PRODUÇÃO TECNICO CIENTÍFICA DO IPEN DEVOLVER NO BALCÃO DE EMPRÉSTIMO

6755

SPECIMEN NUMBER REQUIREMENTS FOR T sub(o) ACCURACY

C.A.J MIRANDA, C.J.; LANDES, J.D.

ASTM MAY MEETING.WORKSHOP ON USER'S EXPERIENCE WITH THE FRACTURE TOUGHNESS MASTER CURVE, ATLANTA, USA, MAY 1-9, 1998 (VIEWGRAPHS)

ATLANTA 198 MEETING MAY Trabalho wompeto 1-9,1998 MAY d'up este. TITULO FINAL: (oventer, do anton) en Number Requirements for To Accuracy " "Specimen considerer 2 antres copie de quantejes vel Calos Alexadre de J. Minada REC 9198 IPEN-DOC- 6755

CONFIDENCE/LEVEL IN THE REFEREN ú í palido TEMPERATURE (F.) DETERMINATION

Carlos A. J. Miranda - *IPEN-CNEN/SP, SP, Brazil* On leave to *University of Tennessee at Knoxville, USA*

John D. Landes - University of Tennessee at Knoxville, USA

Atlanta, GA, USA --- May, 1998

SCOPE:

Find the Confidence Level for a given number of toughness values to determine T_o (the Master Curve).

RESULTS:

(1) the confidence of the obtained T_o with a given set of experimental results,

(2) the minimum number of experimental results necessary to have a given confidence level in the obtained T_0 .

units: MPa \sqrt{m} (toughness) and °C (temperature)

PREVIOUS WORK - 'Direct' Approach

1. Two ideal finite sets, with NTOT = [20, 40] toughness values each fitting perfectly the Weibull Three Parameter Distribution Three (T-T_o)_u or T_{o,u} values were used: [-50, 0, +50] (°C)

2. All subsets were sampled

Calculate $(T-T_o)_s$ or $T_{o,s}$ for each subset. NSET = [3, 4, 5, 6, 8, 10]

3. A distribution of $T_{o,s}$ was defined

4. Find the probability of $|T_{0,u} - T_{0,s}| \le 10$ °C

5. Range of $T_{o,s}$ divided in three regions: 1st region: $T_{o,s} < T_{o,u} - 10^{\circ}C$ 2nd region: $T_{o,u} - 10^{\circ}C < T_{o,s} < T_{o,u} + 10^{\circ}C ==>$ confidence level 3rd region: $T_{o,s} > T_{o,u} + 10^{\circ}C$

6. Results depended too much on NTOT ----> approach impractical with NTOT >> 40 -----> New Approach (from Wallin)

PRESENT WORK - 'Monte Carlo' Approach - Outline

1. $T_{o,u}$ values: [-100, -75, -50, -25, 0, 25, 50, 75, 100] (°C)

2. NSET from [3, 4, 5, 6, 8, 10, 14, 20, 25, 35, 50, 100]

3. Let **NTOT** = ∞

Probabilities (P) will be sampled as random numbers, $(0 \le P \le 1)$ Toughness values Fitting the Weibull Three Parameter Distribution

- 4. How many subsets to give good results? Tested 10^3 , 10^4 , 10^5 OK for $\ge 10^4$ subsets ===> 3*10^4 subsets
- **5. Distribution of T_{oys} \longrightarrow (T-T_o)_s**

6. Find the probability of $|T_{0,u} - T_{0,s}| \le 10$ °C ===> Confidence Level

Analyses Performed in 4 Steps

WORK METHODOLOGY 4 Steps

infinite values of probabilities P, ($0 \le P \le 1$), associated with a given T_{o,u} value

Step 1 – K₀, calculation

Obtain $K_{Jc,med}$ (P = 0.5)

$$KJc, med = 30 + 70e^{0.019(T-To)}$$
 (1)

Obtain K_o, using $K_{Jc,med}$ and $K_{min} = 20 \text{ MPa}\sqrt{m}$

Ko, u =
$$\left(\frac{KJc, med - K\min}{0.9124}\right) + K\min$$
⁽²⁾

Now, at each time, a set with NSET probabilities *Pi* will be randomly sampled.

Step 2 - Obtain NSET toughness values (K_{Jc,i})

Obtain K_{Jc,i} for each probability P_i , using the previously calculated $K_{o,u}$

$$1 - P_i = \exp(-\left[\frac{KJc, i - K_{\min}}{K_{o,u} - K_{\min}}\right]^m), \ K_{\min} = 20, \ m = 4$$
(3)

Step 3 - Treating each set with NSET values

Obtain $K_{o,s}$ associated with this set.

$$Ko, s = \left(\frac{\sum_{i=1}^{NSET} (KJc, i - K \min)^{m}}{NSET - 0.3068}\right)^{1/4} + K \min$$
(4)

Obtain K_{Jc,med}

$$Ko, s = \left(\frac{KJc, med - K \min}{0.9124}\right) + K \min$$
⁽²⁾

Obtain $(T-T_o)_s$ or $(T_{o,s})$ *KJc*, *med* = $30 + 70e^{0.019(T-To)}$ ⁽¹⁾

***** repeat steps 2 and 3 ($3*10^4$ times) for each NSET value *****

Step 4 – **Treating the Results**

1. $T_{o,s}$ or $(T-T_o)_s$ Distributions

2. Curves "Relative (%) Counting X NSET".

probability of $|T_{0,u} - T_{0,s}| \le 10$ °C ===> Confidence Level

3. Curves "Minimum NSET versus $T_{o,u}$ " for each Confidence Level

for 70%, 80%, 90%, 95% and 98% of confidence

4. Fitting the curves "Minimum NSET versus T_{0,u}"

1st - Exponential Equation

fit the curves "Minimum NSET versus T_{o,u}", for each confidence value

2nd - Third Degree Polynomium.

fit the coefficients of the Exponential Equation

5. Curves "Confidence Level versus $T_{o,u}$ " for each NSET for NSET = [3, 4, 5, 6, 7, 8, 9, 10, 12, 14, 16, 18, 20, 25, 30]





Typical Distribution of $T_{o,s}$ for each $T_{o,u}$ - for NSET = 8







Fitting the Curves "Minimum NSET versus T_{0,u}"

$$MinNSET = a_i + b_i e^{\frac{-(T-T_o)}{C_i}}$$
⁽⁵⁾

i	Confid. Level	a _i	b _i	C _i
1	(0.70) 70%	3.00	0.12	28.06
2	(0.80) 80%	3.18	0.75	41.99
3	(0.90) 90%	5.24	1.22	41.59
4	(0.95) 95%	7.40	1.88	42.66
5	(0.98) 98%	10.94	2.41	40.76
	x		Coefficients	<u> </u>

Coefficients to Fit the Curves "Minimum NSET versus T_{o,u}"

Fitting the Coefficients a_i, b_i, c_i

$$\{a_i; b_i; c_i\} = d_j + e_j x + f_j x^2 + g_j x^3$$
 (6)

Coefficients d_j , e_j , f_j and g_j

		Coefficients						
j		dj	ej	f_j	gi			
1	Coeff. a_i	-404.75	1581.7	-2042.8	879.0			
2	Coeff. b_i	-116.65	428.6	-525.6	216.5			
3	Coeff. c_i	-1389.9	4745.1	-5217.9	1904.1			



Original (continuous line) and Fitted (dotted line) curves



DISCUSSION

- **1.** The distributions of $T_{o,s}$ become narrower as NSET increases.
- **2.** The range of the $T_{o,s}$ values shows a reduction as NSET increases. For the lower NSETs this reduction is noticeable for the greater $T_{o,u}$
- **3.** The presented results, are directly tied to the assumption that $|T_{o,u} T_{o,s}| \le 10$ °C is allowed

If this spread value is reduced the number of specimens to be tested to give a certain confidence level will increase.

4. The 3rd region $(T_{o,u} - T_{o,s}) \ge 10$ °C could be considered in the Confidence definition.

This would bring some benefit to those sets with, in average, less than 7 values This option was not adopted to allow some conservatism in the proposed curves

5. No censoring was performed in the sampled sets

CONCLUSION

- The Confidence Level in the T_o determination varies with the number of specimens. This dependence was obtained numerically and presented graphically.
- 2. The showed results give the Confidence Level for a set of toughness measurements as a function of the position on the Master Curve.

Ex.: using 6 specimens the Confidence Level is greater than 90% only when the test is conducted above $(T-T_0) = 25$ °C.

- 3. There is no big benefit in testing at the region at $(T-T_o) > 50 \text{ °C}$. Due to the uncertainties no tests should be performed at $(T-T_o) \le -50 \text{ °C}$
- 4. The best range for testing is $-25 \text{ °C} \leq (T-T_o) \leq 50 \text{ °C}$

"Minimum NSET versus $(T-T_o)_u$ " as function of the Confidence level

$$MinNSET = a + b e^{\frac{-(T-T_o)}{C}}$$

and

$$\{a ; b ; c \} = d_j + e_j x + f_j x^2 + g_j x^3$$

	Coefficients						
j	d _i	ej	fj	g _i			
1 (Coeff. a)	-404.75	1581.7	-2042.8	879.0			
2 (Coeff. b)	-116.65	428.6	-525.6	216.5			
3 (Coeff. <i>c</i>)	-1389.9	4745.1	-5217.9	1904.1			

x = [0.70 - 0.98] is the desired Confidence Level in the T_o determination

 $(T-T_o)$ is the position of the Master Curve



 $(T-T_o)_s$ Distributions for $(T-T_o)_u = -50$. °C NSET = [3, 4, 5, 6, 8, 10, 14, 20, 25, 35, 50, 100]

 $(T-T_o)_s$ Distributions for $(T-T_o)_u = -25$. °C NSET = [3, 4, 5, 6, 8, 10, 14, 20, 25, 35, 50, 100]



 $(T-T_o)_s$ Distributions for $(T-T_o)_u = 0.0$ °C NSET = [3, 4, 5, 6, 8, 10, 14, 20, 25, 35, 50, 100]

 $(T-T_o)_s$ Distributions for $(T-T_o)_u = +50.$ °C NSET = [3, 4, 5, 6, 8, 10, 14, 20, 25, 35, 50, 100]





 $(T-T_o)_s$ Distributions for NSET = 6



 $(T-T_o)_s$ Distributions for NSET = 10

 $(T-T_o)_s$ Distributions for NSET = 20



Relative Counting in Region #1 (T - T_o)_s < $T_{o,u}$ - 10. °C

Relative Counting in Region #3 $(T - T_o)_s > T_{o,u} + 10.$ °C

Table: Relative (%) Counting in Each Region (Range) (The Confidence Level is the Counting in the Region #2)

			N	GRO 50	JPs	NC 30	OMB 000	Se 3000	ed 001	To] 10.	-			
				Con	fido	nco	Post	1+0	(2)					
	Range Range Range	e #1: e #2: e #3:	olo olo olo	of of of	th "	e val "	ues	unde betwe ove	(°) er en er	Delta] Delta] Delta]	Γ - Τς Γ+/-Τς Γ + Τς)1)1)1		
т-то	Range	NSET 03	NSE (ET N)4	1SET 05	NSET 06	NSET 08	NSET 10	NSEI 14	NSET	NSET 25	NSET 35	NSET 50	NSET 100
-100.	#1 #2 #3	29.6 47.3 23.1	25. 53. 20.	.92 .95	22.9 59.5 17.5	20.2 64.8 15.0	17.0 71.9 11.2	14.2 77.2 8.6	9.7 84.8 5.5	6.1 91.1 2.8	4.2 94.2 1.6	2.0 97.4 .5	.7 99.2 .1	.0 100.0 .0
-75.	#1 #2 #3	24.6 56.6 18.8	21. 64. 14.	.01 .37	L7.9 70.4 L1.7	15.5 74.8 9.7	12.0 81.1 6.9	9.4 86.0 4.6	5.8 91.8 2.4	2.9 96.1 .9	1.8 97.9 .4	.6 99.3 .1	.1 99.9 .0	.0 100.0 .0
-50.	#1 #2 #3	21.0 64.0 15.0	17. 71. 11.	.3 1 .7 7	L4.2 77.5 8.2	12.2 81.5 6.3	8.5 87.4 4.1	6.4 91.2 2.4	3.5 95.6 .9	5 1.5 5 98.2 9 .3	.7 99.3 .1	.2 99.8 .0	.0 100.0 .0	.0 100.0 .0
-25.	#1 #2 #3	18.1 69.6 12.3	14 76 8	.7 1 .6 8 .7	11.5 32.4 6.1	9.3 86.3 4.4	6.5 91.0 2.5	4.6 94.0 1.5	2.1 97.4	.7 99.2	.4 99.6 .0	.1 99.9 .0	.0 100.0 .0	.0 100.0 .0
0.	#1 #2 #3	16.7 72.6 10.7	12 80 7	.5 1 .2 8 .3	10.0 34.9 5.1	7.9 88.7 3.4	5.1 93.2 1.8	3.1 95.9 1.0	1.4 98.3	.5 3 99.5 3 .0	.2 99.8 .0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0
25.	#1 #2 #3	15.3 75.2 9.5	11 82 6	.8 .1 8 .1	9.2 36.7 4.1	7.2 89.9 2.8	4.3 94.3 1.4	2.9 96.4 .7	1.1 98.7 .2	.3 99.7 2.0	.1 99.9 .0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0
50.	#1 #2 #3	14.3 77.0 8.7	11 83 5	.1 .2 8 .6	8.2 38.1 3.7	6.5 91.0 2.5	3.9 95.0 1.0	2.4 97.1 .5	99.(1.	9.8 99.8 .0	.1 99.9 .0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0
75.	#1 #2 #3	14.1 77.6 8.3	10 84 5	.4 .3 8 .3	8.2 88.4 3.4	5.9 91.9 2.2	3.3 95.6 1.1	2.2 97.4 .4	.8 99.1 1.	3.2 99.8 .0	.1 99.9 .0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0
100.	#1 #2 #3	13.7 78.6 7.7	10 84 5	.0 .8 8	7.7 89.1 3.2	5.7 92.2 2.1	3.3 95.8 .9	2.0 97.6 .4	. 6 99. 3 . 1	5.2 399.8 1.0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0	.0 100.0 .0

.

Table: Minimum and Maximum $(T-T_o)_s$

.

	Max/M	lin Va	lues c	of (T-I	o) _s for	each	NSET	and	$(T-T_{o})$	u Ana	lyzed	
T-To	NSET	NSET	NSET	NSET	NSET	NSET	NSET	NSET	NSET	NSET	NSET	NSET
	03	04	05	06	08	10	14	20	25	30	35	100
-100.	-434	-270	-207	-217	-210	-157	-135	-134	-125	-122	-115	-112
	-62	-64	-60	-69	-74	-73	-77	-80	-83	-85	-88	-87
-75.	-310	-203	-147	-130	-136	-115	-113	-99	-96	-91	-89	-84
	-40	-45	-47	-49	-50	-51	-56	-59	-60	-61	-64	-67
-50.	-143	-121	-101	-95	-92	-83	-75	-70	-69	-63	-61	-58
	-17	-24	-26	-25	-29	-31	-32	-35	-38	-39	-40	-43
-25.	-93	-85	-67	-64	-56	-56	-47	-41	-39	-39	-34	-31
	0	0	0	-5	-7	-6	-8	-12	-12	-15	-16	-19
0.	-76	-59	-45	-39	-27	-29	-19	-17	-14	-13	-9	-6
	25	21	22	18	16	14	14	11	10	9	8	6
25.	-38	-18	-15	- 9	-3	-3	6	6	10	13	15	17
	48	47	47	4 4	42	40	38	35	35	34	32	30
50.	-9	-4	7	7	25	. 24	30	33	37	38	40	43
	75	73	71	68	66	64	63	61	60	58	57	55
75.	19	26	40	44	50	51	54	60	61	62	65	68
	98	95	94	91	90	88	87	86	84	83	81	79
100.	42	58	64	67	74	79	82	81	86	89	91	94
	123	123	117	116	116	113	112	110	109	109	106	105

Table: CONFIDENCE (%) Level as Function of the NSET Value, for each (T-To)u

.

. .

(T-T _o) _u	NSET=3	NSET=4	NSET=5	NSET=6	NSET=7	NSET=8	NSET=9	NSET=10
-100.	47.30	53.90	59.50	64.80	68.57	71.90	74.67	77.20
-75.	56.60	64.30	70.40	74.80	78.12	81.10	83.71	86.00
-50.	64.00	71.70	77.50	81.50	84.71	87.40	89.43	91.20
-25.	69.60	76.60	82.40	86.30	88.86	91.00	92.60	94.00
Ο.	72.60	80.20	84.90	88.70	91.17	93.20	94.67	95.90
25.	75.20	82.10	86.70	89.90	92.38	94.30	95.42	96.40
50.	77.00	83.20	88.10	91.00	93.23	95.00	96.14	97.10
75.	77.60	84.30	88.40	91.90	93.98	95.60	96.57	97.40
100.	78.60	84.80	89.10	92.20	94.22	95.80	96.77	97.60

(T-T _o) _u	NSET=12	NSET=14	NSET=16	NSET=18	NSET=20	NSET=25	NSET=30	NSET=40
-100.	81.34	84.80	87.21	89.31	91.10	94.20	96.00	98.08
-75.	89.19	91.80	93.49	94.92	96.10	97.90	98.70	99.52
-50.	93.66	95.60	96.62	97.48	98.20	99.30	99.58	99.87
-25.	95.92	97.40	98.16	98.76	99.20	99.60	99.77	99.93
Ο.	97.26	98.30	98.80	99.20	99.50	99.80	99.92	100.00
25.	97.71	98.70	99.12	99.45	99.70	99.90	99.96	100.00
50.	98.18	99.00	99.34	99.61	99.80	99.90	99.96	100.00
75.	98.37	99.10	99.40	99.63	99.80	99.90	99.96	100.00
100.	98.58	99.30	99.49	99.66	99.80	100.00	100.00	100.00

Porte 11 tents complete **100 YEARS** Source of the World-Renowned Annual Book of ASTM Standards Standards for Materials, Products, Systems and Services **A PROVEN PARTNERSHIP** MAY MEETING ATLANTA HILTON AND TOWERS CENTURY of PROGRESS ASTM: 1898 - 1998 ATLANTA, GEORGIA MAY 1-9, 1998 100 YEARS A 100 Barr Harbor Drive, West Conshohocken, PA 19428-2959 610-832-9500 A PROVEN PARTNERSHIP try to complet o 6755 00-03

COMMITTEE E08 CONTINUED

Surface Cracks Monday .07 .03 [Crystal E] 9:00A-11:00A **Dynamics Fracture Toughness** Monday .05 11:00A-12:00N [Crystal E] Welds (Joint with 08.08.07) .07 Monday 1:00P-3:00P [Crystal E] Elastic-Plastic Fracture .08 Tuesday 3:30P-5:00P [Ballroom A] Crack Initiation, Growth, Frac. .02 Tuesday Under Elas.- Plas. Cond. 10:30A-12:30P [Ballroom A] Analytical Tech. And Proced. .04 Tuesday [Ballroom A] 9:30A-10:30A **CTOD Concepts and Procedures** .06 Tuesday [Ballroom A] 1:30P-3:30P .07 Welds (Joint with 08.07.07) Monday [Crystal E] 1:00P-3:00P .09 Advanced Materials and Their Composites Monday [Crystal C] 9:00A-10:30A .01 Student Paper Workshop Wednesday 9:30A-12:00N [Walton] **Fatigue Lecture** Wednesday [DeKalb] 5:00P-6:00P **ISO** Meeting Friday [Embassy] 8:00A-5:00P .05 Workshop on Micro and Nano Scale Wednesday Structures 9:30A-5:00P [DeKalb] Workshop on Users Experience ŧ .07 Wednesday w/The Fracture Toughness Master 1:00P-5:00P Curve [Walton]

Symposium on Mixed Mode Crack Behavior [Crystal F/G]	Wednesday 9:30A-5:15P
[Salon E]	Thursday 8:25A-4:50P
Complete program appears in abstract booklet i	n rear of room

COMMITTEE E20 ON TEMPERATURE MEASUREMENT (Room names in brackets)

Main Briefing [Salon C]

Main Closing [Crystal B]

.90 Executive [Salon A]

.91 Editorial and Terminology [Salon C]

Colloquium [Salon A]

.03 Resistance Thermometry [Salon C]

> .01 Task Group [Salon C]

.04 Thermocouples Briefing [Salon A]

> Thermocouples Report [Crystal B]

ASME [Crystal B]

[Council]

.01 Thermocouples Testing [Salon A]

.02 Thermocouples Materials and Use [Crystal B]

.03 Thermocouples Specifications [Salon A]

.06 New Thermometers and Techniques [Salon C]

.07 Fundamentals [Salon C]

80.

.05 Infrared Thermometry [Rockdale]

> Infrared Thermometry Report [Rockdale]

Monday 8:15A-8:30A

....

Wednesday 10:00A-10:30A

Tuesday 2:00P-4:30P

Monday 7:00P-9:00P

Tuesday 1:00P-2:00P

Monday 1:00P-3:00P

Monday 8:30A-11:00A

Tuesday 8:00A-8:15A

Wednesday 9:30A-10:00A

Tuesday 3:00P-6:00P

Wednesday 1:00P-4:00P

Tuesday 10:15A-12:00N

Wednesday 8:00A-9:30A

Tuesday 8:15A-10:00A

Monday 11:00A-12:00N

Monday 3:00P-6:00P

Monday 8:30A-12:00N

Monday 1:00P-3:00P

31

30

Attendees



Workshop on User's Experience with Fracture Toughness Master Curve Atlanta, May 6, 1998

T. L. Anderson President SRT - Structural Reliability Technology Suite 235, 1898 South Flatiron Court Boulder, CO 80301

B. R. Bass Oak Ridge National Laboratory P.O. Box 2009, MS-8056 Oak Ridge, TN 37831-8056

R. H. Dodds Department of Civil Engineering MC-250 2129 Newmark Laboratory University of Illinois 204 Matthews Avenue Urbana, IL 61801-2397

H. Ito Engineering Science Program 310 Perkins Hall The University of Tennessee Knoxville TN 37996-2030

> J. A. Joyce U.S. Naval Academy Mechanical Engineering Department 590 Holloway Road MS 11C Annapolis, MD 21402

M. T. Kirk Science and Technology Center Westinghouse Electric Corporation 1310 Beulah Road Pittsburgh, PA 15235-5098

J. D. Landes Engineering Science Program 310 Perkins Hall The University of Tennessee Knoxville TN 37996-2030

+ Kim. WALLIN + D. E. McCabe R. E. Link
U.S. Naval Academy
Mechanical Engineering Dept.
590 Holloway Road
Annapolis, MD 21402

C. A. Miranda Engineering Science Program 310 Perkins Hall The University of Tennessee Knoxville TN 37996-2030

D. Scavone Knolls Atomic Power Laboratory Bin 159 1 River Road Schenectady, NY 12301

K. H. Schwalbe GKSS-Forschungszentrum Postfach 1160 21494 Geesthacht GERMANY

J. A. Strharsky Westinghouse PAD 500 Penn Center Boulevard Pittsburgh, PA 15239

W. A. Van der Sluys Babcock and Wilcox 1562 Beeson Street Alliance, OH 44601

K. K. Yoon Framatome Technologies, Inc. 3315 Old Forest Road P.O. Box 10935 Lynchburg, VA 24506-0935

Workshop on User's Experience with the Fracture Toughness Master Curve

May 6, 1998 Atlanta, GA

Chair: T. Anderson, SRT Cochair: D. McCabe, ORNL

- 1. "Overview of the EU Project on Fracture Toughness of Steel in the Ductile to Brittle Transition Regime." J. Heerens, GKSS, Germany.
- 2. "Master Curve Analysis of Data from the European Round-Robin Testing Program." K. Wallin, VTT Manufacturing Technology, Finland.
- 3. "Constraint Effects on Measured To Values: Results of 3-D Numerical Studies." R.H. Dodds Jr., University of Illinois.
- 4. "Bias and Accuracy of ASTM E 1921 Values for Reactor Pressure Vessel Steels." M.T. Kirk, Westinghouse.
- 5. "Activities of the PVRC Task Group on the Master Curve." W.A. Vandersluys, Babcock & Wilcox.
- 6. "Dynamic Fracture Toughness Tests of Linde 80 Welds Using E 1921." K. Yoon, Framatone Technology.
- 7. "Specimen Number Requirements for To Accuracy." C. Miranda, University of > felte ater anter Tennessee.
- 8. Open Discussion.

+ Dr. Landa Dr. Christofer withon. Dr. Ted Anderson Dr. McCabe



100 Barr Harbor Drive
West Conshohocken, PA 19428-2959
Telephone: 610-832-9500
Fax: 610-832-9555
e-mail: service@astm.org
Website: www.astm.org

July 2, 1998

CARLOS MIRANDA UNIVERSITY OF TENNESSEE 350 SUTHERLAND AVE, KNOXVILLE TN 37919

Dear Colleague:

Thank you for your attendance at the Committee E08 on FATIGUE AND FRACTURE standards development meetings which were held MAY 1-9, 1998 in ATLANTA, GA.

You are invited to join ASTM and Committee E08. A membership application is enclosed along with the pamphlet "What is ASTM? If you are already a member of ASTM and Committee E08, please pass the enclosed application on to one of your colleagues.

For \$65 annually you may participate as an individual, representing either yourself or the company you are employed by in the increasingly important standards-writing community, or for \$350 as the official representative of an organizational membership. Benefits of each class of membership are described on the reverse of the application.

As a member you will receive many tangible benefits, including our monthly magazine, <u>Standardization News</u>; one free volume of the ASTM Book of Standards, to be sent to you upon payment of your administrative fee; affiliation with the technical committees in your area of interest; and reduced prices on ASTM journals and Special Technical Publications (STP's).

There are also significant intangible advantages of membership, including the professional contacts made with others in your field of interest, knowledge gained through committee work, and other participation in the Society's activities—even life and health insurance at attractive group rates.

The next meeting of Committee E08 will be held November 2-4, 1998 in Norfolk, VA.

For additional information on ASTM or the Committee, please call, Bode Buckley, Staff Manager of Committee E08, at 610-832-9740. I look forward to your participation in the Society's activities!

Sincerely,

In Richter

Anne Richter Administrative Assistant Membership Promotion

Enclosures