
Workshop on Optimization of Service Life of Operating Nuclear Power Plants

Participation of Research Institutes in Angra's PLiM

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. Center of Nuclear Engineering (CEN)

. Division of Structural Mechanics (CENM)

Activities to Support ETN

(on demand)

1. Structural Integrity of SG Tubing

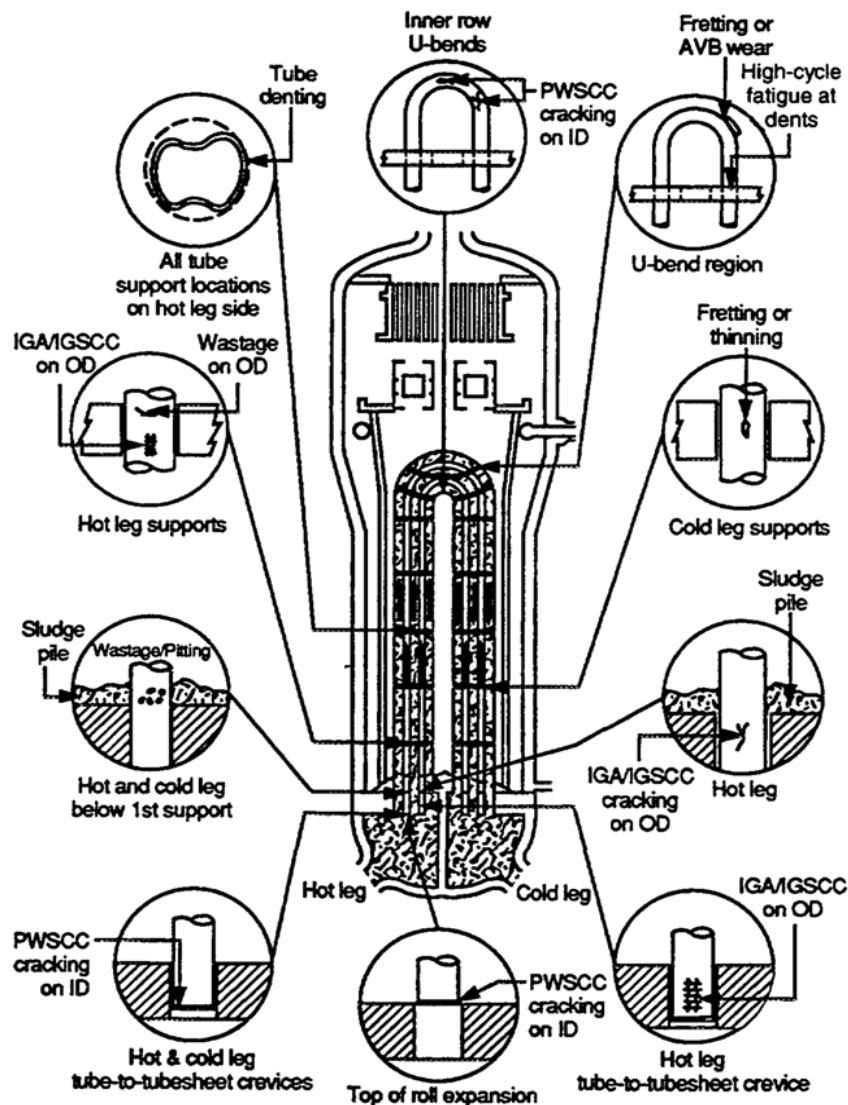
- . **Deterministic Approach (*Initial*)**
- . **Probabilistic Approach**
(Based on EPRI's Correlations
with Monte-Carlo Simulations)

2. Courses

- . **Fracture Mechanics**
- . **Structural Integrity Assessment**
- . **Codes and Standards**
- . **Piping and Mechanical Components**

Deterministic Approach

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1998-1999
 Research on the
 degradation
 mechanisms in PWR
 Steam generators

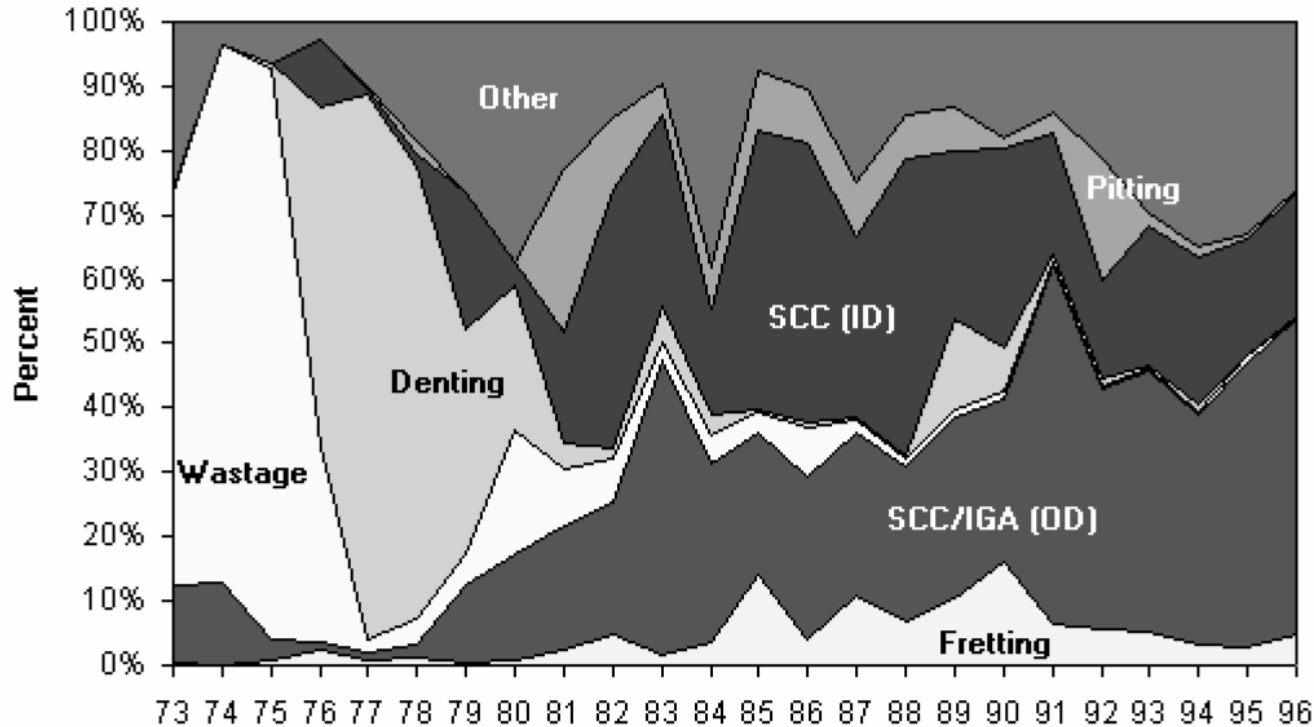
IAEA-TECDOC-981
 (1997)

Assessment and
 management of ageing
 of major
 nuclear power plant
 components
 important to safety:
 Steam generators

FIG. 14. Locations of known tube wall degradations in recirculating steam generators.
 (Courtesy of K. J. Krzywosz of the Electric Power Research Institute NDE Center; modified.)

1998-1999

Research on the degradation mechanisms in PWR Steam generators



Worldwide causes of SG plugging (EPRI, 1997)

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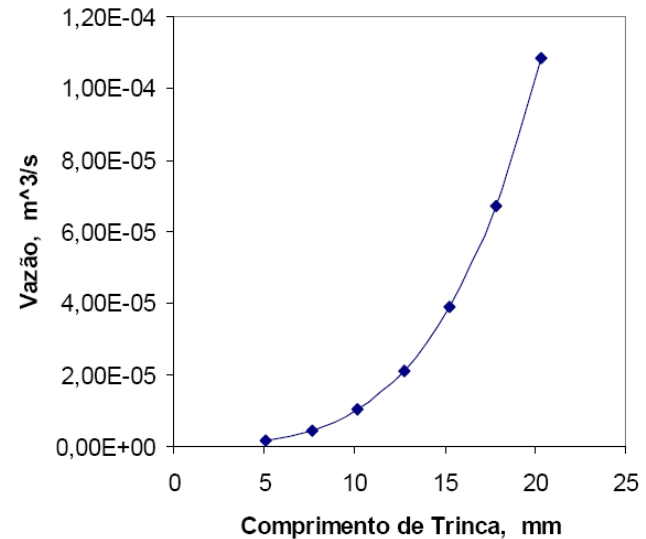
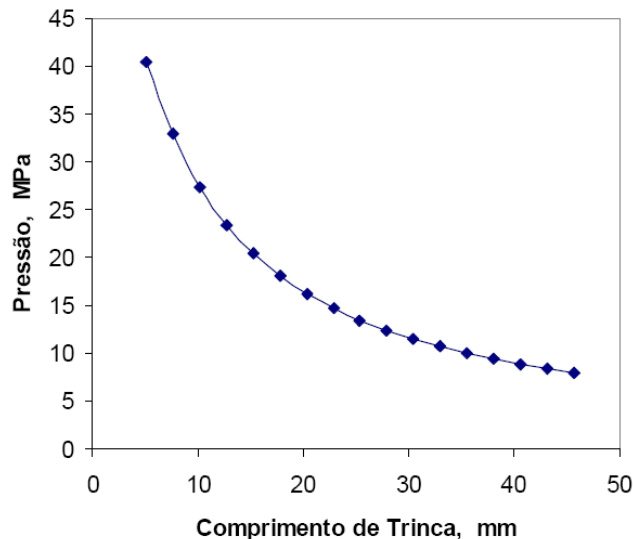
1998-2000

SG Tubes Plugging Criteria – PWSCC in Roll Transition Zone (near the tube sheet)

Axial cracks, with any depth, in RTZ are acceptable if

$$A = a + a_{\text{esp}} - a_{\text{cres}} - a_{\text{ins}}$$

where **A** is the crack length over the tube sheet, **a** is the burst crack length for the worst pressure condition, **a_{esp}** is the correction due to the tube sheet, **a_{cres}** is the tolerance for the crack growth to the next inspection and **a_{ins}** is the measurement error in inspections



2000

SG Tubes Plugging Criteria – ODS/SCC in Support plates -
Based on Bobbin coil voltage limits

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2000 - ...

STRUCTURAL INTEGRITY ASSESSMENT OF STEAM GENERATOR TUBES USING PROBABILISTIC APPROACHES

A fundamental step in tube plugging management is the tube structural integrity evaluation considering different defects, found in in-service inspections (Non-Destructive Examination - NDE), and how to consider the involved uncertainties. These defects arise from different degradation modes under several reactor operational conditions.

The probabilistic approaches, based on experimental results obtained from several and different tube defects morphology, use statistics to consider the uncertainties to assess structural limits of PWR SG tubes.

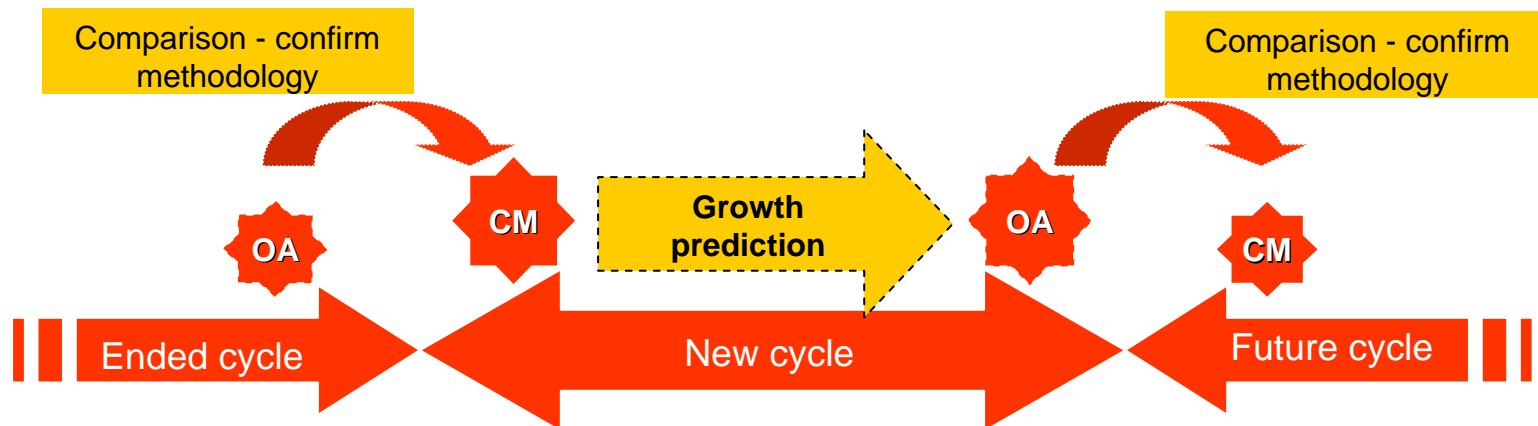
Besides, more sophisticated statistics methods, as Monte Carlo, allow simplified and less conservative analyses as well.

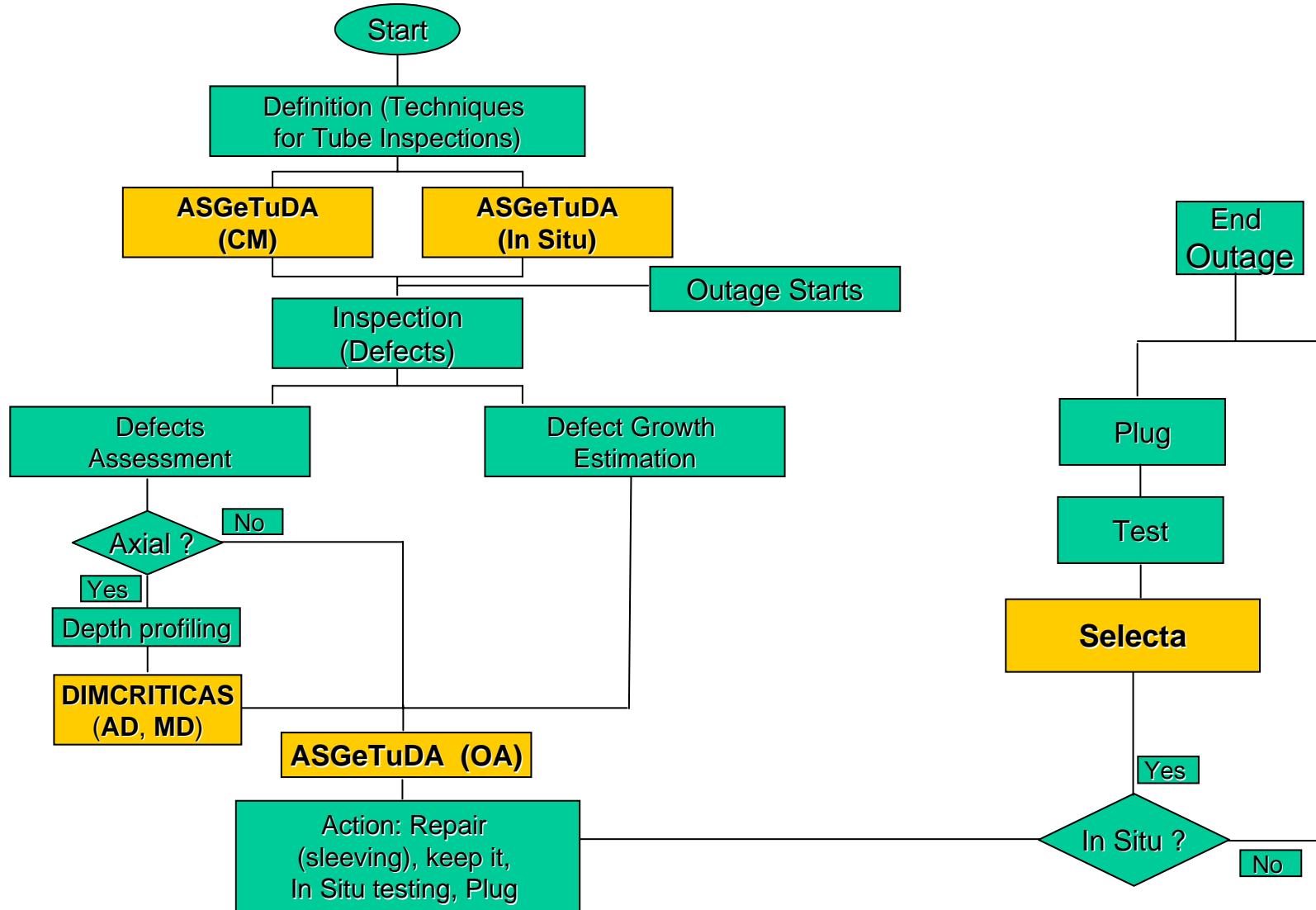
CM & OA

$$PB_{des} (= \Delta P) = \max(3,0 * \Delta P_{oper}, 1,4 * \Delta P_{acid})$$

For any defect, the tube burst pressure PB , associated with the “CM” or with the “OA” condition should be evaluated with probability of 0.95 with 50% confidence

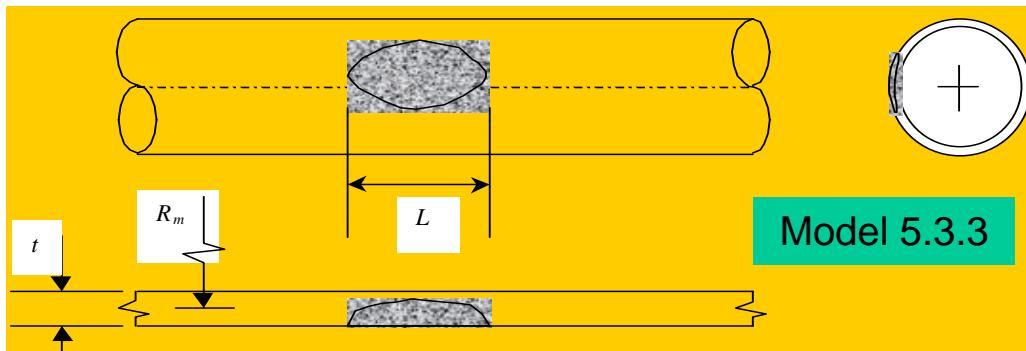
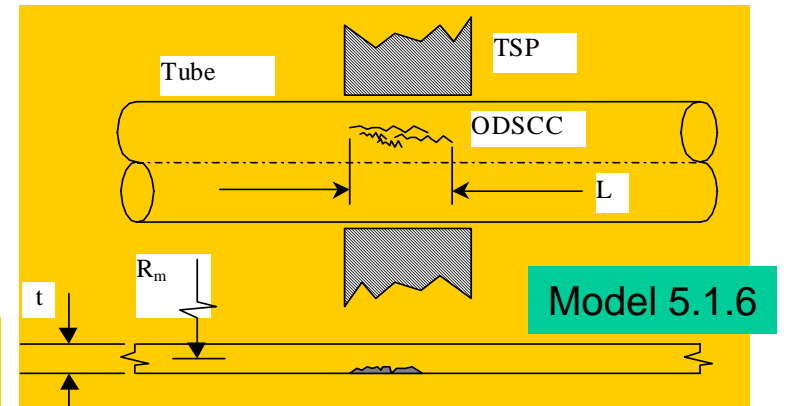
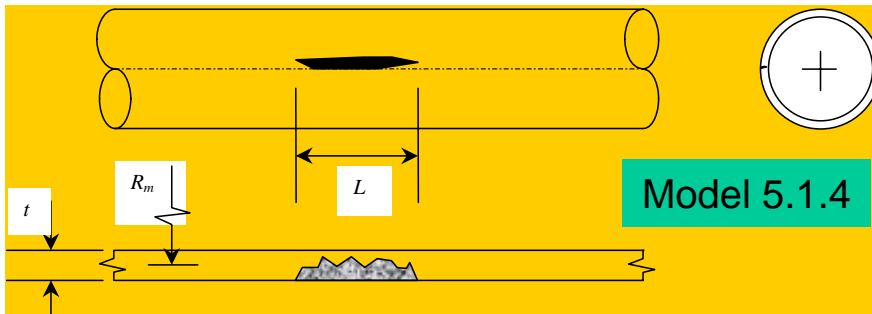
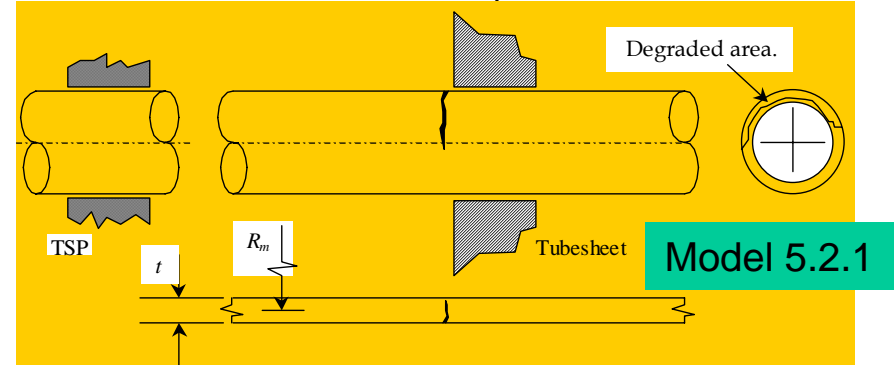
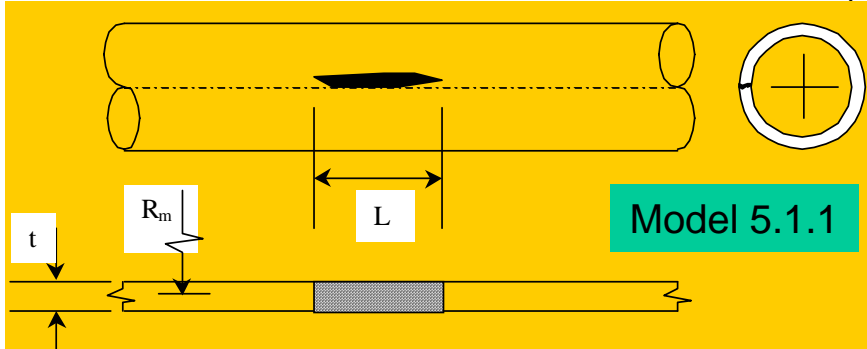
→ in 95% of the occasions the tubes with some defect (size) will not burst when the pressure reaches PB_{des}





- . Obtain the defect critical parameters/dimensions against tube burst to:
 - . Structural integrity analyses (CM & OA)
 - . Selection of tubes candidates to be tested **In Situ**
- . Developed in MATLAB language
- . Customized to Angra 1 (*generic data not associated with defects*):
 - . differential pressure (primary – secondary)
 - . Tube geometry – nominal diameter, thickness and internal radius
 - . Tube material - (Sy+Su) average and standard deviation
 - . Number of the Monte Carlo Simulations

Some Models/Defects (from EPRI *Flaw Handbook*):

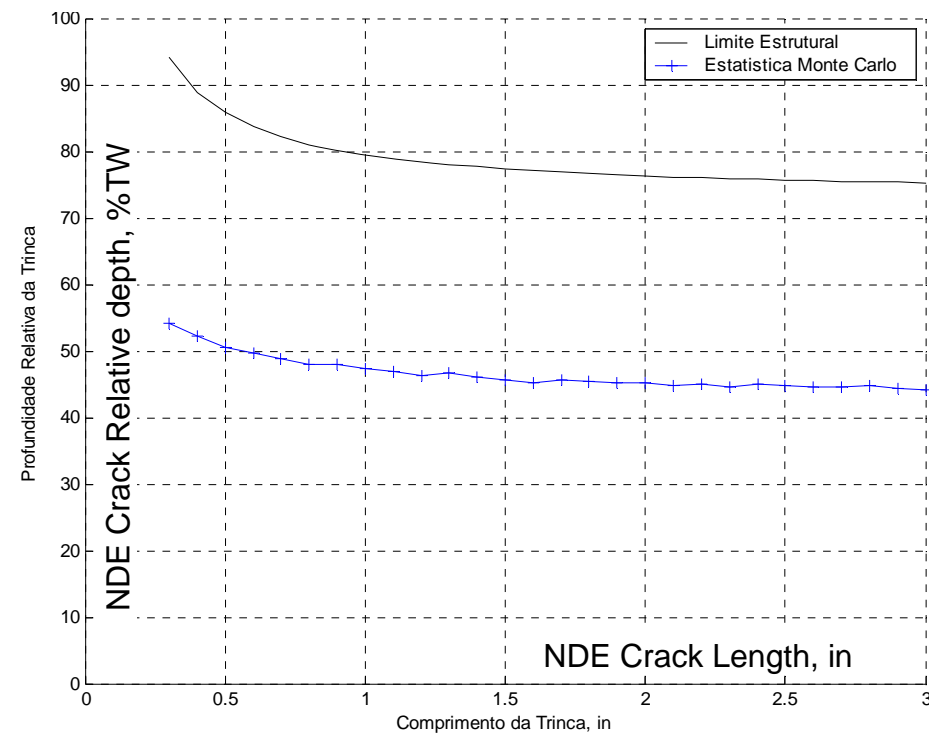
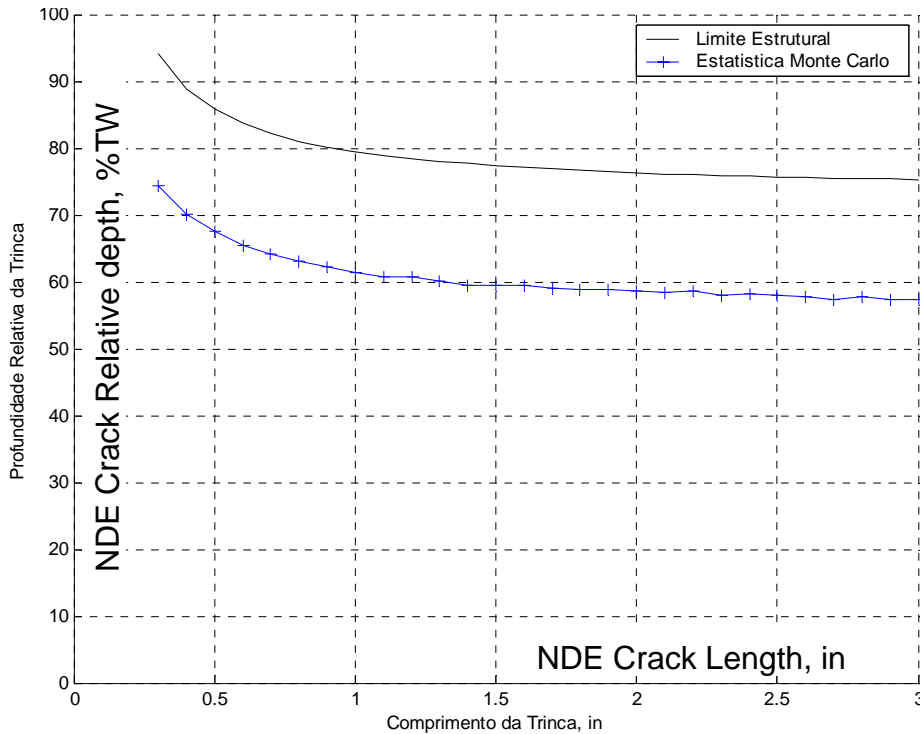


+ Model 5.3.1

Ex.1: Axial Partial Throughwall Defect (OD) - CM/OA

Length, L: $L_x = Ca_L * L_{NDE} + Cb_L$
 $Ca_L = 1.00; Cb_L = 0.00$ in } **CM**
 Std dev, $\sigma L_{NDE} = 0.10$ in }
 Growth: MeanGrowth_L = 0.25 in } **OA**
 SDevGr_L = 0.10 in }

Depth, h: $h_x = Ca_H * h_{NDE} + Cb_H$
 $Ca_H = 1.01; Cb_H = 0.00$ % } **CM**
 Std dev, $\sigma H_{NDE} = 11$ % }
 Growth: MeanGrowth_H = 5.0 % } **OA**
 SDevGr_H = 5.0 % }



Ex. 2: ODSCC at TSP, 3/4" Drilled Tube - CM/OA

Bobbin Coil Voltage, BCV

$$BCV_x = Ca_{BCV} * BCV_{nde} + Cb_{BCV}$$

$$Ca_{BCV} = 1.00$$

$$Cb_{BCV} = 0.00 \text{ (Volt)}$$

$$\text{Std deviation, } \sigma_{BCV} = 0.30 \text{ (Volt)}$$

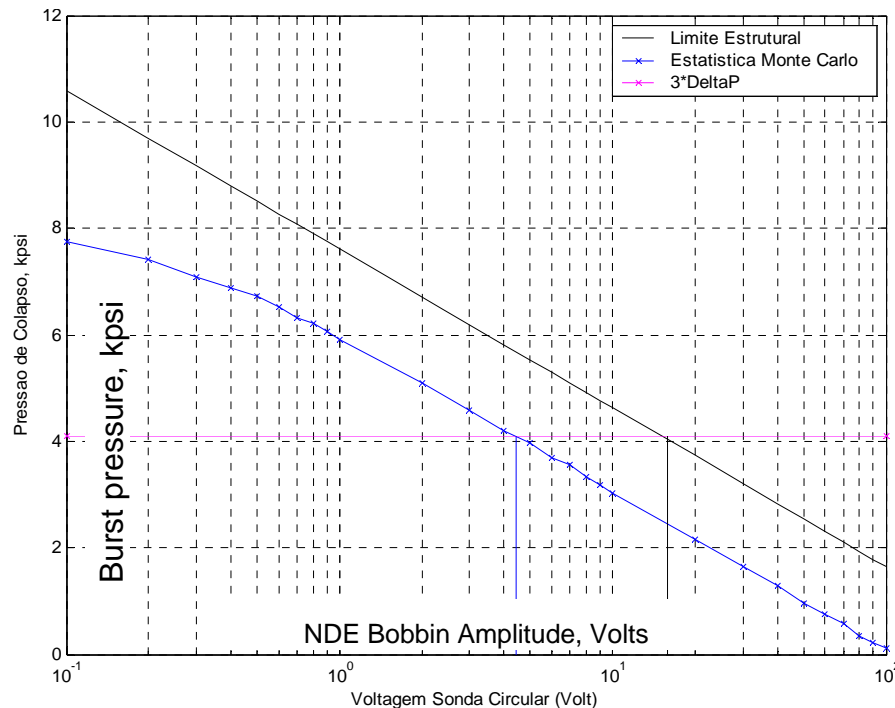
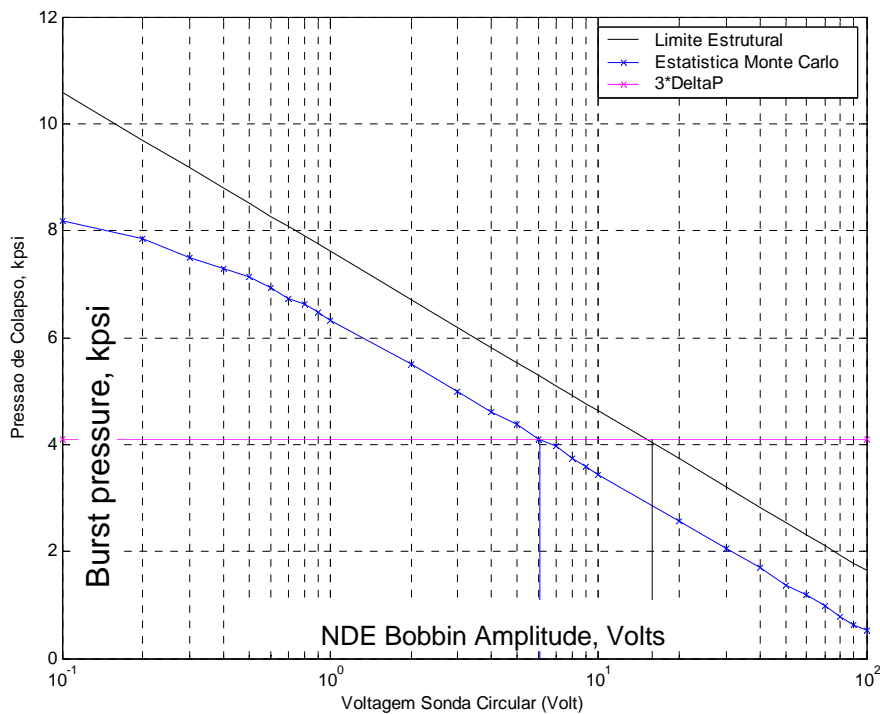
} **CM**

Growth:

$$\text{MeanGrowth}_{BCV} = 0.25 \text{ (Volt)}$$

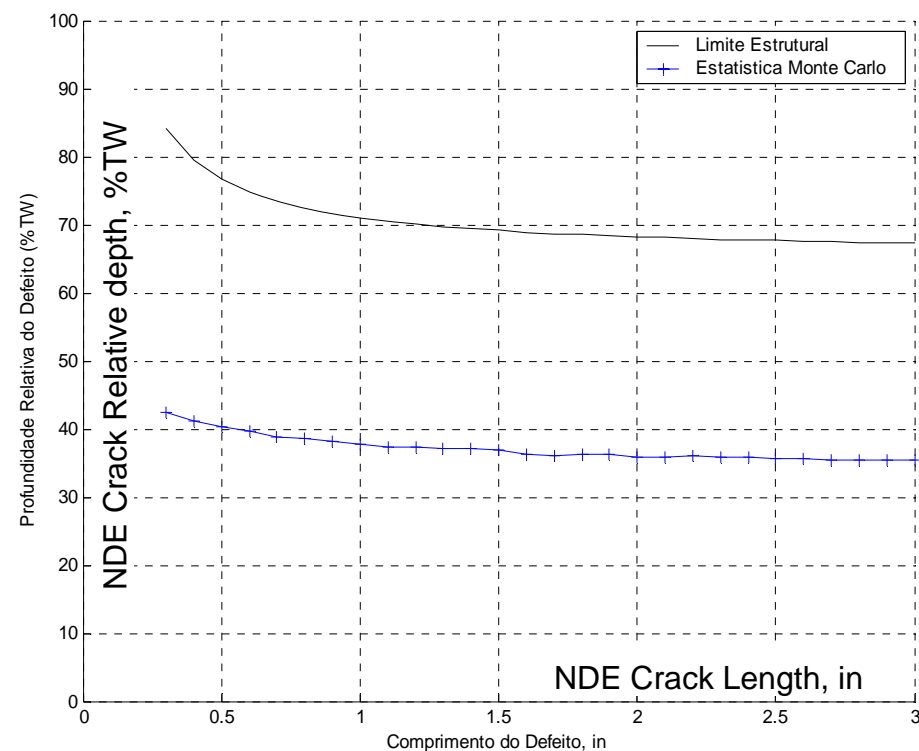
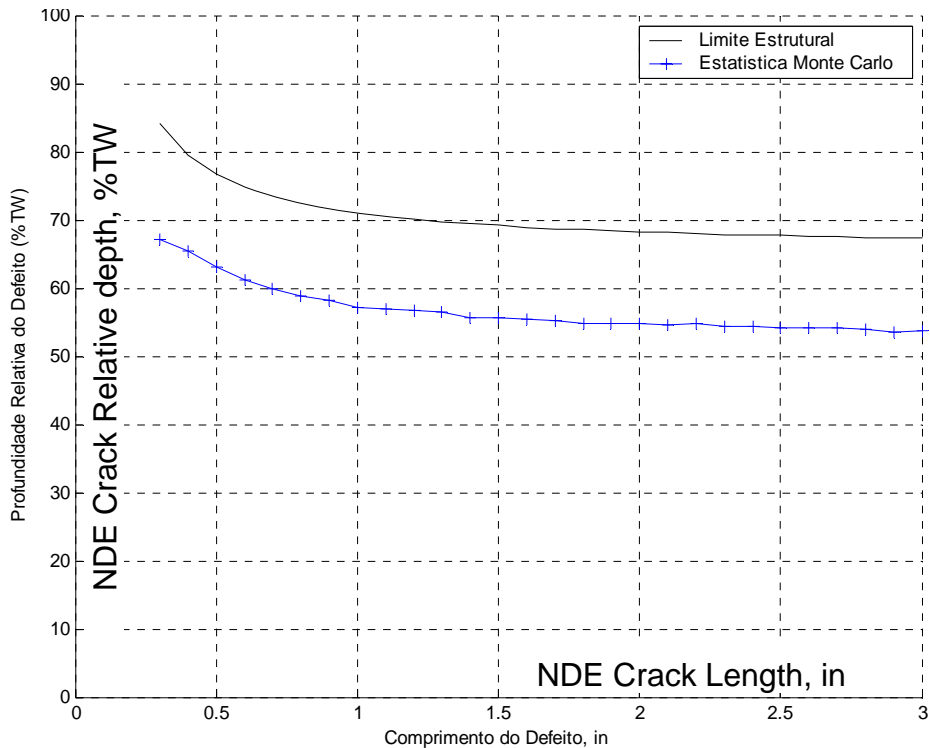
$$\text{Std deviation, } \sigma_{Gr,BCV} = 0.10 \text{ (Volt)}$$

} **OA**

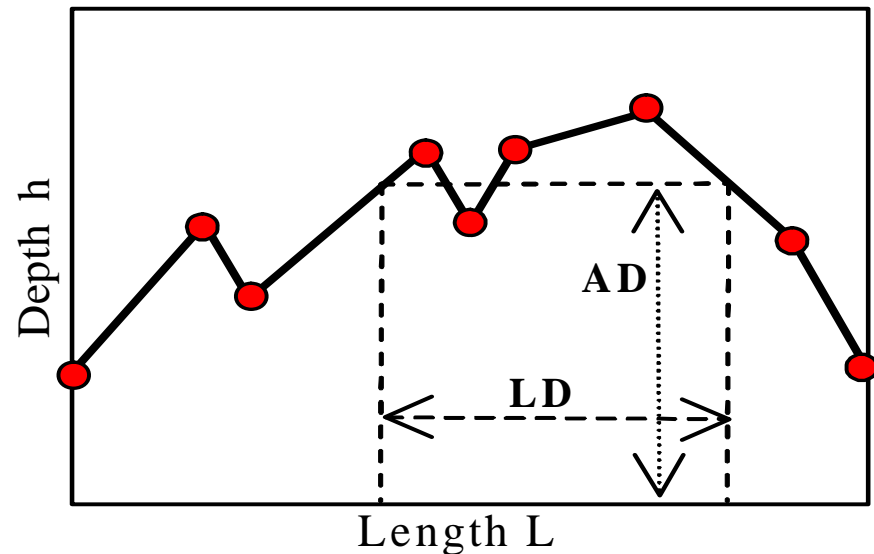
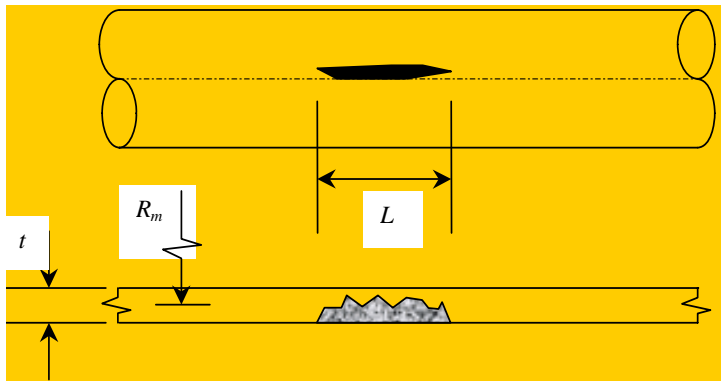


Ex. 3: Axial Thinning with Limited Circumferential Extent (Volumetric) - CM/OA

$Ca_L = 1.0$ $Ca_h = 1.0$ MeanGrowth_L = 0.2 ; MeanGrowth_h = 10 %
 $Cb_L = 0.0$ $Cb_h = 0.0$ Std dev., $\sigma_{L,Gr} = 0.1$; Std. dev., $\sigma_{h,Gr} = 5 \%$
 $SDev_L = 0.15$ $SDev_h = 10 \%$





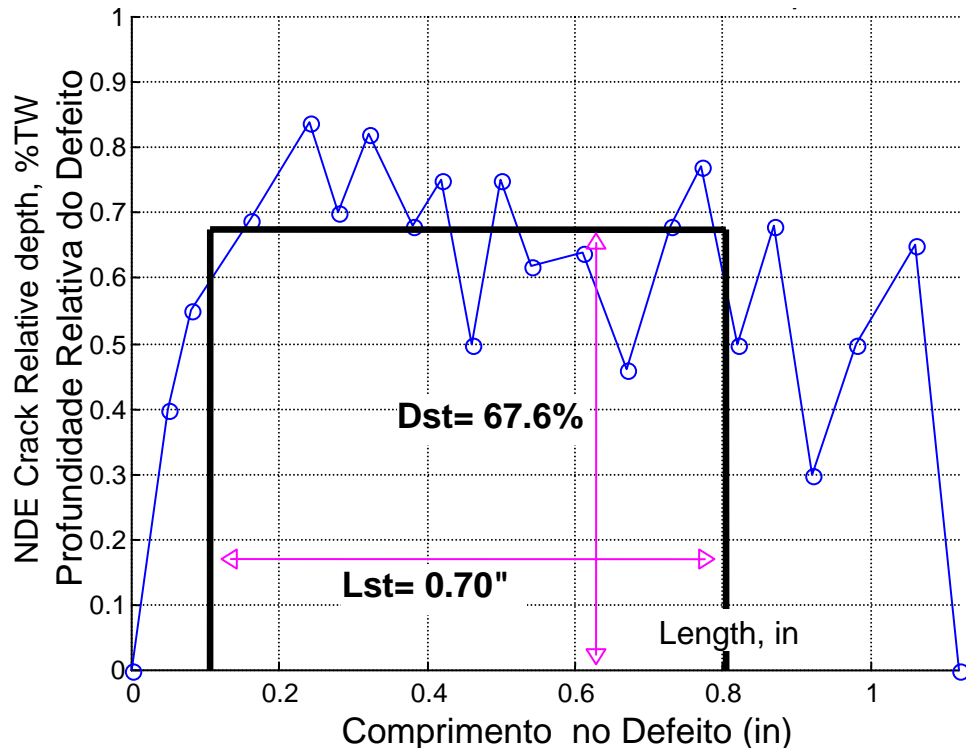
- . Obtain the critical equivalent dimensions AD & LD for an axial defect from its irregular (actual) profile obtained during the tube inspection
- . Developed in MATLAB language



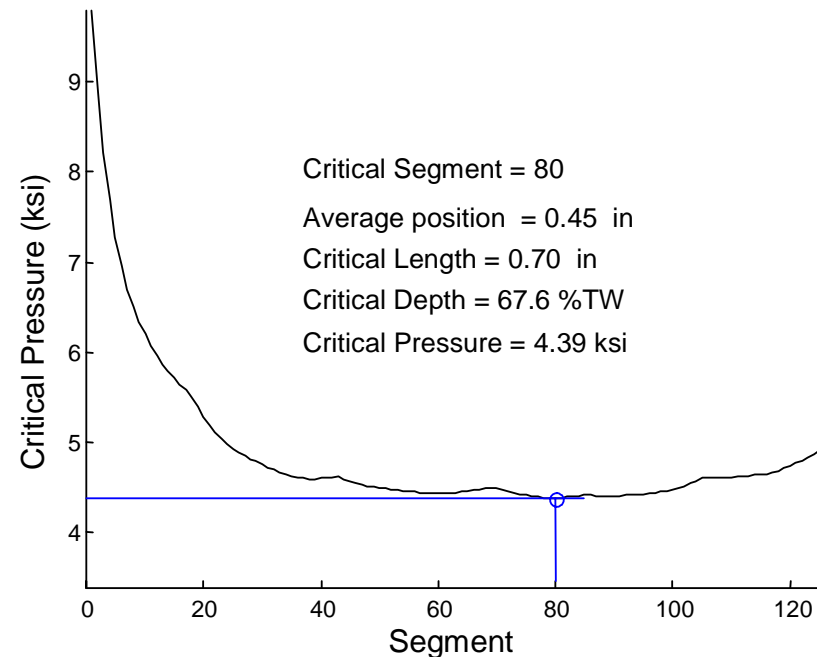
The tube with the idealized defect $AD \times LD$ will fail/burst with the same pressure P_B from the actual defect/profile (h_i, L_i)

Example of a defect/profile & Results

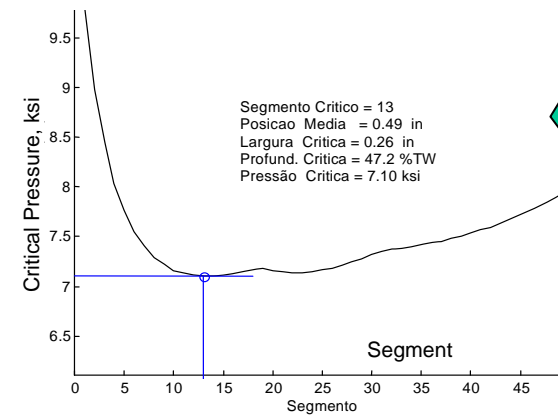
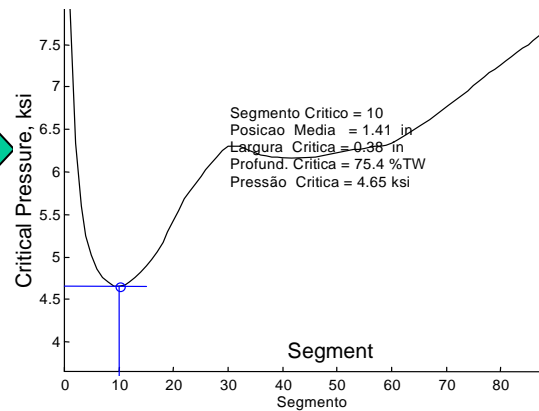
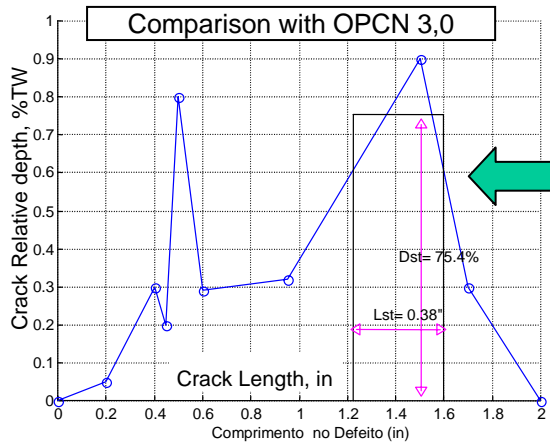
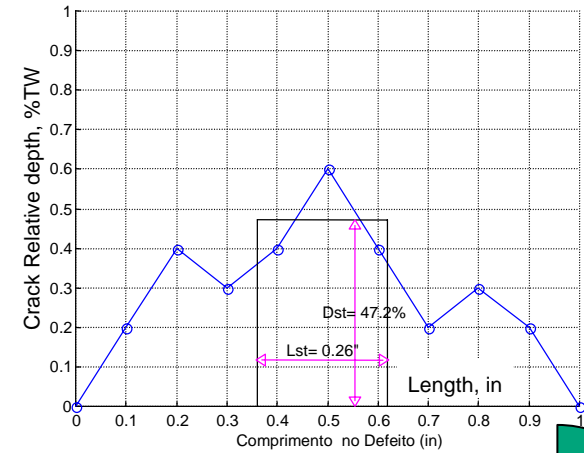
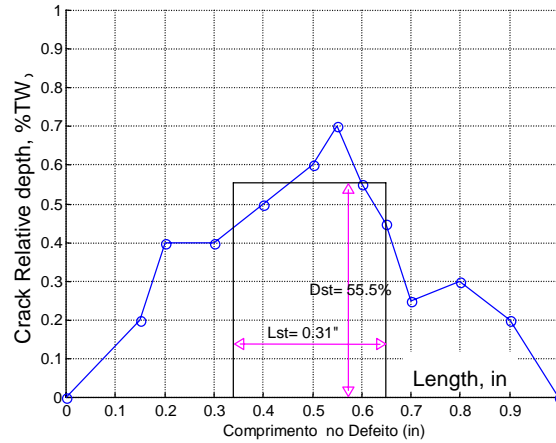
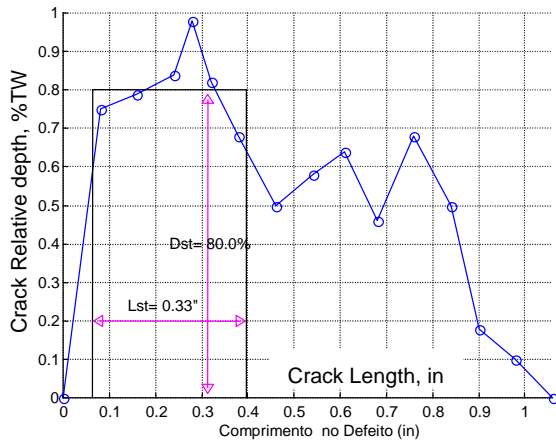
Equivalent defect 
 Actual defect 



Critical Pressure associated with the created segment defects



Other Tests & Results:

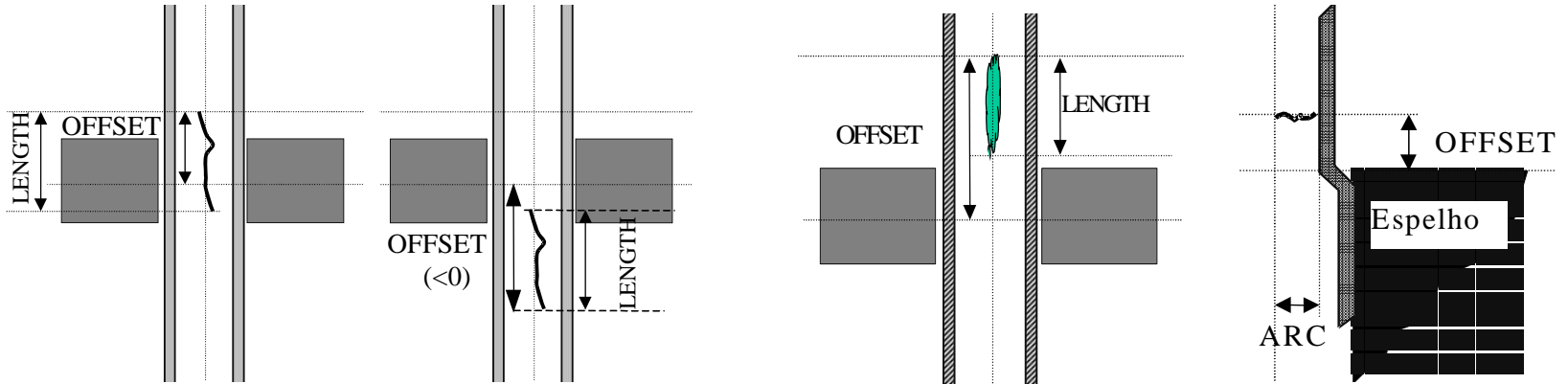


- . Select the defects/tubes of Angra 1 SG candidate to be tested *in situ* for burst (selection based on the defect dimensions)

The defects should be stratified (classified) based on:

- . Location along the tube/SG:
 - . Tubesheet
 - . Support Plate 01H
 - . Support Plate (Other)
 - . Free span, etc.
- . Orientation (with respect to the tube):
 - . Axial
 - . Circumferential
 - . Volumetric
- . Origin:
 - . Internal
 - . External
- . Developed in MATLAB language

Basic Defects – Dimensions (LENGTH / ARC) & OFFSET



Axial Defect

OFFSET > 0

OFFSET < 0

Volumetric

Circumferential

StrucLen - 'effective' defect length for Axial or Volumetric defects

→ it is the part of the defect outside of the TSP/TS

StrucLen ≤ LENGTH → defect partially inside

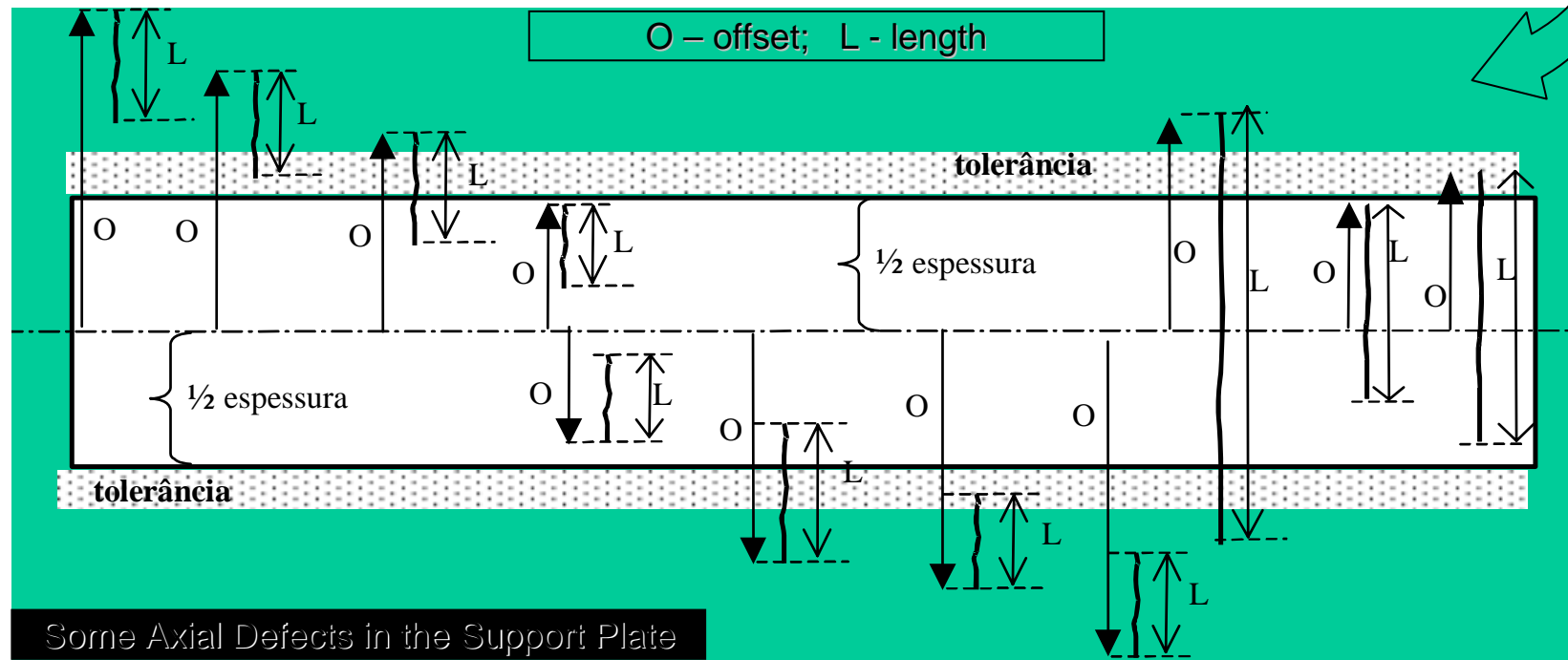
StrucLen = 0 → defect inside of the TSP/TS

Support Plate Thickness = 0,75"

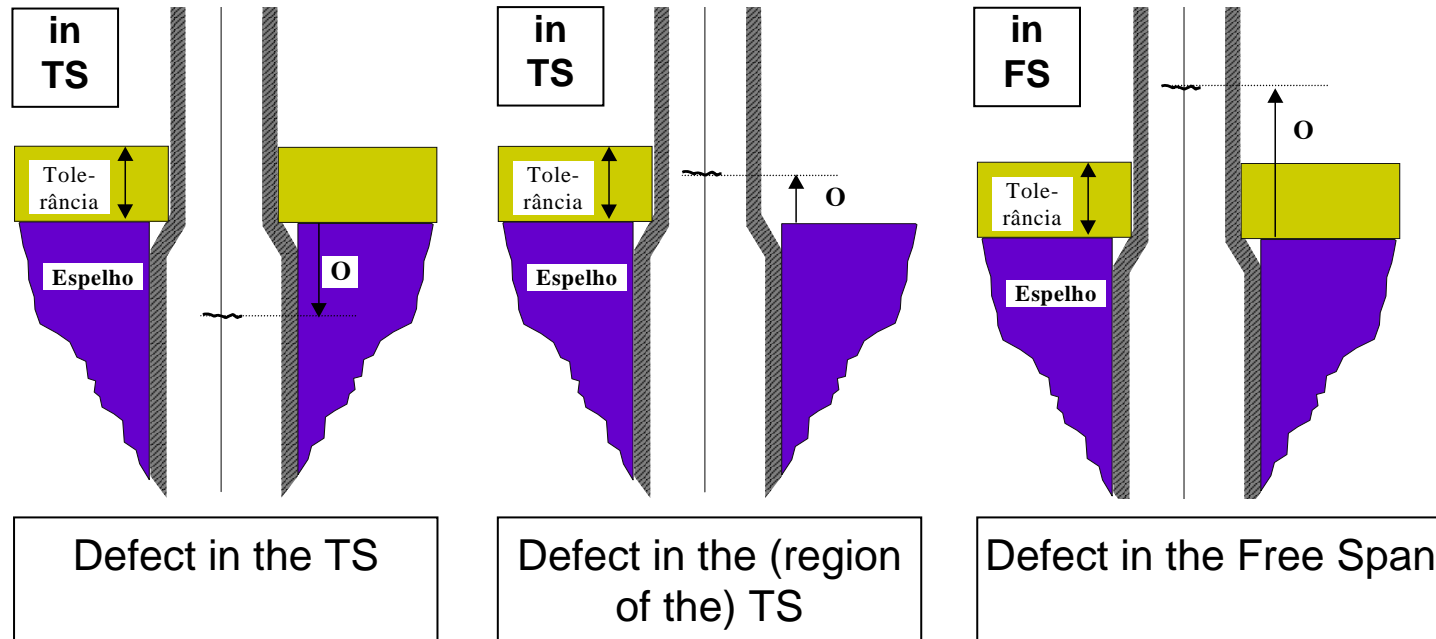
Defects in the Support Plates

The combination of the parameters (**Location**, **OFFSET** & **LENGTH**) gives multiple possibilities that should be tested one by one, being mutually exclusive

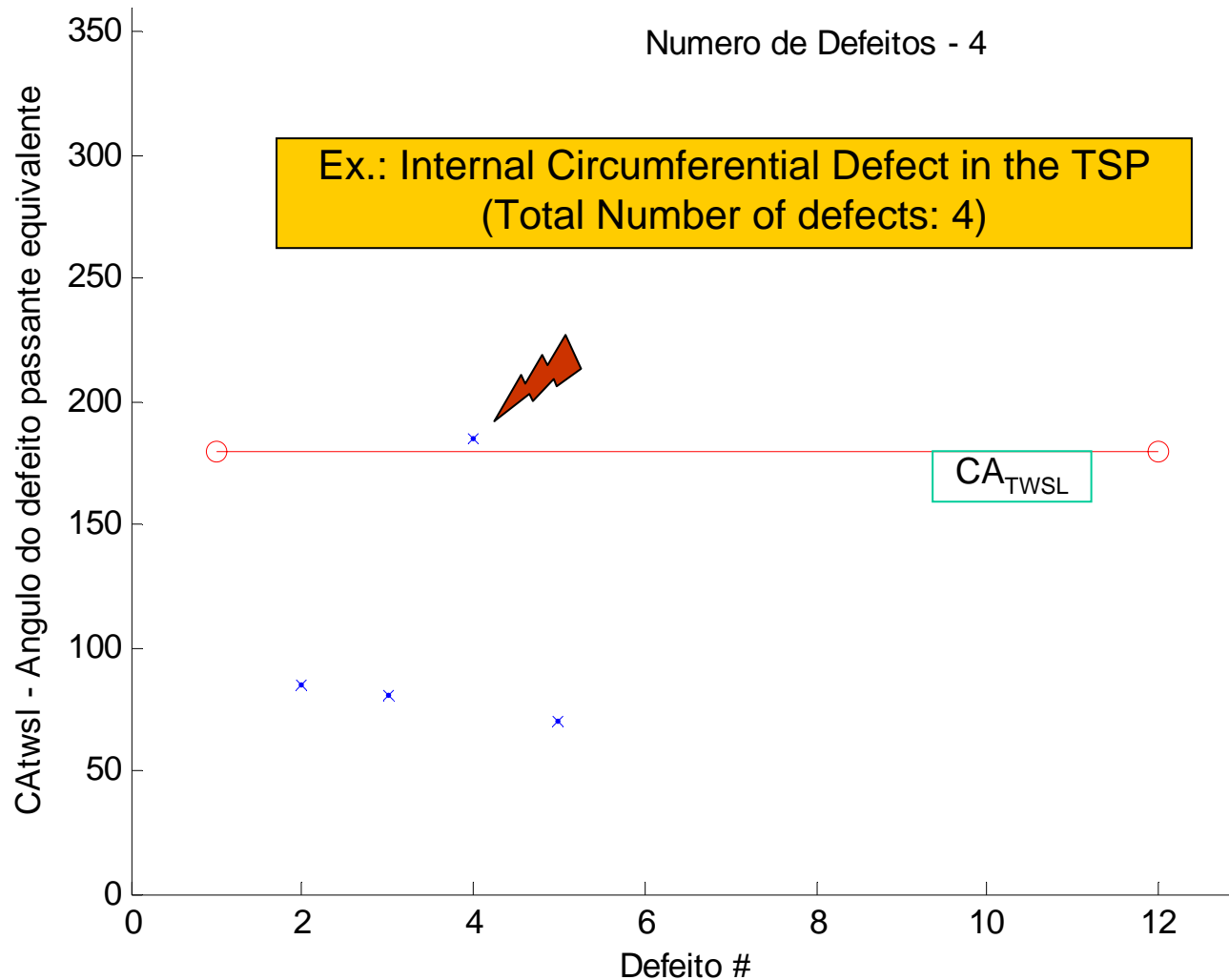
→ **More critical for the Axial defects in the Support Plate**

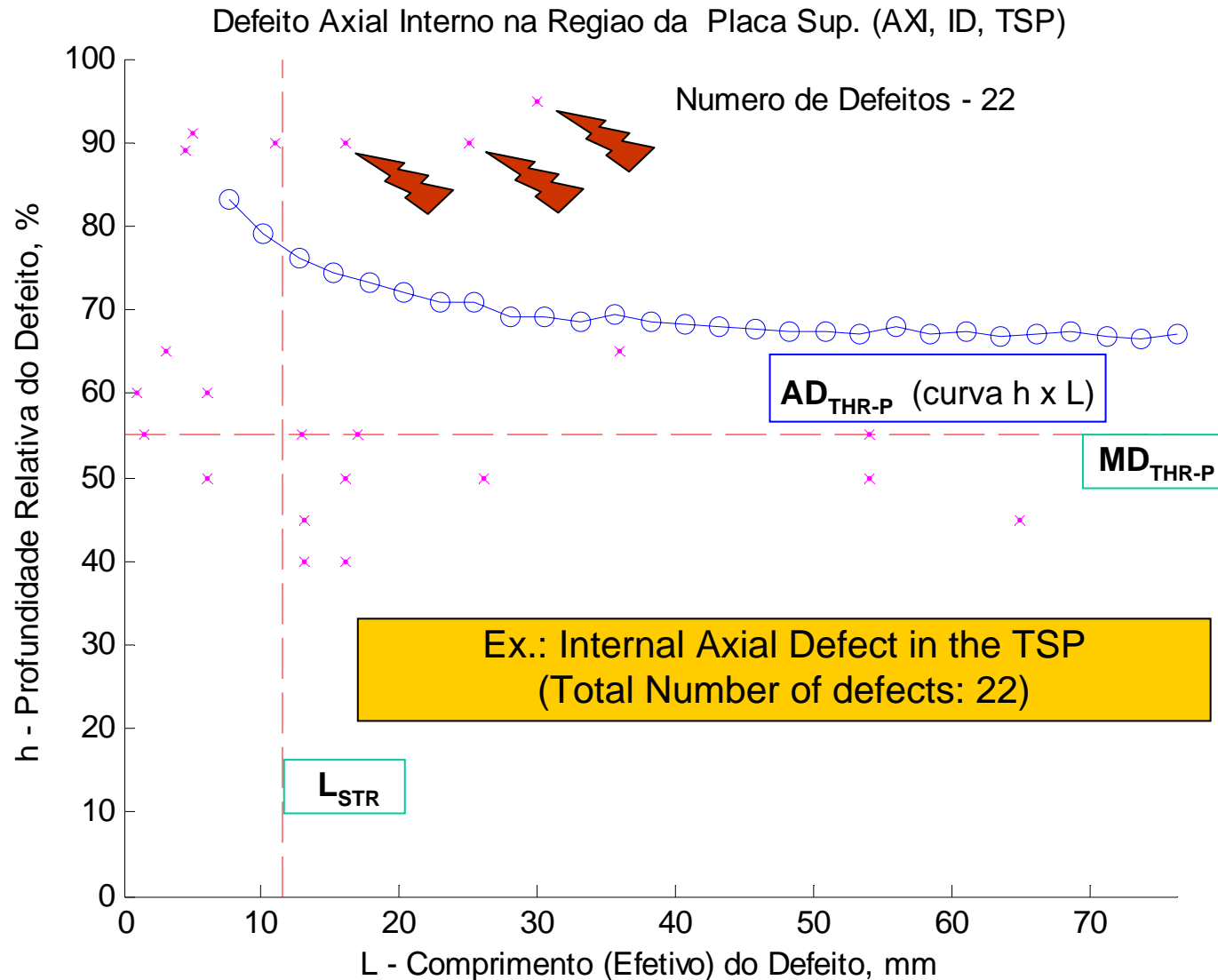


Examples of the Stratification/Classification for Circumferential Defects in the Tubesheet (TS) region



Defeito Circ. Interno na Regiao da Placa Sup. (CIR, ID, TSP)





Courses

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I – Fracture Mechanics and Crack Propagation

II – Codes and Standards for:

- a. Structural Integrity (*)
- b. Piping Design (*)
- c. Mechanical Equipment Design (*)

III – Structural Integrity Assessment in Angra 1 & 2

IV – Programs for Structural Integrity Assessment

(*) basically ASME Section III (Subsection NB) and Section XI