# ELECTRICAL CONDUCTIVITY AND MICROSTRUCTURAL ANALYSIS OF Cu-Ni-Be ALLOY FOR ELECTRONIC DEVICES

Jesus, S. L.; Monteiro, W. A.; Silva, L. C. E.

IPEN – Instituto de Pesquisas Energéticas e Nucleares

Caixa Postal 11049 – CEP 05422-970, São Paulo – SP – e-mail sl.jesus@net.ipen.br

In this work a study for a Cu-Ni-Be alloy was development using a Scanning Electron Microscopy (SEM), Energy Dispersive X-Ray Spectrometer (EDS) and a milliohmmeter. The high strength of Cu-Ni-Be used in electronic connectors is thought to be due to the enhanced precipitation of nickel-rich beryllium intermetallic phases from the supersaturated solution and a dislocation structure after a thermomechanical treatment <sup>3</sup>. This TMT, as well as the effect of two final aging were evaluated.

## **Experimental Procedure**

Six ingots were obtained by melting with electric-arc furnace and the concentration of Be range of 0,1 to 0,6%. All samples were homogenized at 955°C in resistance furnace and water quench at room temperature. These ingots were cold rolling with 35% reduction, pre-aging at 400°C and water quench. Other cold rolling with 60% reduction and two different final aging treatments at 380°C and 425°C. A Wolpert microhardness machine with 100g load and a model 4338B HP Milliohmmeter was used for mechanical and electrical analysis. The scanning microscopy was carried out on the Philips XL 30 combining the spectroscopy analysis.

#### **Results and Discussion**

Figure 1 shows the presence of a precipitate rich in nickel at matrix of copper after cold rolling and aging. The figure 2 presents precipitates at the structure after cold rolling and a TT. The electronic micrography in figure 3 shows the morphology of the precipitate. The increase of strength at the 0,3 and 0,6% Be alloys is a strong indicate the presence of beryllides and CuNi phases at copper matrix. The electrical conductivity values around 45% to 60% IACS agrees with other authors.

#### Conclusion

Cu-Be alloy are extremely hardened by aging at 250 to 400°C after quenching from solution treatment. The hardening is caused by the formation of G. P. zone and  $\gamma$ ' e  $\gamma$ '' phases (CuBe')<sup>1-2</sup> and  $\beta$ -NiBe. A thermomechanical treatment developed for a Cu-Ni-Be alloy consists in solution treatment - cold rolling to 35% reduction - pre-aging at 400°C - cold rolling to 60% reduction - final aging in the temperature range of 350-450°C. This TMT are convenient to improve the mechanical properties without expressive lost in electrical conductivity.

### **Bibliography**

- 1. Masamichi, M.; Yoshikiyo, O.; Syuhei, I.; "Effect of TM Processing on the Age-Hardening and Contraction Behavior of Cu-Be Alloys with Co and Ni, Conf., THERMEC 97, pp 1661 1667.
- 2. Tseng, A. A.; Chen, T. C.; Jen, K.P.; Ochiai, T.; "Forming and Fractographical Characteristics of Cu-Ni-Be Sheets Under Tension and Bending", J. M. Eng. Perform., Oct. 1994, pp. 619-634.
- 3. Rotem, A.; Shechtman, D.; and Rosen, A.; "Correlation among microstructure, strength and electrical conductivity of Cu-Ni-Be alloy"; Metall. Trans. A. 1988, vol. 19 A, pp.2279-2285.

#### Acknowledgment

The authors are grateful to FAPESP for financial support.

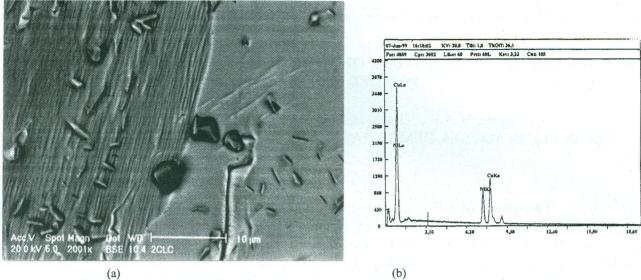


Figure 1 – (a) Showing Cu-Ni phases at grain boundary and (b) the spectroscopy -0.6% Be after solution treatment.

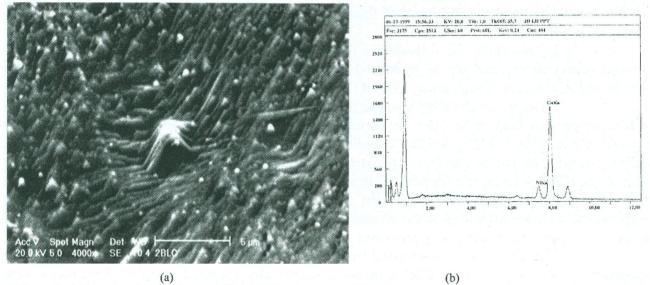
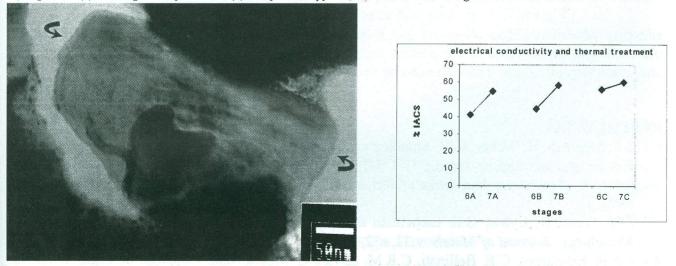


Figure 2 – (a) Showing Cu-Ni phases and (b) the spectroscopy – 0,3% Be after cold rolling and thermal treatment.



(a) (b) Figure 3-(a) Micrography of beryllites precipitates by TEM - 0,3% Be and (b) eletrical condutivity.