

# EPITHERMAL NEUTRON FLUX CHARACTERIZATION OF THE IEA-R1 RESEARCH REACTOR, SAO PAULO, BRAZIL, FOR USE IN INAA.

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## ABSTRACT

The nonideality of the epithermal neutron flux distribution at a reactor site parameter ( $\alpha$ ) and the thermal-to-epithermal neutron ratio ( $f$ ) were determined in three typical irradiation positions of the IEA-R1 reactor of IPEN-CNEN/SP, Sao Paulo, Brazil, using the "Cd-ratio for multimonitor" and "bare bi-isotopic monitor" -methods respectively. This characterization is to be used in the  $K_0$ -method of NAA, recently introduced at the IPEN.

## INTRODUCTION

When applying the  $K_0$ -method of instrumental ( $n,\gamma$ ) activation analysis with reactor neutrons (INAA), it is found that the general accepted  $1/E_n$ -epithermal neutron flux distribution is not often acceptable from the standpoint of the analysis accuracy [1]. The use of the semiempirical representation [2,3] is better;

$$\varphi_e(E_n) \sim 1/E^{1+\alpha}$$

which was proved to be satisfactory for INAA needs [4] and where  $\alpha$  is a measure of the epithermal flux deviation from the ideal, and is a characteristic of the reactor irradiation position. Both positive and negative  $\alpha$ -values are reported in the literature [5], corresponding to "softened" and a "hardened" epithermal spectrum, as compared to the ideal one. This is illustrated in Fig. 1. The  $1/E^{1+\alpha}$  representation enables easy correction of the resonance integral (and hence of the analytical result) for the deviating epithermal spectrum [4]. Thus, when calculating the concentration of an element in a sample,  $\alpha$  should be known to preserve the accuracy of the analysis.

100 45

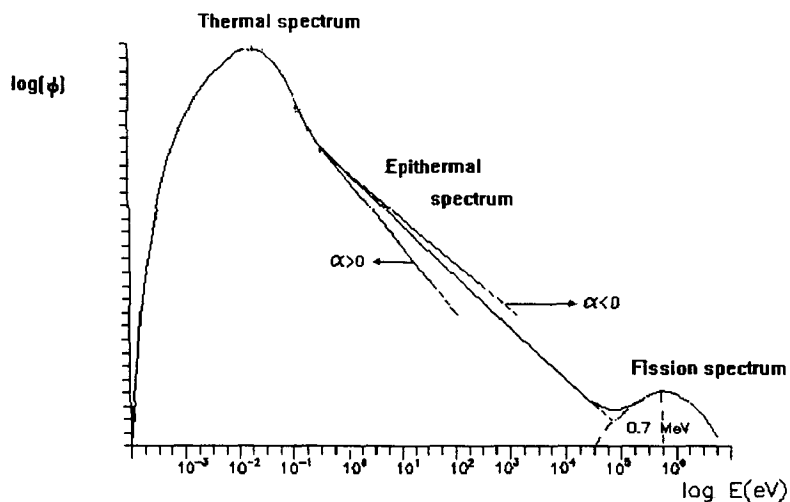


Figure 1.-Epithermal spectrum nonideality.

With the same aim, the thermal (subcadmium)-to-epithermal ratio -  $f = \Phi_{th}/\Phi_e$  must be well known [6]. The designation "subcadmium" refers to the definition of  $\Phi_{th}$ , the conventional thermal fluence rate, as  $\Phi_{th} = n_s v_0$  where  $v_0$  is the  $2200 \text{ m.s}^{-1}$  neutron velocity and  $n_s$  is the "subcadmium" neutron density up to  $0.55 \text{ eV}$  neutron energy. On the other hand,  $\Phi_e$  - the conventional epithermal neutron fluence rate, is defined as the true epithermal neutron fluence rate per unit  $\ln E$  interval. The use of  $f$  is strictly associated with  $Q_0$  (the resonance integral to  $2200 \text{ ms}^{-1}$  cross section ratio), both parameters being linked to the Høgdahl convention [7], on which the application of the  $K_0$ -method is based.

## EXPERIMENTAL AND RESULTS

All through this work we investigate  $\alpha$  and  $f$  in the three characteristic irradiation channels of the IEA-R1 reactor, i.e., in the "pneumatic transfer tube channel" (Station 4) and in the positions EIRA-24B and EIRA-36B (fixed systems for large irradiation).

We use thin high pure foils as  $\alpha$ -monitors considering the self-shielding effects (0.125 mm Zr, 0.125 mm Au, 0.05 mm Co<sub>2</sub>). Relevant nuclear data for the nuclides chosen as monitors are given in Table 1. So as to obtain good statistics on  $A_{sp}$  values, the irradiation was repeated 3 times. In all studied positions, the monitors were irradiated during 30 minutes. After appropriate cooling times (24 – 48 h),  $\gamma$ -activities were measured on a HPGe (CANBERRA GMX20190, 1.9 keV for 1332 keV line of  $^{60}\text{Co}$ ). All monitor spectra were processed using the VISPECT system, developed at IPEN.

Table 1.- Nuclear data for the nuclides chosen as monitors [8,9]

Monitor	$E_r$ , eV	$Q_0$	$G_{th}^*$	$G_{epi}^*$	$F_{Cd}$	$\gamma$ -line, keV	$T_{1/2}$
$^{197}\text{Au}(n,\gamma)^{198}\text{Au}$	$5.65 \pm 0.40$	$15.7 \pm 0.28$	0.989	0.755	0.991	411.8	2.695 d
$^{59}\text{Co}(n,\gamma)^{60}\text{Co}$	$136 \pm 7$	$1.990 \pm 0.054$	0.986	0.950	1	1173.0	5.271 y
$^{96}\text{Zr}(n,\gamma)^{97}\text{Zr}$	$338 \pm 7$	$248.0 \pm 0.4$	1	0.966	1	743.6	16.74 h
$^{94}\text{Zr}(n,\gamma)^{95}\text{Zr}$	$6260 \pm 250$	$5.05 \pm 0.10$	1	0.987	1	(724.2 + 756.7)	64.033 d

\* - Calculated by program CCOMP [10], using the De Corte methodology [11] and considering the Doppler effect.

The epithermal spectrum shape factor  $\alpha$  was obtained [8] as the slope ( $-\alpha$ ) of the straight line when plotting  $\log(T_i)$  versus  $\log(E_{r,i}/1 \text{ eV})$ , which comes to the same as solving the implicit equation (1 eV omitted):

$$\alpha + \frac{\sum_1^N \left\{ \left[ \log(E_{r,i}) - \frac{\sum_1^N \log(E_{r,i})}{N} \right] \left[ \log(T_i) - \frac{\sum_1^N \log(T_i)}{N} \right] \right\}}{\sum_1^N \left[ \log(E_{r,i}) - \frac{\sum_1^N \log(E_{r,i})}{N} \right]^2} = 0$$

where  $N$  is the number of coirradiated  $\alpha$ -monitors,  $E_{r,i}$  - the average resonance energy of the monitor  $i$  and  $T_i$  was given by the "Cd-covered multi-monitor method" [12] as

$$T_i = \frac{(E_{r,i})^{-\alpha} (A_{sp,i})_{Cd}}{k_{0,Au}(i) \varepsilon_{p,i} F_{Cd,i} Q_{0,i}(\alpha) G_{e,i}}$$

with  $A_{sp} = (N_p/t_m)/SDCw$ , where  $N_p$  - measured net peak area,  $t_m$  - counting time,  $S$  - saturation factor,  $D$  - decay factor,  $C$  - counting factor and  $w$  - sample mass (in grams).  $k_{0,Au}$  - tabulated  $k_0$ -factors,  $\varepsilon_{p,i}$  - detector efficiency for used  $\gamma$ -line,  $F_{Cd,i}$  - Cd-transmission factor and  $G_e$  is the correction factors for epithermal neutron self-shielding.

The thermal-to-epithermal neutron flux ratio ( $f$ ) was determined by the "bare bi-isotopic monitor" method using Zr [13] as

$$f = \frac{G_{e,1} \frac{k_{0,Au}(1) \varepsilon_{p,1}}{k_{0,Au}(2) \varepsilon_{p,1}} Q_{0,1}(\alpha) - G_{e,2} \frac{A_{sp,1}}{A_{sp,2}} Q_{0,2}(\alpha)}{G_{th,2} \frac{A_{sp,1}}{A_{sp,2}} - G_{th,1} \frac{k_{0,Au}(1) \varepsilon_{p,1}}{k_{0,Au}(2) \varepsilon_{p,1}}}$$

were 1 =  $^{97}\text{Zr}/^{97m}\text{Nb}$  (743 keV), 2 =  $^{95}\text{Zr}$  (724.2 + 756.7 keV),  $G_{th}$  - the correction factors for thermal neutron self-shielding and  $\varepsilon_{p,1} = \varepsilon_{p,2}$ . Due to the single-decayed gamma lines, it is allowed to position the Zr monitor as close as possible to the detector cap.

Table 2 shows the obtained results for  $\alpha$  and  $f$ . Average values and all statistic processing was performed using the BABXEL system. The quoted uncertainties were calculated according to the error propagation study given in [12]. Though relatively high (~10-30%), such inherent  $\alpha$ -uncertainties are satisfactory for NAA needs, due to the large error reduction factor when calculating the concentration in the absolute or a single comparator method [4]. In this regard, large relative uncertainties are acceptable for lower absolute  $\alpha$ 's.

Table 2.-  $\alpha$  and  $f$ -values determined in the irradiation positions of the IEA-R1M reactor.

Channel	$\alpha$ (Cd-ratio)	$f$ (bare)
PT	$0.16 \pm 0.01$	$11.1 \pm 0.6$
EIRA-24B	$0.14 \pm 0.01$	$26.5 \pm 0.2$
EIRA-36B	$0.15 \pm 0.01$	$31.2 \pm 0.3$

Positive  $\alpha$ -values correspond to a "softened" (strongly thermalized) epithermal spectrum, which is indeed to be expected due to the reactor configuration and to  $^{235}\text{U}$  enrichment (<20%) in the fuel elements [14]. The practically non-variation of  $\alpha$  values in all studied position is relevant. The relative low  $f$ -value in the pneumatic channel is evidence of the presence of a great portion of fast neutron in that position.

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