(N1),NC(N1),MAXGP,MXREG,IO)         OUT 1320
165 IF(SKILL)175,175,170                              OUT 1330
170 WRITE(IO,1180)                                     OUT 1340
1180 FORMAT(33H1NUMBER OF RUSSIAN ROULETTE KILLS)    OUT 1350
  N1 = LOCWTS + 8*NGPREG + 1                         OUT 1360
  CALL OUTPT2(WTS(N1),NC(N1),MAXGP,MXREG,IO)         OUT 1370
  WRITE(IO,1190)                                     OUT 1380
1190 FORMAT(37H1NUMBER OF RUSSIAN ROULETTE SURVIVALS) OUT 1390
  N1 = N1 + 2*NGPREG                                  OUT 1400
  CALL OUTPT2(WTS(N1),NC(N1),MAXGP,MXREG,IO)         OUT 1410
175 IF(NKCALC)185,185,180                             OUT 1420
180 VARK = VARK/FNK                                    OUT 1430
  FKSUM = FKSUM/FNK                                   OUT 1440
  VARK = SQRT ((VARK-FKSUM**2)/(NITSK-1))            OUT 1450
  WRITE(IO,1200) FKSUM,VARK,NITSK                    OUT 1460
1200 FORMAT(11H1AVERAGE K=,E15.4,10X,14HSTANDARD DEV.=,E15.4,5X,3HFOR,IO) OUT 1470
  14,9H BATCHES)                                     OUT 1471
185 FNK= 0.                                           OUT 1480
  FKSUM=0.                                           OUT 1490
  VARK=0.                                           OUT 1500
  NITSK=0                                           OUT 1510
  CALL RNDOUT(RANDOM)                                OUT
  WRITE (IO,1210) RANDOM                              OUT
1210 FORMAT('0 ** NEXT RANDOM NUMBER IS ',Z12)       OUT
  RETURN                                             OUT 1520
  END                                               OUT 1530
SUBROUTINE SCORIN                                     SCORI 10
C                                                    * * * *
C THIS ROUTINE READS INPUT DATA FOR THE ANALYSIS MODULE * * * * * * * *
C                                                    * * * *
REAL * 8 SS, LNK1
COMMON /USER/ AGSTRT,WTSTRT,ISTRT,YSTRT,ZSTRT,DFP,EBOTN,EBOTG, SCORI 20
1 TCUT,IO,I1,IADJM,NGPQT1,NGPQT2,NGPQT3,NGPQTG,NGPQTN,NITS,BLAST, SCORI 21
2 NLEFT,NMGP,NMTG,NSTRT                               SCORI 22
COMMON /PDET/ ND,NFE,NE,NT,NA,NRESP,HEX,HEXND,WEND,NDNR,FTNR,RTWE, SCORI 30
1 NAME,HTDNR,HTNEND,NANEND,LOCESP,LOCED,LOCIB,LOCCO,LOCT,LOCUD, SCORI 31
2 LOCSD,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EFIRST,EGTOP   SCORI 32
COMMON BLNK(1)                                       SCORI 40
COMMON /SSS/ SS(1)

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DIMENSION LNK(1),LNK1(1),IHOL(20),IHF(6),IHA(6),IHP(6)	SCORI 50
EQUIVALENCE(BLNK(1),LNK(1)),(SS(1),LNK1(1))	SCORI 60
DATA IHDLB,IHF,IEA/1H,4HPRIM,4HARY,4HENER,4HGY B,4HINS,1H,	SCORI 70
1 4HSECO,4HNDAR,4HY EN,4HERGY,4H BIV,1ES/,JUP/3HUPP/,JLD/3ELOW/	SCORI 71
C**** WILSON JUNE 2, 1989 ****	MOR 1150
C LOCUD = LOCT + 2*ND*NT	SCOR 680
LOCUD = 0	SCOR 680
C**** WILSON JUNE 2, 1989 ****	MOR 1150
LOCSD = LOCUD + 3*NDNR	SCOR 690
C**** WILSON APRIL 19,1989 ****	MOR 1150
C LOCQE = LOCSD + 3*NDNR + 20	SCOR 700
LOCQE = LOCSD + 14*NDNR + 20	SCOR 700
C**** WILSON APRIL 19,1989 ****	MOR 1150
RETURN	SCO 3330
END	SCO 3340
SUBROUTINE STBTCH (NBAT)	STBTC 10
C THIS ROUTINE IS CALLED AT THE START OF EACH BATCH	STBTC *
C THIS ROUTINE ZEROES THE ARRAYS USED TO ACCUMULATE ESTIMATED	STBTC *
C QUANTITIES DURING A BATCH .	STBTC *
C AT THE START OF THE FIRST BATCH, THE ARRAYS WHICH ACCUMULATE	STBTC *
C ESTIMATES AND SQUARED ESTIMATES ARE ALSO ZEROED . * *	STBTC *
REAL * 8 BL	
COMMON /PDET/ ND,NNE,NE,NT,NA,NRESP,NEX,NEXND,NEND,NDNR,NTNR,NTNE,	STBTC 30
1 NANE,NTDNR,NTWEND,NAVEND,LOCESP,LOCID,LOCIB,LOCCO,LOCT,LOCUD,	STBTC 31
2 LOCSD,LOCQE,LOCQT,LOCQTE,LOCQAE,LMAX,EPIRST,EGTOP	STBTC 32
COMMON /SSS/ BL(1)	STBTC 40
IF (NBAT) 10,20,150	STBTC 50
10 CALL ERROR	STBTC 60
20 IA = LOCUD + 1	STBTC 70
C**** WILSON APRIL 18,1989 ****	MOR 1150
C IB = IA + 6*NDNR - 1	STBTC 80
IB = IA + 17*NDNR - 1	STBTC 80
C**** WILSON APRIL 18,1989 ****	MOR 1150
DO 30 I=IA,IB	STBTC 90
30 BL(I) = 0.0	STBT 100
IF (NE) 60,60,40	STBT 110
40 IA = LOCQE + 1	STBT 120
IB = IA + 3*NEND - 1	STBT 130
DO 50 I=IA,IB	STBT 140
50 BL(I) = 0.0	STBT 150
60 IF (NT) 110,110,70	STBT 160
70 IA = LOCQT + 1	STBT 170
IB = IA + 3*NTDNR - 1	STBT 180
DO 80 I=IA,IB	STBT 190
80 BL(I) = 0.0	STBT 200
IF (NE) 140,140,90	STBT 210
90 IA = LOCQTE + 1	STBT 220

	IB = IA + 3*NTWEND - 1	STBT 230
	DO 100 I=IA,IB	STBT 240
100	BL(I) = 0.0	STBT 260
110	IF (NA*NE) 140,140,120	STBT 260
120	IA = LOCQAE + 1	STBT 270
	IB = IA + 3*NAWEND - 1	STBT 280
	DO 130 I=IA,IB	STBT 290
130	BL(I) = 0.0	STBT 300
140	RETURN	STBT 310
150	IA = LOCSD	STBT 330
	IJ = LOCSD + 4*NDNR	STBT 330
	IV = LOCSD + 5*NDNR	STBT 330
	DO 290 I=1,ND	STBT 380
	DO 210 M=1,NRESP	STBT 430
	IA = IA + 1	STBT 450
	IJ = IJ + 1	STBT 450
	IV = IV + 1	STBT 450
	BL(IA) = 0.0	STBT 470
	BL(IJ) = 0.0	STBT 470
	BL(IV) = 0.0	STBT 470
210	CONTINUE	STBT 650
290	CONTINUE	STBT 650
	RETURN	STBT 650
	END	STBT 660
	 SUBROUTINE STPART	STBTC 10
C	THIS ROUTINE IS CALLED AT THE START OF EACH SOURCE PARTICLE	STBTC *
C	THIS ROUTINE ZEROES THE ARRAYS USED TO ACCUMULATE ESTIMATED	STBTC *
C	QUANTITIES DURING A BATCH .	STBTC *
	REAL * 8 BL	
	COMMON /PDET/ ND, NNE, NE, NT, NA, NRESP, NEX, NEXND, NEND, NDNR, NTR, NTRN, STBTC 30	
	1 NANE, NTHNR, NTHEND, NAWEND, LOCSP, LOCXD, LOCIB, LOCCO, LOCT, LDCUD, STBTC 31	
	2 LOCSD, LOCQE, LOCQT, LOCQTE, LOCQAE, LMAX, EFIRST, EGTOP STBTC 32	
	COMMON /SSS/ BL(1)	STBTC 40
	IA = LDCUD	STBT 320
	IJ = LOCSD + 3*NDNR	STBT 330
	IC = LOCQE	STBT 340
	ID = LOCQT	STBT 350
	IE = LOCQTE	STBT 360
	IF = LOCQAE	STBT 370
	DO 290 I=1,ND	STBT 380
	IF (NE) 180,180,160	STBT 390
160	DO 170 J=1,NE	STBT 400
	IC = IC + 1	STBT 410
170	BL(IC) = 0.0	STBT 420
180	DO 210 M=1,NRESP	STBT 430
	IA = IA + 1	STBT 440
	IJ = IJ + 1	STBT 450
	BL(IA) = 0.0	STBT 460
	BL(IJ) = 0.0	STBT 470
	IF (NT) 210,210,190	STBT 480
190	DO 200 K=1,NT	STBT 490

	ID = ID + 1	STBT 500
200	BL(ID) = 0.0	STBT 510
210	CONTINUE	STBT 520
	IF (NE) 290,290,220	STBT 530
220	DO 280 J=1,NE	STBT 540
	IF (NT) 250,250,230	STBT 550
230	DO 240 K=1,NT	STBT 560
	IK = IE + 1	STBT 570
240	BL(IE) = 0.0	STBT 580
250	IF (NA) 280,280,260	STBT 590
260	DO 270 L=1,NA	STBT 600
	IF = IF + 1	STBT 610
270	BL(IF) = 0.0	STBT 620
280	CONTINUE	STBT 630
290	CONTINUE	STBT 640
	RETURN	STBT 650
	END	STBT 660
	SUBROUTINE TESTW	TESTW 10
C * *	THIS VERSION OF TESTW IS FOR MORSE-CGA * * *	
C	THIS ROUTINE TESTS WHETHER RUSSIAN ROULETTE OR SPLITTING OPTIONS	TESTW **
C	ARE IN EFFECT AND THEN PERFORMS THE SPLITTING OR ROULETTE	TESTW **
C	SPLITTING IS PERFORMED UNTIL THE WEIGHT FALLS BELOW WTHR	TESTW **
	COMMON /NUTRON/ NAME, NAMEX, IG, IGO, EMED, MEDOLD, NREG, U, V, W, UOLD, VOLD	TESTW 20
1	, WOLD, X, Y, Z, XOLD, YOLD, ZOLD, WATE, OLDWT, WTBC, BLZNT, BLZON, AGE, OLDAGETESTW	TESTW 21
	COMMON /APOLLO/ AGSTRT, DDF, DEADWT(6), ETA, ETATE, ETAUSD, UINP, VINP,	TESTW 30
1	WIMP, WTSTRT, ISTRT, YSTRT, ZSTRT, TCUT, ITRA(10),	TESTW 31
2	IO, I1, MEDIA, IADJK, ISBIAS, ISOUR, ITERS, ITIME, ITSTR, LOCWTS, LOCFWL,	TESTW 32
3	LOCEPR, LOCHSC, LOCFSN, MAXGP, MAXTIM, MEDALB, MGPREG, NXREG, NALB,	TESTW 33
4	NDEAD(5), NEWNM, NGEOM, NGPQT1, NGPQT2, NGPQT3, NGPQTG, NGPQTW, NITS,	TESTW 34
5	NKCALC, NKILL, ELAST, NMEM, NMGP, NMOST, NMTG, NOLEAK, NORMF, NPAST,	TESTW 35
6	NPSCL(13), NQUIT, NSIGL, NSOUR, NSPLT, NSTRT, NTRA(10)	TESTW 36
	COMMON /NS/ NS	GSTOR 40
	COMMON NWT(1)	TESTW 40
	DIMENSION WTS(1)	TESTW 50
	EQUIVALENCE (NWT(1), WTS(1))	TESTW 60
	IF (IG-MAXGP) 10,10,65	TESTW 70
10	IF (NKILL+NSPLT) 65,65,15	TESTW 80
15	NWT = (NREG-1)*MAXGP+IG+LOCWTS	TESTW 90
	WTHR = WTS(NWT)	TEST 100
	NWT = NWT+MGPREG	TEST 110
	WTLOR = WTS(NWT)	TEST 120
	NWT = NWT+MGPREG	TEST 130
	WTAVR = WTS(NWT)	TEST 140
	IF (NKILL) 45,45,20	TEST 150
20	IF(WTLOR-ABS (WATE))40,40,25	TEST 160
25	IF(FLTRNF(NARG)*WTAVR-ABS (WATE))35,35,30	TEST 170
30	WATE=0.	TEST 180
	NWT = NWT + 6*MGPREG	TEST 190
	NWTS(NWT)=NWTS(NWT)+1	TEST 200
	NWT = NWT + MGPREG	TEST 210

	WTS(NWT) = WTS(NWT) + OLDWT	TEST 220
C	WEIGHT KILLED ENTERING COLLISION IS SCORED	TEST *
	WPSCL(11) = WPSCL(11) + 1	TEST 240
C	CALL BANKR(11) FOR R R KILL ANALYSIS	TEST 230
C	R R KILL	TEST 240
	RETURN	TEST 270
35	W1=WATE	TEST 280
	WATE=SIGN (WTAVR,W1)	TEST 290
	NWT = NWT + 8*MGPREG	TEST 300
	NWTS(NWT)=NWTS(NWT)+1	TEST 310
	NWT = NWT + MGPREG	TEST 320
	WTS(NWT) = WTS(NWT) + W1	TEST 330
C	WEIGHT ENTERING COLLISION (BUT BELOW WTLOR) AND SURVIVING IS SCORED	TEST *
	WPSCL(12) = WPSCL(12) + 1	TEST 350
C	CALL BANKR(12) FOR R R SURV ANALYSIS	TEST 310
C	R R SURVIVAL	TEST 320
	OLDWT=WATE	TEST 380
	RETURN	TEST 390
40	IF (NSPLT) 65,65,45	TEST 400
45	IF(WTHR-ABS (WATE)) 50, 65, 65	TEST 410
50	IF(NMOST-NS) 60,60,55	TEST 420
55	NS=NS+1	TEST 430
	NEWNM=NEWNM+1	TEST 440
	WATE=WATE*.5	TEST 450
	NAME1=NAME	TEST 460
	NAME=NEWNM	TEST 470
	CALL STORNT(NS,1)	TEST 480
	WPSCL(2) = WPSCL(2) + 1	TEST 490
C	CALL BANKR(2) FOR SPLIT DAUGHTER ANALYSIS	TEST 450
C	SPLITD	TEST 480
	NAME=NAME1	TEST 520
	OLDWT=WATE	TEST 530
	NWS = NWT+2*MGPREG	TEST 540
	NWTS(NWS) = NWTS(NWS)+1	TEST 550
	NWS = NWS + MGPREG	TEST 560
	WTS(NWS) = WTS(NWS) + WATE	TEST 570
C	WEIGHT AFTER SPLITTING IS SCORED	TEST *
	GO TO 45	TEST 590
60	NWS = NWT + 4*MGPREG	TEST 600
	NWTS(NWS) = NWTS(NWS)+1	TEST 610
	NWS = NWS + MGPREG	TEST 620
	WTS(NWS) = WTS(NWS) + WATE	TEST 630
C	WEIGHT WHICH COULD HAVE SPLIT IS SCORED	TEST *
65	RETURN	TEST 650
	END	TEST 680
	SUBROUTINE FTEST(SX, SY, SZ, M1, M2, NBAT, NPAR)	VAR2 10
C	NBAT IS THE NO. OF INDEPENDENT BATCHES	VAR2 20
C	NPAR IS THE TOTAL NUMBER OF PARTICLES PROCESSED	VAR2 30
C	IT IS ASSUMED THAT THE SUMSQ ARRAY HAS ACCUMULATED THE NUMBER OF PARTICLES	
C	TIMES THE SQUARE OF THE BATCH AVERAGE (THIS IS OBTAINED BY DIVIDING	50

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C     THE SQUARED BATCH SUM BY THE NUMBER OF PARTICLES STARTING THE BATCH) 60
REAL * 8 SX, SY, SZ, AN, AI, AJ, SSB, SSW, SST
DIMENSION SX(M1,M2), SY(M1,M2), SZ(M1,M2)          VAR2 70
AN = NPAR
AI = NBAT
AJ = AN/AI
DO 29 I=1,M1
DO 29 J=1,M2
    SSB = AJ*( SX(I,J)/AJ-SZ(I,J)**2/AJ/AN)
    SST = SY(I,J) - SZ(I,J)**2/AN
    SSW = SST - SSB
    SY(I,J) = (SSB/(AI-1.))/(SSW/(AI*(AJ-1.)))
C     SY(I,J) = DSQRT(SSB/(AI-1.)/AN)/(SZ(I,J)/AN)
C     SY(I,J) = DSQRT(SSW/(AI*(AJ-1.)/AN)/(SZ(I,J)/AN)
C     SY(I,J) = DSQRT(SST/(AN-1.)/AN)/(SZ(I,J)/AN)
29  CONTINUE
    RETURN          VAR2 240
    END            VAR2 250

    SUBROUTINE VAR2(SX,SX2,M1,M2,NBAT,NPAR)          VAR2 10
C     NBAT IS THE NO. OF INDEPENDENT BATCHES          VAR2 20
C     NPAR IS THE TOTAL NUMBER OF PARTICLES PROCESSED  VAR2 30
C     IT IS ASSUMED THAT THE SUMSQ ARRAY HAS ACCUMULATED THE NUMBER OF PARTICLES
C     TIMES THE SQUARE OF THE BATCH AVERAGE (THIS IS OBTAINED BY DIVIDING 50
C     THE SQUARED BATCH SUM BY THE NUMBER OF PARTICLES STARTING THE BATCH) 60
REAL * 8 SX, SX2, AN, DUM, BN, CN
DIMENSION SX(M1,M2),SX2(M1,M2)          VAR2 70
IF (NBAT-1) 5,5,15          VAR2 80
C**** WILSON  APRIL 20,1989 ****          MOR 1150
6     AN = NPAR          VAR2 130
    DO 29 I=1,M1          VAR2 160
    DO 29 J=1,M2          VAR2 170
    IF (SX(I,J)) 24,19,24          VAR2 180
19    SX2(I,J) = 0.0          VAR2 190
    GO TO 29          VAR2 200
C24  WRITE(6,651) SX(I,J),SX2(I,J),AN

C651  FORMAT(1H ,3(2X,1PE10.3))
24    DUM      = SX2(I,J)/AN - (SX(I,J)/AN)**2          VAR2 210
    SX2(I,J) = DSQRT(DABS(DUM)/AN)/(SX(I,J)/AN)          VAR2 220
C     WRITE(6,651) SX(I,J),SX2(I,J),DUM
29    CONTINUE          VAR2 230
C**** WILSON  APRIL 20,1989 ****          MOR 1150
    RETURN          VAR2 120
15    AN = NPAR          VAR2 130
    BN = NBAT          VAR2 140
    CN = DSQRT(BN - 1.)          VAR2 150
    DO 30 I=1,M1          VAR2 160
    DO 30 J=1,M2          VAR2 170
    IF (SX(I,J)) 26,20,26          VAR2 180
20    SX2(I,J) = 0.0          VAR2 190
    GO TO 30          VAR2 200

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26  DUM      = SX2(I,J)*AN - SX(I,J)**2          VAR2 210
    SX2(I,J) = DSQRT(DABS(DUM      ))/(SX(I,J)*CW)  VAR2 220
30  CONTINUE                                     VAR2 230
    RETURN                                       VAR2 240
    END                                         VAR2 250

    SUBROUTINE VAR3(SX,SX2,M1,M2,M3,NBAT,NPART)     VAR3 10
C   NBAT IS THE NO. OF INDEPENDENT BATCHES       VAR3 20
C   NPART IS THE TOTAL NUMBER OF PARTICLES PROCESSED  VAR3 30
C   IT IS ASSUMED THAT THE SUMSQ ARRAY HAS ACCUMULATED THE NUMBER OF PARTICLES
C   TIMES THE SQUARE OF THE BATCH AVERAGE (THIS IS OBTAINED BY DIVIDING 50
C   THE SQUARED BATCH SUM BY THE NUMBER OF PARTICLES STARTING THE BATCH) 60
    REAL * 8 SX, SX2, DUM
    DIMENSION SX(M1,M2,M3), SX2(M1,M2,M3)        VAR3 70
    CALL ERRSET( 208,300,-1,1,1,208)
    IF (NBAT-1) 5,5,15                            VAR3 80
5   DO 10 I=1,M1                                  VAR3 90
    DO 10 J=1,M2                                  VAR3 100
    DO 10 K=1,M3                                  VAR3 110
    IF (SX2(I,J,K)) 24,19,24                      VAR3 110
19  SX2(I,J,K) = 0.0                             VAR3 120
    GO TO 10
24  DUM      = SX2(I,J,K)/AN - (SX(I,J,K)/AN)**2  VAR2 210
    SX2(I,J,K) = DSQRT(DABS(DUM)/AN)/(SX(I,J,K)/AN)  VAR2 220
10  CONTINUE                                     VAR3 130
    RETURN                                       VAR3 130
15  DO 30 I=1,M1                                  VAR3 140
    DO 30 J=1,M2                                  VAR3 150
    DO 30 K=1,M3                                  VAR3 160
    IF (SX(I,J,K)) 25,20,25                      VAR3 170
20  SX2(I,J,K) = 0.0                             VAR3 180
    GO TO 30                                     VAR3 190
25  SX2(I,J,K) = (SX2(I,J,K)/NPART-(SX(I,J,K)/NPART)**2)/(NBAT-1.)  VAR3 200
    IF (SX2(I,J,K).LT.1.E-70) GO TO 30
    SX2(I,J,K) = DSQRT(DABS(SX2(I,J,K)))/SX(I,J,K)*NPART  VAR3 210
30  CONTINUE                                     VAR3 220
    CALL ERRSET( 208, 10,-1,1,1,208)
    RETURN                                       VAR3 230
    END                                         VAR3 240

    SUBROUTINE VAR4(SX,SX2,SX3,SX4,SX5,SX6,
    *M1,M2,NBAT,NPART,IPL)                       VAR2 10
C   NBAT IS THE NO. OF INDEPENDENT BATCHES       VAR2 20
C   NPART IS THE TOTAL NUMBER OF PARTICLES PROCESSED  VAR2 30
C   IT IS ASSUMED THAT THE SUMSQ ARRAY HAS ACCUMULATED THE NUMBER OF PARTICLES
C   TIMES THE SQUARE OF THE BATCH AVERAGE (THIS IS OBTAINED BY DIVIDING 50
C   THE SQUARED BATCH SUM BY THE NUMBER OF PARTICLES STARTING THE BATCH) 60
    REAL * 8 AN, X1, X2, X3, X4, DUM2, DUM4, DUM42
    REAL * 8 SX, SX2, SX3, SX4, SX5, SX6
    REAL * 8 BETA, BETAJ, S2, S4, AJ, V2S2, V2SL
    DIMENSION SX(M1,M2),SX2(M1,M2),SX3(M1,M2),SX4(M1,M2),SX5(M1,M2)  VAR2 70
    *,SX6(M1,M2)

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C**** WILSON   APRIL 20,1989 ****
AN = NPART
AJ = NPART/51.
DO 29 I=1,M1
DO 29 J=1,N2
IF (SX(I,J)) 24,19,24
19 SX2(I,J) = 0.0
SX5(I,J) = 0.0
GO TO 29
24 X1      = (1./AN)*SX(I,J)
X2      = (1./AN)*SX2(I,J)
X3      = (1./AN)*SX3(I,J)
X4      = (1./AN)*SX4(I,J)
S2      = X2 - X1**2
C      S4      = X4-4.*X1*X3+8.*X1**2*X2-4.*X1**4-X2**2
S4      = X4-4.*X1*X3+6.*X1**2*X2-3.*X1**4
BETA    = S4/S2**2
BETAJ   = BETA/AJ + 3.*(AJ-1.)/AJ
V2S2    = 1./51.*(BETAJ - 48./50.)
C      IF(IFL .GT.0) GO TO 51
V2SL    = (1./AN)*(BETA-(AN-3.)/(AN-1))
SX5 (I,J) = DSQRT(DABS(V2S2/4.))
C51 SX2 (I,J) = DSQRT(DABS( S2)/AN)/(SX(I,J)/AN)
SX2 (I,J) = DSQRT(DABS( S2)/AN)/(SX(I,J)/AN)
SX6 (I,J) = DSQRT(DABS(V2SL/4.))
29 CONTINUE
RETURN
END

```

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NOB 1150
VAR2 130
VAR2 160
VAR2 170
VAR2 180
VAR2 190
VAR2 200
VAR2 210
VAR2 220
VAR2 220
VAR2 230
VAR2 240
VAR2 250

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Appendix D

Derivation of Some Equations of Chapter 2

The derivations in this appendix are found in Hansen, Hurwitz, and Madow [7].

D.1 Derivation of Equation 2.38

Equation 2.38 in Section 2.4 is given by

$$V_{S^2}^2 = \frac{1}{N} \left(\beta - \frac{N-3}{N-1} \right), \quad (\text{D.1})$$

where

$$\beta = \frac{\mu_4}{(\sigma^2)^2}, \quad (\text{D.2})$$

$$\sigma^2 = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})^2, \quad (\text{D.3})$$

and

$$\mu_4 = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})^4. \quad (\text{D.4})$$

Proof:

The relative variance of the variance is given by

$$V_{S^2}^2 = \frac{\sigma_{S^2}^2}{(S^2)^2}. \quad (\text{D.5})$$

By definition

$$V_{S^2}^2 = \frac{E(S^2 - ES^2)^2}{(ES^2)^2} = \frac{E(S^2 - \sigma^2)^2}{(\sigma^2)^2} = \frac{ES^4 - \sigma^4}{\sigma^4}. \quad (\text{D.6})$$

To evaluate ES^4 the following transformation is used:

$$z_i - \mu = z_i \quad (D.7)$$

$$\bar{z} - \mu = \bar{z}, \quad (D.8)$$

which gives

$$ES^4 = E \left[\frac{\sum^N (z_i - \bar{z})^2}{N-1} \right]^2, \quad (D.9)$$

$$ES^4 = \frac{1}{(N-1)^2} E \left[\left(\sum^N (z_i^2)^2 - 2N\bar{z}^2 \sum^N z_i^2 + N^2\bar{z}^4 \right) \right], \quad (D.10)$$

where

$$\left(\sum^N (z_i^2) \right)^2 = \sum^N z_i^4 + \sum_{i \neq j}^N z_i^2 z_j^2, \quad (D.11)$$

$$\bar{z}^2 \sum^N z_i^2 = \frac{1}{N^2} \left[\sum^N z_i^4 + 2 \sum_{i \neq j}^N z_i^2 z_j^2 + \sum_{i \neq j}^N z_i^2 z_j^2 + \sum_{i \neq j \neq k}^N z_i^2 z_j z_k \right], \quad (D.12)$$

and

$$\bar{z}^4 = \frac{1}{N^4} \left[\sum^N z_i^4 + 4 \sum_{i \neq j}^N z_i^2 z_j^2 + 3 \sum_{i \neq j}^N z_i^2 z_j^2 + 6 \sum_{i \neq j \neq k}^N z_i^2 z_j z_k + \sum_{i \neq j \neq k \neq m}^N z_i^2 z_j z_k z_m \right]. \quad (D.13)$$

For sampling with replacement, independent samples, and using the fact that $Ez_j = 0$, when $i \neq j \neq k \neq m$ it follows that

$$Ez_i^2 z_j^2 = Ez_i^2 Ez_j^2, \quad (D.14)$$

$$Ez_i^2 z_j = Ez_i^2 Ez_j = 0, \quad (D.15)$$

$$Ez_i^2 z_j z_k = Ez_i^2 Ez_j Ez_k = 0, \quad (D.16)$$

and

$$Ez_i^2 z_j z_k z_m = Ez_i^2 Ez_j Ez_k Ez_m = 0. \quad (D.17)$$

Therefore

$$E \left(\sum^N (z_i^2) \right)^2 = N\mu_4 + N(N-1)\sigma^4, \quad (D.18)$$

$$E\bar{z}^2 \sum z_i^2 = \frac{1}{N^2} [N\mu_4 + N(N-1)\sigma^4], \quad (\text{D.19})$$

and

$$E\bar{z}^4 = \frac{1}{N^4} [N\mu_4 + 3N(N-1)\sigma^4]. \quad (\text{D.20})$$

Substituting equations D.18, D.19, and D.20 in Equation D.6, subtracting and dividing by σ^4

$$V_{S^2}^2 = \frac{1}{N} \left(\beta - \frac{N-3}{N-1} \right). \quad (\text{D.21})$$

D.2 Derivation of Equations 2.46 and 2.47

For I random groups of J elements

$$V_{S^2}^2 = \frac{1}{I} \left(\beta_J - \frac{J-3}{J-1} \right), \quad (\text{D.22})$$

where

$$\beta_J = \frac{\beta}{J} + 3 \frac{J-1}{J}. \quad (\text{D.23})$$

Proof:

In Chapter 2 it was shown that

$$S_b^2 = \frac{J}{I-1} \sum_{i=1}^I (\bar{x}_i - \bar{x})^2. \quad (\text{D.24})$$

The relative variance of S_b^2 is also given by

$$V_{S_b^2}^2 = \frac{\sigma_{S_b^2}^2}{(\sigma^2)^2}. \quad (\text{D.25})$$

Similar to Equation D.6

$$V_{S_b^2}^2 = \frac{ES_b^4 - \sigma^4}{\sigma^4}. \quad (\text{D.26})$$

Using the following transformation:

$$\bar{x}_i - \mu = \bar{z}_i \quad (\text{D.27})$$

$$\bar{x} - \mu = \bar{z}, \quad (\text{D.28})$$

Equation D.24 can be written as

$$S_b^2 = \frac{J}{I-1} \sum_{i=1}^I (\bar{z}_i - \bar{z})^2, \quad (\text{D.29})$$

which gives

$$ES_b^4 = \frac{J^2}{(I-1)^2} E \left[\sum_i^I (\bar{z}_i - \bar{z})^2 \right]^2, \quad (\text{D.30})$$

or

$$ES_b^4 = \frac{J^2}{(I-1)^2} E \left[\left(\sum_i^I \bar{z}_i^2 \right)^2 - 2I\bar{z}^2 \sum_i^I \bar{z}_i^2 + I^2\bar{z}^4 \right]. \quad (\text{D.31})$$

The first term of Equation D.31 is given by

$$E \left(\sum_i^I \bar{z}_i^2 \right)^2 = E \sum_i^I \bar{z}_i^4 + E \sum_{i \neq h}^I \bar{z}_i^2 \bar{z}_h^2, \quad (\text{D.32})$$

$$E \left(\sum_i^I \bar{z}_i^2 \right)^2 = E \sum_i^I \left(\frac{\sum_j^J z_{ij}}{J} \right)^4 + E \sum_{i \neq h}^I \left(\frac{\sum_j^J z_{ij}}{J} \right)^2 \left(\frac{\sum_j^J z_{ih}}{J} \right)^2, \quad (\text{D.33})$$

which gives

$$E \left(\sum_i^I \bar{z}_i^2 \right)^2 = I \left[\frac{\mu_4}{J^3} + \frac{3(J-1)\sigma^4}{J^3} \right] + I(I-1) \frac{\sigma^4}{J^2}. \quad (\text{D.34})$$

The second term in Equation D.31 is given by

$$E \left(2I\bar{z}^2 \sum_i^I \bar{z}_i^2 \right) = 2IE \left[\left(\frac{\sum_i^I \bar{z}_i}{I} \right)^2 \sum_i^I \bar{z}_i^2 \right] = \frac{2}{I} E \left(\sum_i^I \bar{z}_i^2 \right), \quad (\text{D.35})$$

which becomes

$$E \left(2I\bar{z}^2 \sum_i^I \bar{z}_i^2 \right) = 2 \left[\frac{\mu_4}{J^3} + \frac{3(J-1)\sigma^4}{J^3} \right] + 2(I-1) \frac{\sigma^4}{J^2}. \quad (\text{D.36})$$

The third term in Equation D.31 becomes

$$EI^2\bar{z}^4 = \frac{1}{I^2} E \left(\sum_i^I \bar{z}_i \right)^4 = \frac{1}{I^2} E \left(\sum_i^I \bar{z}_i^4 + 3 \sum_{i \neq h}^I \bar{z}_i^2 \bar{z}_h^2 \right), \quad (\text{D.37})$$

which gives

$$EI^2\bar{z}^4 = \frac{1}{I^2} \left\{ I \left[\frac{\mu_4}{J^3} + \frac{3(J-1)\sigma^4}{J^3} \right] + 3I(I-1) \frac{\sigma^4}{J^2} \right\}. \quad (\text{D.38})$$

Substituting equations D.34, D.36, and D.38 in Equation D.31 Es_0^4 will be given by

$$Es_0^4 = \frac{\mu_4}{JJ} + \frac{3(J-1)}{IJ} \sigma^4 + \frac{I^2 - 2I + 3}{(I-1)I} \sigma^4. \quad (D.39)$$

Substituting Equation D.39 in Equation D.26

$$V_{S_0^2}^2 = \frac{1}{I} \left[\frac{1}{J} \frac{\mu_4}{\sigma^4} + \frac{3(J-1)}{J} - \frac{I-3}{I-1} \right], \quad (D.40)$$

$$V_{S_0^2}^2 = \frac{1}{I} \left[\frac{\beta}{J} + \frac{3(J-1)}{J} - \frac{I-3}{I-1} \right], \quad (D.41)$$

or finally

$$V_{S_0^2}^2 = \frac{1}{I} \left(\beta_J - \frac{I-3}{I-1} \right). \quad (D.42)$$

D.3 Derivation of Equation 2.48

In terms of the relative variance Equation 2.48 in Section 2.4 can be written as

$$V_S^2 = \frac{V_{S_0^2}^2}{4}. \quad (D.43)$$

Proof:

Since

$$E(S - \sigma)^2 = ES^2 - 2\sigma ES + \sigma^2 = 2\sigma(\sigma - ES), \quad (D.44)$$

then

$$V_S^2 = 2 \left(\frac{\sigma - ES}{\sigma} \right). \quad (D.45)$$

Using the expansion

$$\frac{S - \sigma}{\sigma} = \frac{(S^2 - \sigma^2)}{2\sigma^2} - \frac{(S^2 - \sigma^2)^2}{8\sigma^4} + \frac{(S^2 - \sigma^2)^3}{16\sigma^6} - \dots \quad (D.46)$$

it follows that

$$\frac{\sigma - ES}{\sigma} = \frac{1}{8\sigma^4} E(S^2 - \sigma^2)^2 - \frac{1}{16\sigma^6} E(S^2 - \sigma^2)^3 + \dots \quad (D.47)$$

Since

$$\frac{V_S^2}{2} = \frac{\sigma - ES}{\sigma}, \quad (D.48)$$

Equation D.47 becomes

$$\frac{V_S^2}{2} = \frac{V_{S^2}^2}{8} - \frac{1}{16\sigma^6} E(S^2 - \sigma^2)^3 + \dots \quad (\text{D.49})$$

Finally for sufficiently large N

$$V_S^2 = \frac{V_{S^2}^2}{4}. \quad (\text{D.50})$$

VITA

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